

Lecture 8: Limiting, Finite R, and Slew Rate

- Announcements:
- HW#3 online and due Friday via Gradescope
- Lab#2 is a two week lab
  - ↳ Prelab is due in the second week
  - ↳ But you should have proof of having started it when you go to lab this week
  - ↳ You will still do the lab this week and continue next week

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• Lecture Topics:

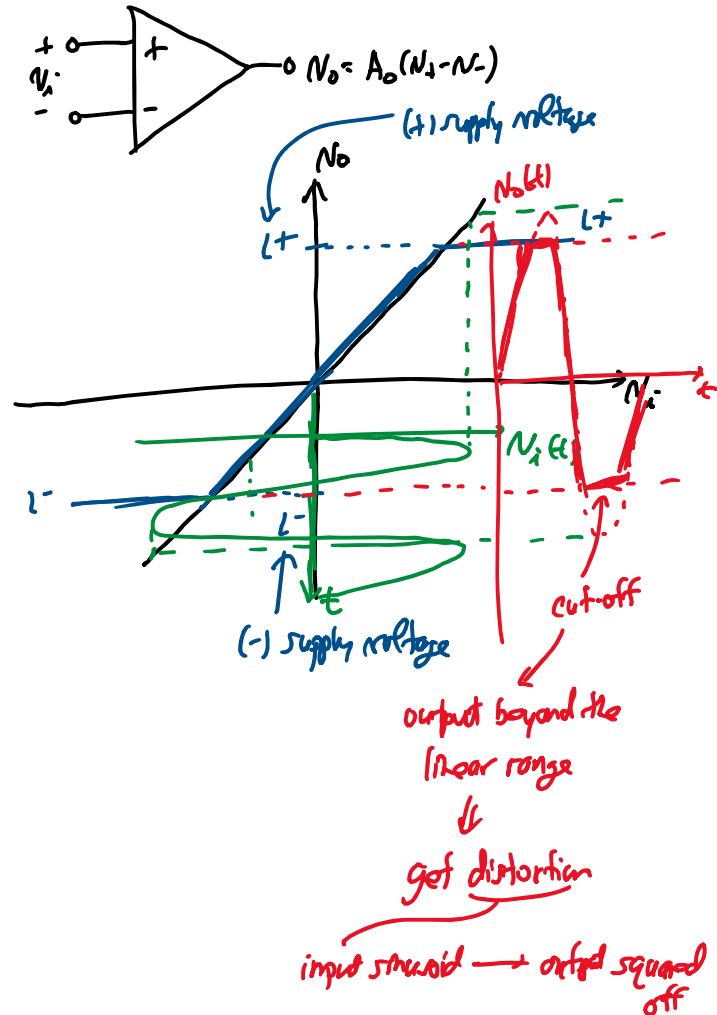
- ↳ Limiting
- ↳ Finite Input & Output Resistance
- ↳ Slew Rate

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• Last Time:

- Finished finite gain-BW op amp circuits
- Started limiting
- Now, continue with this ...

Output Saturation



**Finite Input & Output Resistance**

⇒ Equiv. ckt. for an op amp w/ finite  $R_i, R_o, A_v, BW$

$V_{DD}$   
 $V_{SS}$   
 $N^-$   
 $N^+$   
 $R_o$   
 $R_i$   
 $C_o$   
 $N_o$   
 $A_v(N^+ - N^-)$   
 $\omega_b = \frac{1}{R_o C_o}$

$|A(j\omega)|$  [dB]  
 $A_v$   
 $\omega_b$   
 $\omega$  (log)

**Slew Rate**

Unity Gain Follower -

$N_o$   
 $N_i$   
 $|A(j\omega)|$  [dB]  
 $A_o$   
 $\omega_b$   
 $\omega_T$   
 $\omega$  (log)  
 $A(s) = \frac{A_o}{1 + \frac{s}{\omega_b}}$

Step Response:

$$N_o(t) = N_o|_{t=\infty} - (N_o|_{t=\infty} - N_o|_{t=0}) e^{-t/\tau}$$

$$= N_o|_{t=\infty} (1 - e^{-t/\tau})$$

$\tau = \frac{1}{\omega_T}$

$N_i$   
 $V'$   
 $V$   
 $t=0$   
 $N_o$   
 $t$   
 step input w/ larger  $V'$   
 step input w/ small  $V$   
 expected

\*  
 ↓  
 Linear increase caused by internal op amp limitations (i.e., transistors) that constrain the output current of the op amp!

slope — slope  
 ↓  
 Max. Rate of change of output voltage }  $\equiv$  Slew Rate =  $SR = \left. \frac{dv_o}{dt} \right|_{\max}$  [V/ $\mu$ s]

Example. Output a sinusoid (or at least try to...)

largest slope =  $\frac{dv_o}{dt} > SR$       SR turns sinusoid into triangle wave

**Full Power Bandwidth**  $\leftarrow f_M$

- Suppose you wanted your op amp circuit to output a signal with a maximum amplitude  $V_{omax}$
- Then the full power bandwidth is the maximum frequency of this  $V_{omax}$  amplitude that the op amp can track without slewing

$v_o = V_{omax} \sin \omega t$

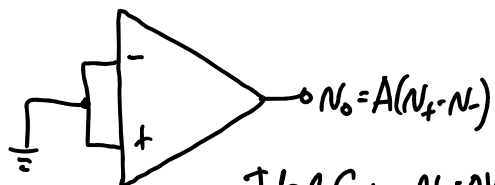
$\frac{dv_o}{dt} = \omega V_{omax} \cos \omega t$   
 $= \left. \frac{dv_o}{dt} \right|_{\max}$  at the max. expected output  
 ↓  
 this must equal to SR for proper tracking

$\omega_M V_{omax} = SR$

max frequency  $\therefore f_M = \frac{SR}{2\pi V_{omax}}$

Full Power Bandwidth

Input Offset Voltage,  $V_{os}$



Ideal Case:  $N_o = 0V$

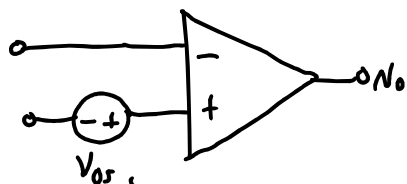
Reality:  $N_o \neq 0V$

(usually,  $N_o = I^+ - I^-$ )

it rails out

Model this w/ equivalent ckt:

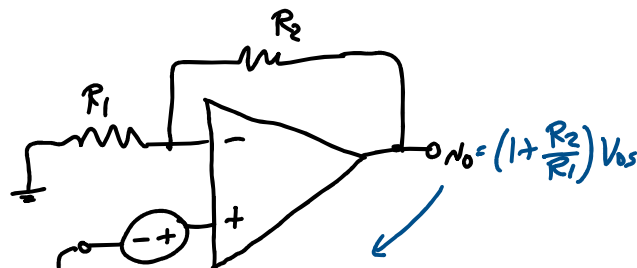
contains input offset  $V_{os}$ :



typically,  $V_{os} \sim 1mV - 5mV$

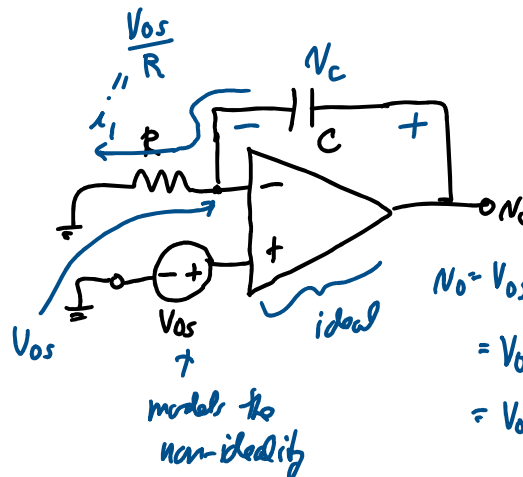
Effect of  $V_{os}$  on Op Amp Ckts

Example. Non-Inverting Amplifier



e.g.,  $\frac{R_2}{R_1} = 9$ ,  $V_{os} = 5mV \rightarrow V_o = 50mV$   
 (not so bad...)

Example. Integrator



$$\begin{aligned}
 N_o &= V_{os} + \frac{1}{C} \int_0^t i_i dt \\
 &= V_{os} + \frac{1}{C} \int_0^t \frac{V_{os}}{R} dt \\
 &= V_{os} \left(1 + \frac{t}{RC}\right) + N_c \Big|_{t=0}
 \end{aligned}$$

