

4.1 EECS 105 SPRING 2001, Solution HW #4 Xuesong Jiang Feb. 16, 2001

a) $\Phi_n = (60 \text{ mV}) \cdot \log\left(\frac{N_d}{10^{16}}\right) = (60 \text{ mV}) \cdot \log\left(\frac{10^{15}}{10^{16}}\right) = 300 \text{ mV}$

$\Phi_p = -(60 \text{ mV}) \cdot \log\left(\frac{N_a}{10^{16}}\right) = -(60 \text{ mV}) \cdot \log\left(\frac{10^{17}}{10^{16}}\right) = -420 \text{ mV}$

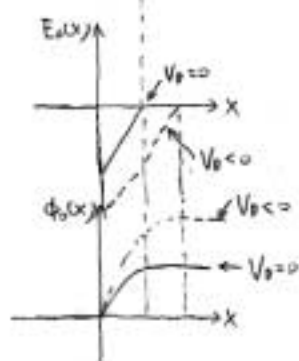
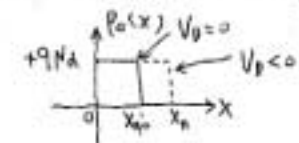
$\Phi_0 = \Phi_n - \Phi_p = 300 - (-420) = \boxed{720 \text{ mV}}$

b) $X_{do} = X_{no} + X_{po} = \sqrt{\frac{2\epsilon_s \Phi_0}{q} \left(\frac{1}{N_a} + \frac{1}{N_d}\right)}$

$= \sqrt{\frac{2(11.7)(8.85 \times 10^{-14} \text{ F/cm}^2)(0.72 \text{ V})}{1.6 \times 10^{-19} \text{ C}} \cdot \left(\frac{1}{10^{17} \text{ cm}^{-3}} + \frac{1}{10^{15} \text{ cm}^{-3}}\right)}$

$= \boxed{970 \text{ nm}}$

c) Assume the PN junction is a one-sided PN junction



$\frac{dE_o}{dx} = \frac{\rho(x)}{\epsilon_s}$

On the n-side of the depletion region

$E_o(x) = E_o(x_n) - \int_x^{x_n} \frac{qN_d}{\epsilon_s} dx'$

$= 0 - \frac{qN_d}{\epsilon_s} (x_n - x)$

$\Phi_o(x) = \Phi_o(0) + \int_0^x -E_o(x') dx'$

$= 0 + \int_0^x \frac{qN_d}{\epsilon_s} (x_n - x') dx'$

$= \frac{qN_d}{\epsilon_s} x_n x - \frac{qN_d}{2\epsilon_s} x^2$

$\Phi_o(x_n) = \frac{qN_d}{2\epsilon_s} x_n^2$

Since $\Phi_0 - V_D = \Phi_o(x_n) - \Phi_o(0) = \Phi_o(x_n)$ in the one-sided PN junction

$\Phi_0 - V_D = \frac{qN_d}{2\epsilon_s} x_n^2$

$x_n = \sqrt{\frac{2\epsilon_s(\Phi_0 - V_D)}{qN_d}}$

4.2

a) $V_{DS} > V_{DS} - V_{TN}$, Saturation $V_{TN} = V_{Tn}$

$I_D = (W/2L) \mu_n C_{ox} \cdot (V_{GS} - V_{TN})^2 (1 + \lambda_n V_{DS})$

$= \left(\frac{100 \mu\text{m}}{2.2 \mu\text{m}}\right) \cdot 50 \times 10^{-6} \frac{\text{A}}{\text{V}^2} \cdot (4 \text{ V})^2 \cdot \left[1 + \left(\frac{0.1}{2} \text{ V}^{-1}\right) \cdot 4.5 \text{ V}\right]$

$= \boxed{24.5 \text{ mA}}$

b) $V_{TN} = V_{Tn} + V_n \sqrt{-2\phi_p - V_{GS}} - \sqrt{-2\phi_p}$

$= 1 \text{ V} + (0.6 \text{ V}^{1/2}) \cdot (\sqrt{-2(-0.42 \text{ V}) + 2 \text{ V}} - \sqrt{-2 \cdot (-0.42)})$

$= 1.46 \text{ V}$

$V_{DS} > V_{DS} - V_{TN}$, Saturation

$I_D = (W/2L) \mu_n C_{ox} \cdot (V_{GS} - V_{TN})^2 (1 + \lambda V_{DS})$

$= \left(\frac{100 \mu\text{m}}{4 \mu\text{m}}\right) \cdot (50 \times 10^{-6} \frac{\text{A}}{\text{V}^2}) \cdot (3 + 1.46 \text{ V})^2 \cdot \left[1 + \left(\frac{0.1}{2} \text{ V}^{-1}\right) \cdot 2.5 \text{ V}\right]$

$= \boxed{3.335 \text{ mA}}$

$$V_{SD} < V_{SG} + V_{TP} \quad \boxed{\text{Triode}} \quad V_{TP} = V_{TOP}$$

$$I_D = (W/L) \mu_n C_{ox} \left[V_{SG} + V_{TP} - (V_{SD}/2) \right] (1 + \lambda_p V_{SD}) V_{SD}$$

$$= \left(\frac{100 \mu\text{m}}{2 \mu\text{m}} \right) \cdot 25 \times 10^{-6} \frac{\text{A}}{\text{V}^2} \left[4\text{V} - 1\text{V} - \frac{2.5\text{V}}{2} \right] \cdot \left[1 + \left(\frac{0.1}{2} \right) \cdot 2.5\text{V} \right] \cdot 2.5\text{V}$$

$$= \boxed{6.152 \text{ mA}}$$

$$V_{TP} = V_{TOP} - V_p \left(\sqrt{2\phi_n - V_{SG}} - \sqrt{2\phi_n} \right)$$

$$= -1\text{V} - 0.6\text{V} \cdot \left(\sqrt{2 \cdot 0.42\text{V} + 1\text{V}} - \sqrt{2 \cdot 0.42\text{V}} \right)$$

$$= -1.264 \text{ V}$$

$$V_{SD} < V_{SG} + V_{TP} \quad \boxed{\text{Triode}}$$

$$-I_D = (W/L) \mu_p C_{ox} \left[V_{SG} + V_{TP} - (V_{SD}/2) \right] (1 + \lambda_p V_{SD}) V_{SD}$$

$$= \left(\frac{100 \mu\text{m}}{2 \mu\text{m}} \right) \cdot 25 \times 10^{-6} \frac{\text{A}}{\text{V}^2} \left[3\text{V} - 1.264\text{V} - \frac{1.5\text{V}}{2} \right] \cdot \left[1 + \left(\frac{0.1}{2} \right) \cdot 1.5\text{V} \right] \cdot 1.5\text{V}$$

$$= \boxed{1.987 \text{ mA}}$$

$$3. \quad k_p = \mu_n C_{ox} \quad \text{from the graph, } V_{TH} \approx 0.5\text{V}$$

a) In triode region

$$I_D = (W/L) \cdot k_p \cdot \left[V_{GS} - V_{TH} - \frac{V_{DS}}{2} \right] V_{DS} \quad (\text{neglect } \lambda \cdot V_{DS})$$

$$\frac{dI_D}{dV_{GS}} = k_p \left(\frac{W}{L} \right) (V_{GS} - V_{TH} - V_{DS})$$

$$\frac{dI_D}{dV_{GS}} (V_{DS} = 0) = k_p \left(\frac{W}{L} \right) (V_{GS} - V_{TH}) = k_p \cdot \left(\frac{100 \mu\text{m}}{20 \mu\text{m}} \right) \cdot (V_{GS} - 0.5\text{V})$$

$$\text{when } V_{GS} = 5\text{V}, \quad \frac{dI_D}{dV_{GS}} (V_{DS} = 0) \approx 1 \frac{\text{mA}}{\text{V}}$$

$$\therefore k_p = \frac{dI_D}{dV_{GS}} (V_{DS} = 0) \cdot \left(\frac{20 \mu\text{m}}{100 \mu\text{m}} \right) \cdot \frac{1}{V_{GS} - 0.5\text{V}} = 10^{-3} \frac{\text{A}}{\text{V}} \cdot \frac{1}{5} \cdot \frac{1}{4.5\text{V}} = \boxed{44 \mu\text{A}/\text{V}^2}$$

3/5

b) In saturation region

$$I_D = \frac{k_p}{2} \cdot \frac{W}{L} (V_{GS} - V_{TH})^2$$

$$\text{When } V_{GS} = 5\text{V}, \quad V_{DS} = 5\text{V}, \quad I_D = 2.25 \text{ mA}$$

$$k_p = \frac{2I_D}{\frac{W}{L} \cdot (V_{GS} - V_{TH})^2} = \frac{2 \cdot 2.25 \text{ mA}}{\frac{100 \mu\text{m}}{20 \mu\text{m}} (5\text{V} - 1\text{V})^2} = \boxed{44 \mu\text{A}/\text{V}^2}$$

4.4.

a) In triode region,

$$\begin{cases} I_D = (W/L) \mu_n C_{ox} \left[V_{GS} - V_{TN} - \left(\frac{V_{DS}}{2} \right) \right] V_{DS} \\ V_{DS} = V_{out} = 5\text{V} - I_D \cdot R_L \end{cases}$$

$$\therefore V_{out} = 5\text{V} - (W/L) \mu_n C_{ox} \left[V_{in} - V_{TN} - \frac{V_{out}}{2} \right] \cdot V_{out} \cdot R_L$$

$$\therefore (W/L) \mu_n C_{ox} \frac{V_{out}^2}{2} \cdot R_L - [(W/L) \mu_n C_{ox} (V_{in} - V_{TN}) \cdot R_L + 1] \cdot V_{out} + 5\text{V} = 0$$

$$\therefore V_{out} = \frac{[(W/L) \mu_n C_{ox} (V_{in} - V_{TN}) \cdot R_L + 1] \pm \sqrt{[(W/L) \mu_n C_{ox} (V_{in} - V_{TN}) \cdot R_L + 1]^2 - 4 \cdot 5\text{V} \cdot \text{A}}}{2 \cdot (W/L) \mu_n C_{ox} \cdot R_L \cdot \frac{1}{2}}$$

$$\text{A} = \frac{1}{2} (W/L) \mu_n C_{ox} R_L$$

$$(W/L) \mu_n C_{ox} \cdot R_L = 25 \cdot \text{V}^{-1}$$

$$\therefore V_{out} = \frac{[(25 \text{ V}^{-1}) \cdot (V_{in} - 1\text{V}) + 1] \pm \sqrt{[(25 \text{ V}^{-1}) \cdot (V_{in} - 1\text{V}) + 1]^2 - 4 \cdot 5\text{V} \cdot \frac{1}{2} \cdot 25 \text{ V}^{-1}}}{25 \text{ V}^{-1}}$$

b) $V_{in} = 3\text{V}$, the MOSFET is in triode region

$$\therefore V_{out} = \frac{[25 \text{ V}^{-1} \cdot (3\text{V} - 1\text{V}) + 1] - \sqrt{[25 \text{ V}^{-1} \cdot (3\text{V} - 1\text{V}) + 1]^2 - 2 \cdot 3\text{V} \cdot 25 \text{ V}^{-1}}}{25 \text{ V}^{-1}}$$

$$= \boxed{100 \text{ mV}}$$

$$I_{out} = \frac{5\text{V} - V_{out}}{R_L} = \frac{5\text{V} - 100 \text{ mV}}{10 \text{ k}\Omega} = \boxed{0.49 \text{ mA}}$$

4/5

$$c). V_{in} = V_{in0} + \Delta V_{in}, \quad V_{out} = V_{out0} + \Delta V_{out}$$

From a).

$$V_{out0} + \Delta V_{out} = 5V - (W/L) \mu_n C_{ox} \left[(V_{in0} + \Delta V_{in} - V_{Tn}) - \frac{V_{out0} + \Delta V_{out}}{2} \right] \cdot (V_{out0} + \Delta V_{out}) \cdot R_L$$

$$\therefore \Delta V_{out} = - (W/L) \mu_n C_{ox} \cdot \left[\Delta V_{in} - \frac{\Delta V_{out}}{2} \right] \cdot (V_{out0} + \Delta V_{out}) \cdot R_L$$

$$- (W/L) \mu_n C_{ox} \cdot \left[V_{in0} - V_{Tn} - \frac{V_{out0}}{2} \right] \cdot \Delta V_{out} \cdot R_L$$

Neglect higher-order terms and using $(W/L) \mu_n C_{ox} \cdot R_L = 25 V^{-1}$

$$\therefore \Delta V_{out} = - 25 V^{-1} \cdot \left[\Delta V_{in} - \frac{\Delta V_{out}}{2} \right] \cdot V_{out0} - 25 V^{-1} \cdot \left[V_{in0} - V_{Tn} - \frac{V_{out0}}{2} \right] \cdot \Delta V_{out}$$

$$\therefore \frac{\Delta V_{out}}{\Delta V_{in}} = \frac{-V_{out0}}{V_{in0} - V_{Tn} - V_{out0} + \frac{1}{25 V^{-1}}} = \frac{-100 mV}{3V - 1V - 0.1V + 0.04V} = \boxed{-\frac{1}{19.4}}$$

$$= \boxed{-0.0515}$$

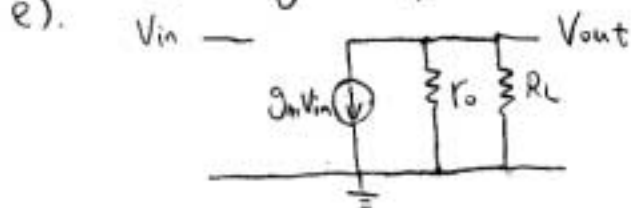
$$d) g_m = \frac{\partial I_D}{\partial V_{GS}} = (W/L) \cdot \mu_n C_{ox} \cdot V_{DS} = \left(\frac{100 \mu m}{2 \mu m} \right) \cdot 50 \mu A/V^2 \cdot V_{DS}$$

$$= 50 \cdot 50 \mu A/V^2 \cdot 0.1V = \boxed{250 \mu A/V}$$

$$\frac{1}{r_o} = \left(\frac{\partial I_D}{\partial V_{DS}} \right)$$

$$\therefore r_o = \frac{1}{(W/L) \cdot \mu_n C_{ox} [V_{GS} - V_{Tn} - V_{DS}]} = \frac{1}{50 \cdot 50 \mu A/V^2 \cdot 1.9V} = \boxed{210.5 \Omega}$$

e). Small signal equivalent circuit



$$\frac{V_{out}}{V_{in}} = -g_m (r_o \parallel R_L) = -(250 \mu A/V) \cdot (210.5 \Omega \parallel 10k\Omega)$$

$$= \boxed{-0.0515}$$