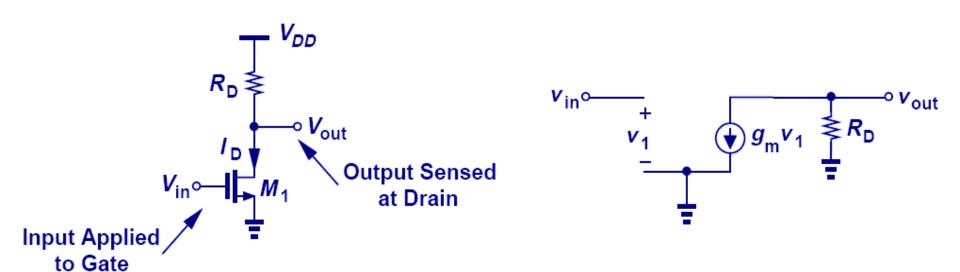
Lecture 18

OUTLINE

- Basic MOSFET amplifier
- MOSFET biasing
- MOSFET current sources
- Common-source amplifier

• Reading: Chap. 7.1-7.2

Common-Source Stage



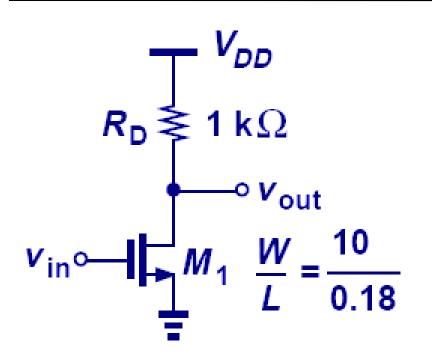
$$\lambda = 0$$

$$A_{v} = -g_{m}R_{D}$$

$$A_{v} = -\sqrt{2\mu_{n}C_{ox}\frac{W}{L}I_{D}}R_{D}$$

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Operation in Saturation



Condition for M₁ in saturation

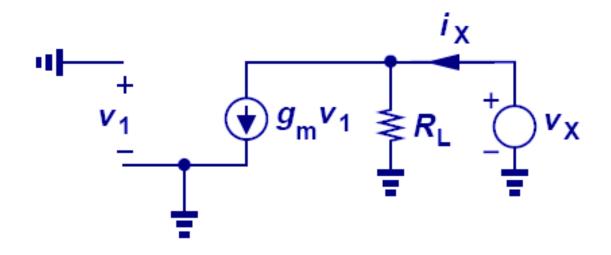
$$V_{out} > V_{in} - V_{TH}$$

$$\Rightarrow V_{DD} - R_D I_D > (V_{GS} - V_{TH})$$

- In order to maintain operation in saturation, V_{out} cannot fall below V_{in} by more than one threshold voltage.
- The condition above ensures operation in saturation.

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CS Stage with λ =0

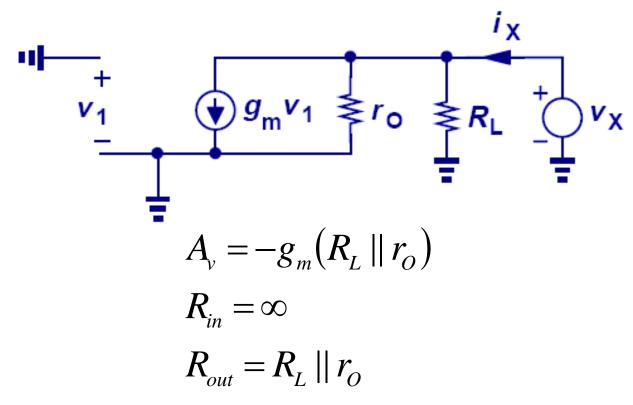


$$A_{v} = -g_{m}R_{L}$$

$$R_{in} = \infty$$

$$R_{L} = R_{L}$$

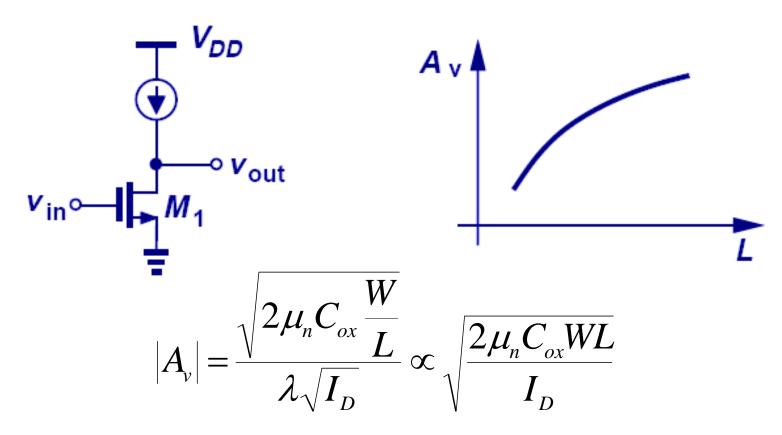
CS Stage with $\lambda \neq 0$



 However, channel length modulation leads to finite output resistance, r_o, which is in parallel with the load resistance, R_I

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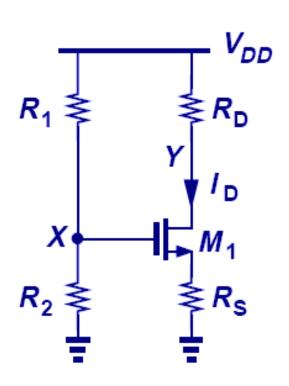
CS Gain Variation with Channel Length



• Since λ is inversely proportional to L, the intrinsic voltage gain actually becomes proportional to the square root of L.

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MOS Biasing



$$\frac{R_{1}}{R_{1} + R_{2}} V_{DD} = V_{GS} + I_{D} R_{S}$$

$$I_{D} = \frac{1}{2} \mu_{n} C_{ox} \frac{W}{L} (V_{GS} - V_{TH})^{2}$$

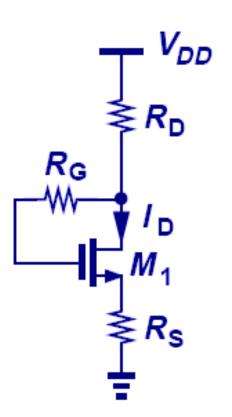
2 unknows (V_{GS}, I_D) , 2 equations \Rightarrow

$$V_{GS} = -(V_1 - V_{TH}) + \sqrt{V_1^2 + 2V_1 \left(\frac{R_2 V_{DD}}{R_1 + R_2} - V_{TH}\right)}$$

$$V_1 = \frac{1}{\mu_n C_{ox} \frac{W}{I} R_S}$$

- Voltage at X is determined by V_{DD}, R₁, and R₂.
- V_{GS} can be found using the equation above, and I_D can be found by using the NMOS current equation.

Self-Biased MOS Stage

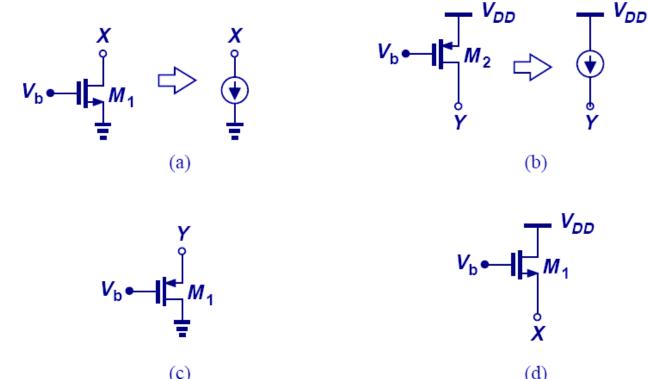


$$I_{D}R_{D} + V_{GS} + R_{S}I_{D} = V_{DD}$$

$$I_{D} = \frac{1}{2}\mu_{n}C_{ox}\frac{W}{L}(V_{GS} - V_{TH})^{2}$$

 The circuit above is analyzed by noting M₁ is in saturation and no potential drop appears across RG.

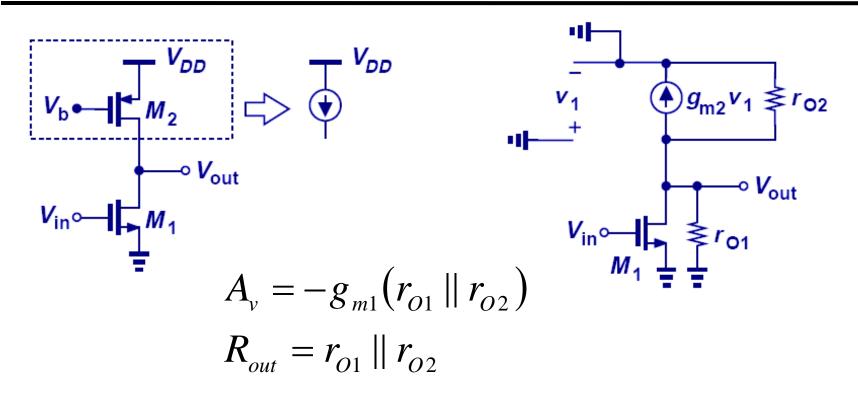
Current Sources



- When in saturation region, a MOSFET behaves as a current source.
- NMOS draws current from a point to ground (sinks current), whereas PMOS draws current from V_{DD} to a point (sources current).

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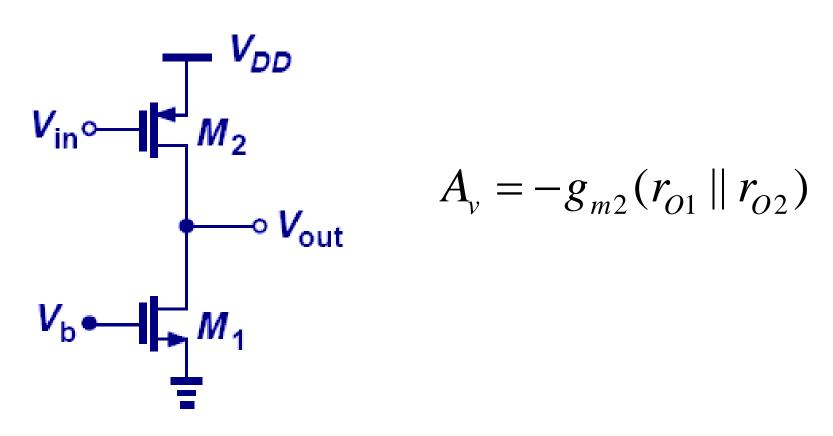
CS Stage with Current-Source Load



- To alleviate the headroom problem, an active current-source load is used.
- This is advantageous because a current-source has a high output resistance and can tolerate a small voltage drop across it.

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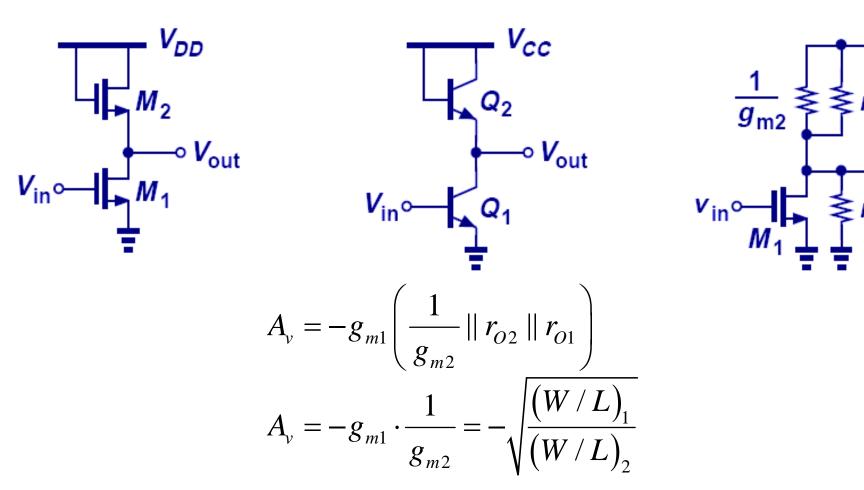
PMOS CS Stage with NMOS as Load



• Similarly, with PMOS as input stage and NMOS as the load, the voltage gain is the same as before.

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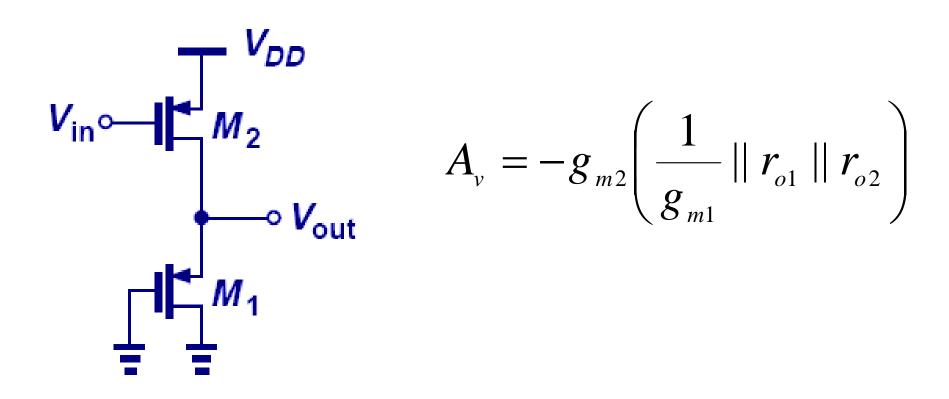
CS Stage with Diode-Connected Load



Lower gain, but less dependent on process parameters.

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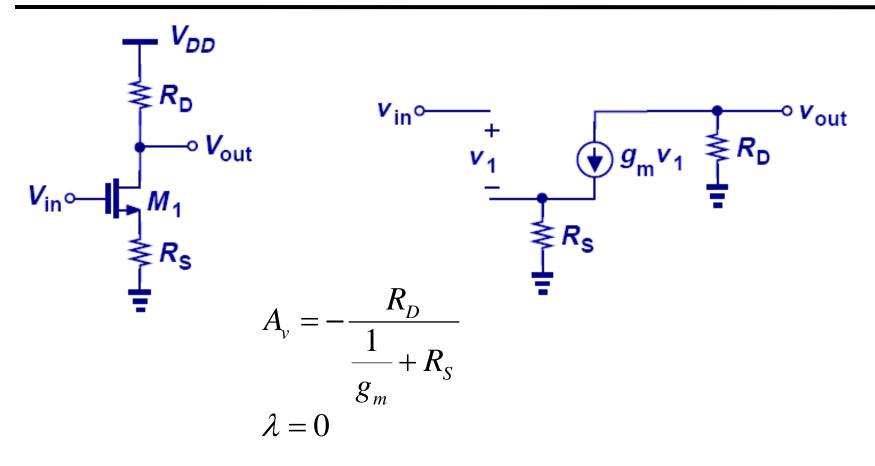
CS Stage with Diode-Connected PMOS Device



 Note that PMOS circuit symbol is usually drawn with the source on top of the drain.

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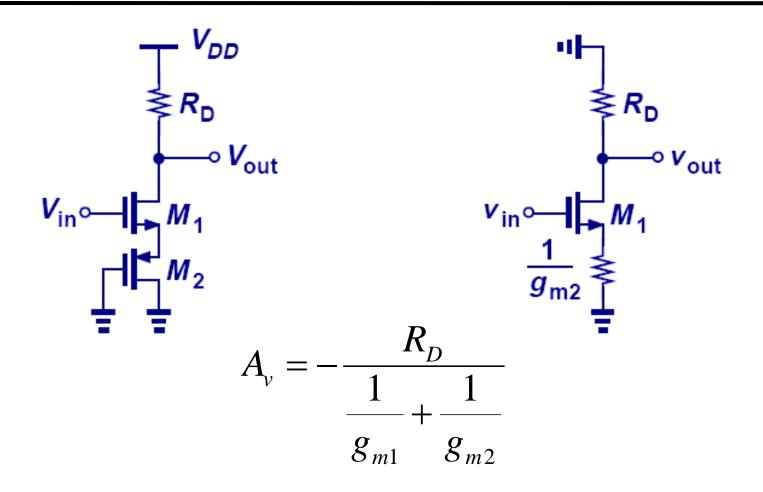
CS Stage with Degeneration



 Similar to bipolar counterpart, when a CS stage is degenerated, its gain, I/O impedances, and linearity change.

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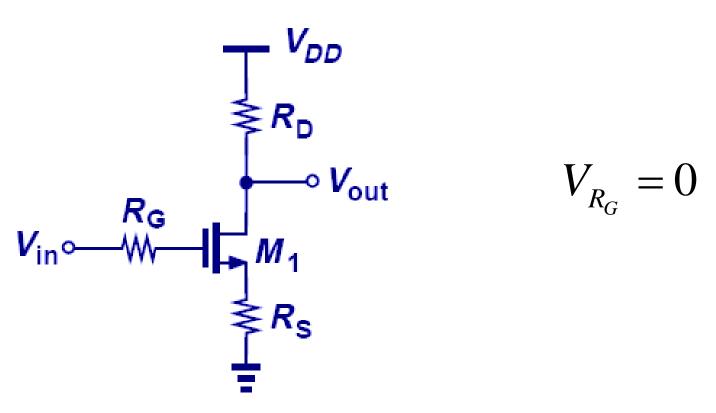
Example of CS Stage with Degeneration



A diode-connected device degenerates a CS stage.

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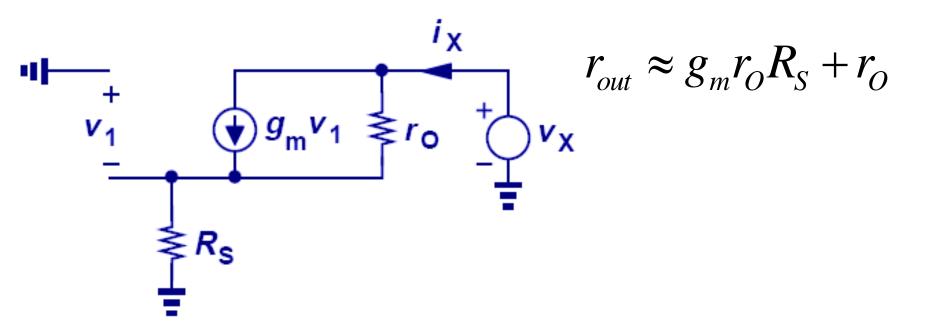
CS Stage with Gate Resistance



 Since at low frequencies, the gate conducts no current, gate resistance does not affect the gain or I/O impedances.

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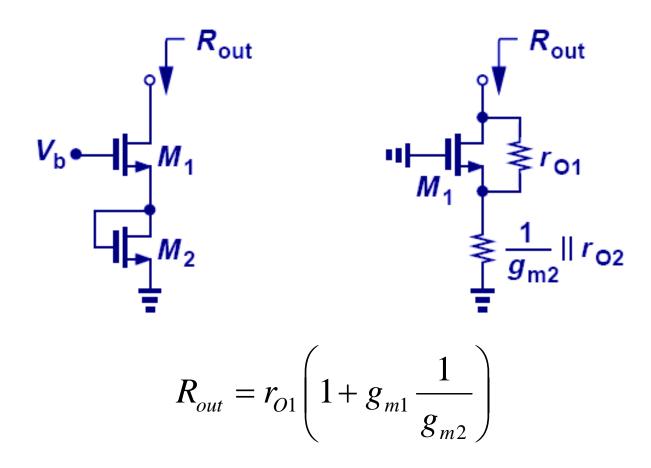
Output Impedance of CS Stage with Degeneration



 Similar to the bipolar counterpart, degeneration boosts output impedance.

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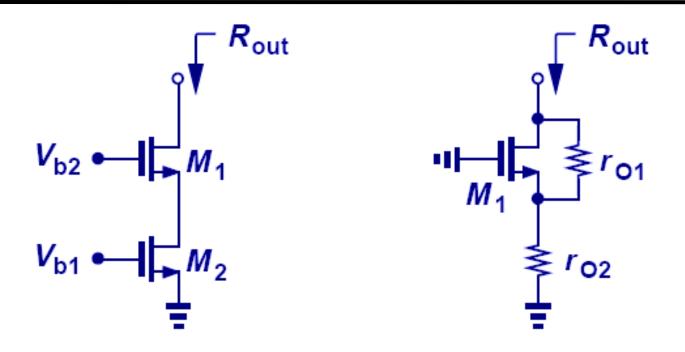
Output Impedance Example (I)



• When $1/g_m$ is parallel with r_{O2} , we often just consider $1/g_m$

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Output Impedance Example (II)

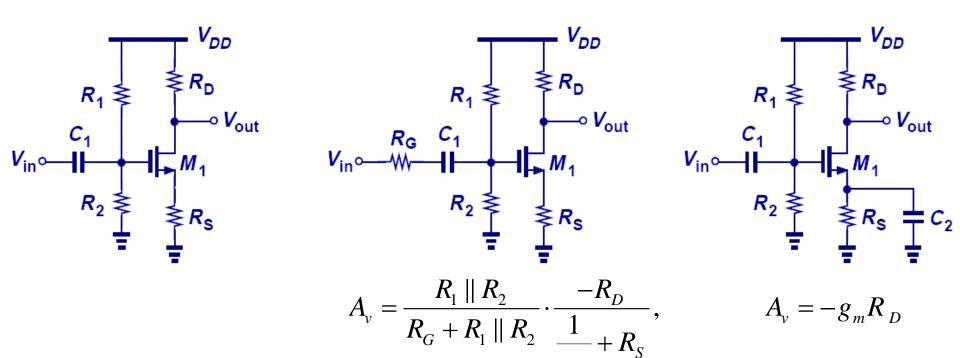


$$R_{out} \approx g_{m1} r_{O1} r_{O2} + r_{O1}$$

• In this example, the impedance that degenerates the CS stage is r_0 , instead of $1/g_m$ in the previous example.

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CS Core with Biasing



 Degeneration is used to stabilize bias point, and a bypass capacitor can be used to obtain a larger small-signal voltage gain at the frequency of interest.

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