

Lecture 23

OUTLINE

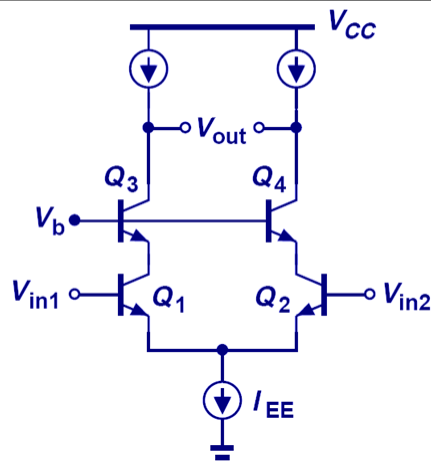
- BJT Differential Amplifiers (cont'd)
 - Cascode differential amplifiers
 - Common-mode rejection
 - Differential pair with active load
- Reading: Chapter 10.4-10.6.1

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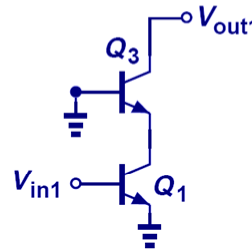
Cascode Differential Pair



$$R_{out} = [1 + g_{m3}(r_{O1} \parallel r_{\pi3})]r_{O3} + r_{O1} \parallel r_{\pi3}$$

$$R_{out} \cong g_{m3}(r_{O1} \parallel r_{\pi3})r_{O3} + r_{O1} \parallel r_{\pi3}$$

Half circuit for ac analysis



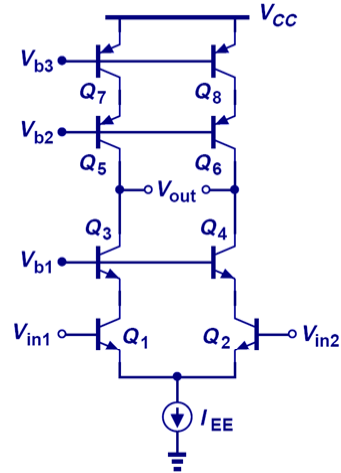
$$A_v = -g_{m1}R_{out} \cong -g_{m1}[g_{m3}(r_{O1} \parallel r_{\pi3})r_{O3} + r_{O1} \parallel r_{\pi3}]$$

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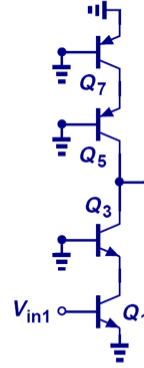
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Telescopic Cascode Differential Pair



Half circuit for ac analysis



$$A_v \approx -g_{m1} [g_{m3} r_{O3} (r_{O1} \parallel r_{\pi3})] \parallel [g_{m5} r_{O5} (r_{O7} \parallel r_{\pi5})]$$

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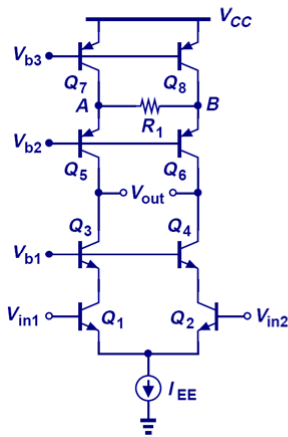
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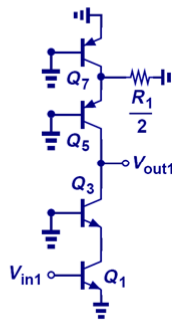
Example

$$R_{op} = \left[1 + g_{m5} \left(r_{O7} \parallel r_{\pi5} \parallel \frac{R_1}{2} \right) \right] r_{O5} + r_{O7} \parallel r_{\pi5} \parallel \frac{R_1}{2}$$

$$A_v = -g_{m1} \left([g_{m3} r_{O3} (r_{O1} \parallel r_{\pi3})] \parallel R_{op} \right)$$



Half circuit for ac analysis



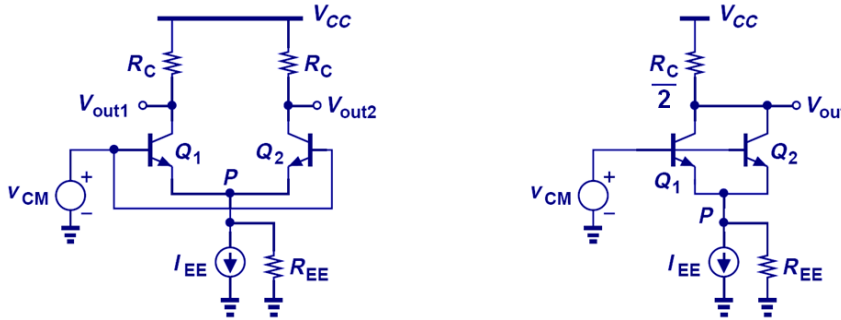
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Effect of Finite Tail Impedance

- If the tail current source is not ideal, then when an input common-mode voltage is applied, the currents in Q_1 and Q_2 and hence the output common-mode voltage will change.



$$\frac{\Delta V_{out,CM}}{\Delta V_{in,CM}} = -\frac{(R_C/2)}{\frac{1}{2g_m} + R_{EE}} = -\frac{R_C}{\frac{1}{g_m} + 2R_{EE}} \leftarrow \text{Common-mode gain should be small}$$

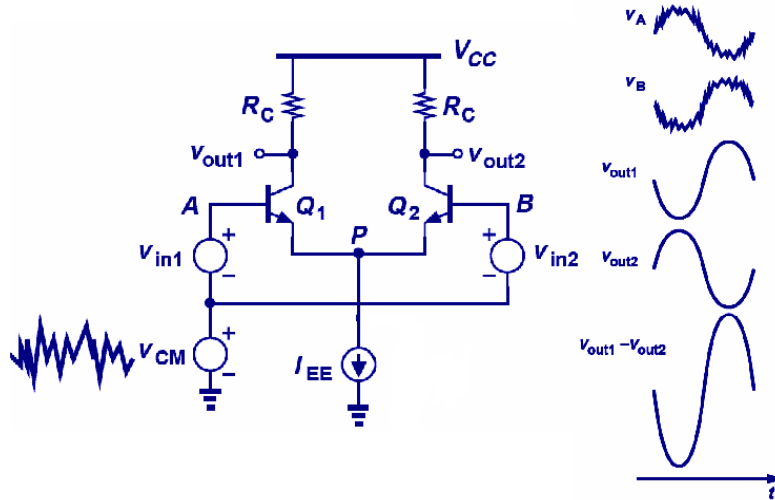
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Effect of Input CM Noise Ideal Tail Current

- There is no effect of the input CM noise at the output.



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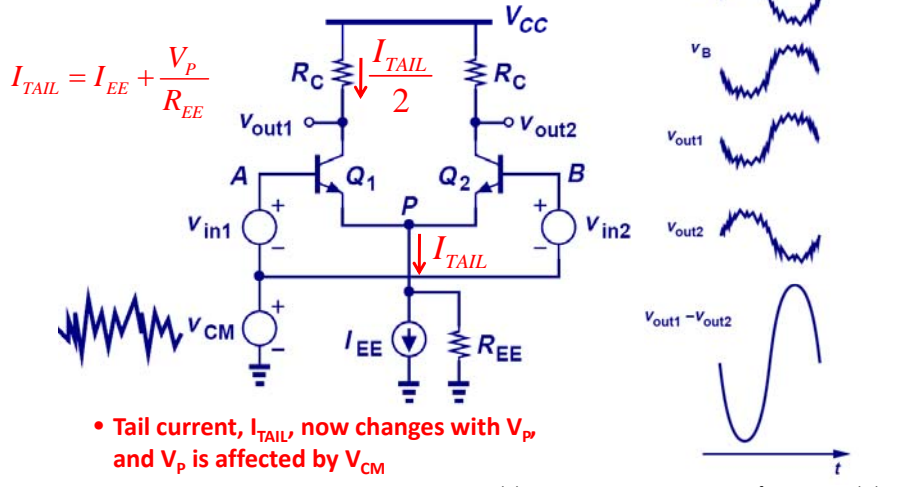
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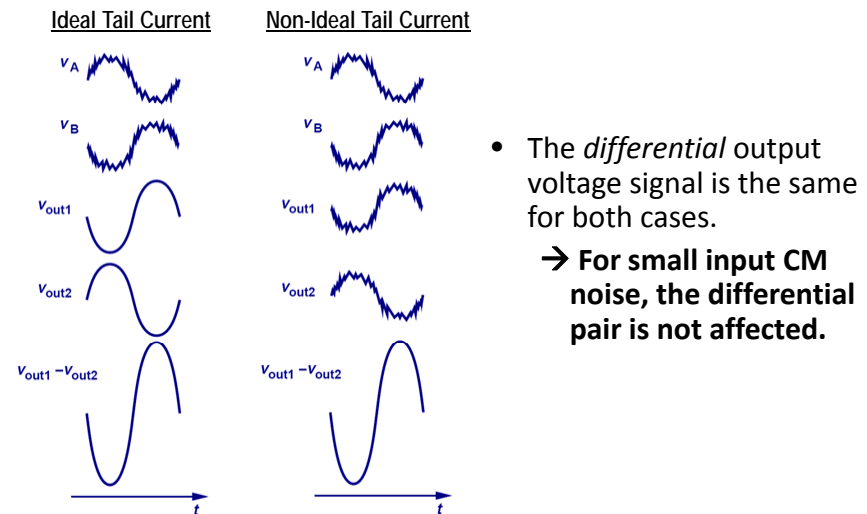
Effect of Input CM Noise

Non-Ideal Tail Current

- The single-ended outputs are corrupted by the input CM noise.



Comparison

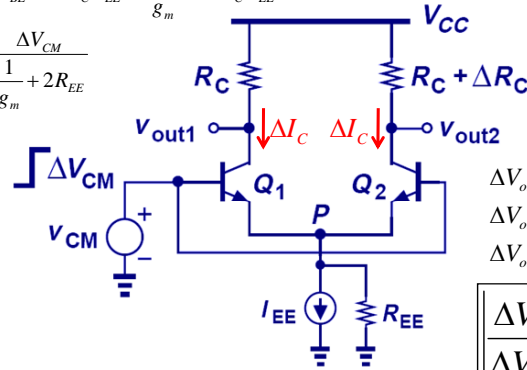


CM to DM Conversion; gain A_{CM-DM}

- If finite tail impedance and asymmetry (e.g. in load resistance) are *both* present, then the differential output signal *will* contain a portion of the input common-mode signal.

$$\Delta V_{CM} = \Delta V_{BE} + 2\Delta I_C R_{EE} = \frac{\Delta I_C}{g_m} + 2\Delta I_C R_{EE}$$

$$\Rightarrow \Delta I_C = \frac{\Delta V_{CM}}{\frac{1}{g_m} + 2R_{EE}}$$



$$\Delta V_{out1} = -\Delta I_C R_C$$

$$\Delta V_{out2} = -\Delta I_C (R_C + \Delta R_C)$$

$$\Delta V_{out} = \Delta V_{out1} - \Delta V_{out2} = -\Delta I_C \Delta R_C$$

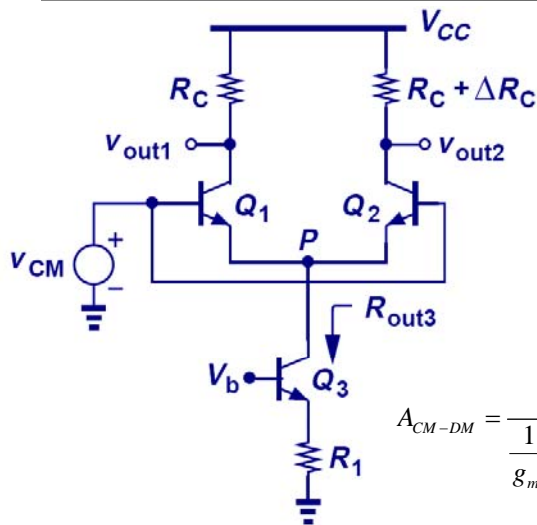
$$\frac{\Delta V_{out}}{\Delta V_{CM}} = \frac{\Delta R_C}{\left(\frac{1}{g_m}\right) + 2R_{EE}}$$

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Example



$$A_{CM-DM} = \frac{\Delta R_C}{\frac{1}{g_{m1}} + 2\{[1 + g_{m3}(R_1 \parallel r_{\pi 3})]r_{o3} + R_1 \parallel r_{\pi 3}\}}$$

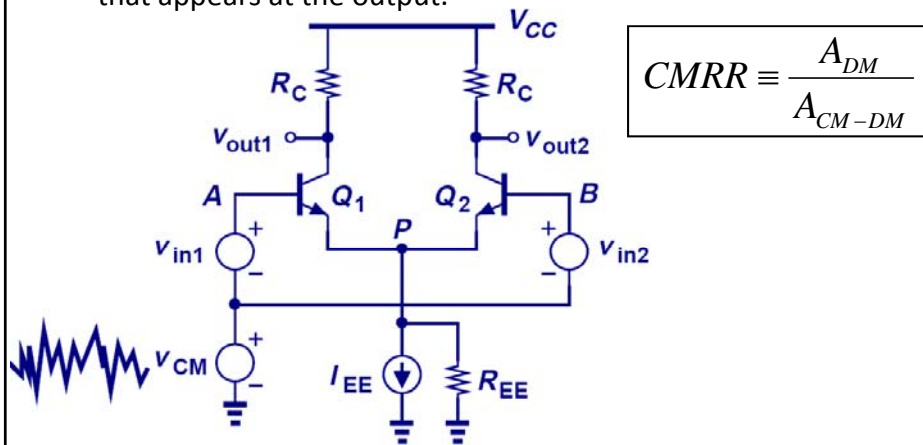
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Common-Mode Rejection Ratio

- CMRR is the ratio of the wanted amplified differential input signal to the unwanted converted input common-mode noise that appears at the output.



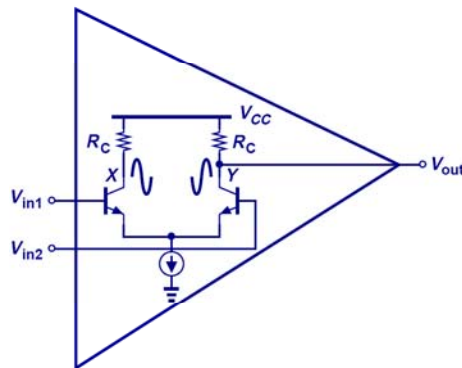
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Differential to Single-Ended Conversion

- Many circuits require a differential to single-ended conversion.



- This topology is not very good; its most critical drawback is supply noise corruption, since no common-mode cancellation mechanism exists. Also, we lose half of the voltage signal.

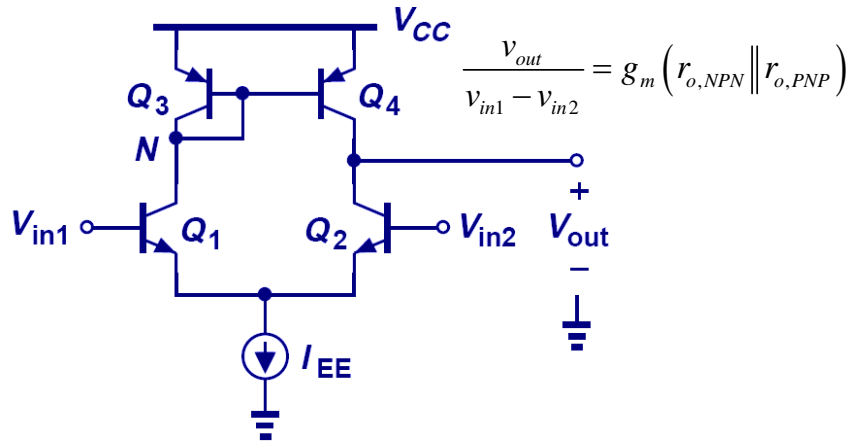
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... A Better Alternative

- This circuit topology performs differential to single-ended conversion with no loss of gain.



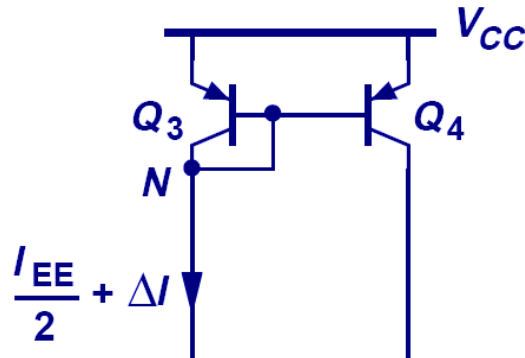
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Active Load

- With a current mirror as the load, the signal current produced by Q_1 can be replicated onto Q_4 .
- This type of load is different from the conventional "static load" and is called an "active load."



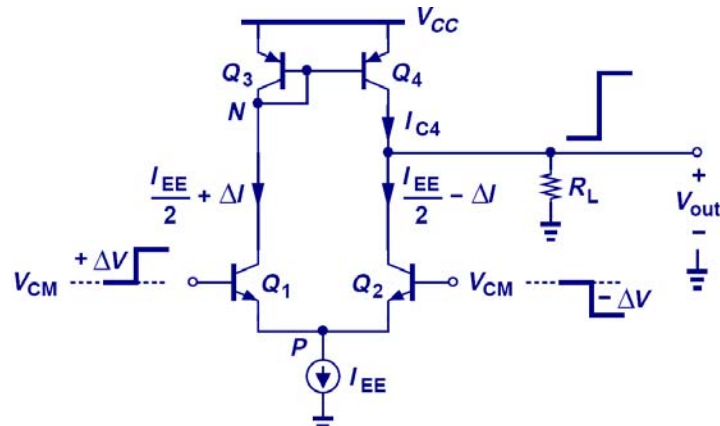
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Differential Pair with Active Load

- The input differential pair decreases the current drawn from R_L by ΔI , and the active load pushes an extra ΔI into R_L by current mirror action; these effects enhance each other.



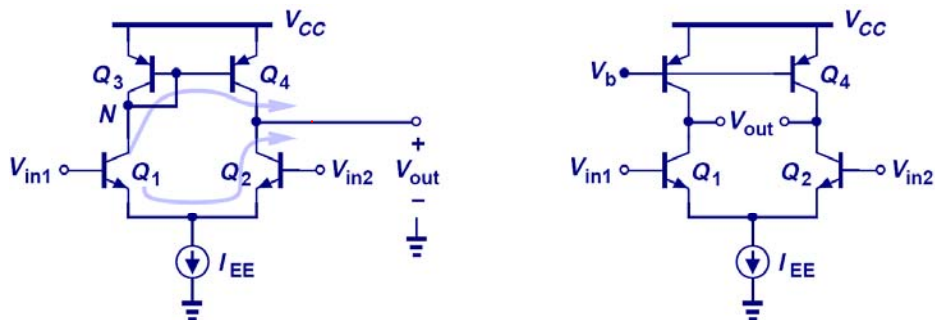
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Active Load vs. Static Load

- The load in the circuit on the left responds to the input signal and enhances the single-ended output, whereas the load in the circuit on the right does not.



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