

Lecture #12

OUTLINE

- pn Junctions
 - narrow-base diode
 - charge-control model

Reading: Finish Chapter 6

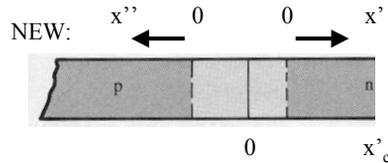
Carrier Concentration Profiles

Narrow or Short-Base Diode

- We have the following boundary conditions:

$$\Delta p_n(x_n) = p_{n0}(e^{qV_A/kT} - 1) \quad \Delta p_n(x' = x'_c) \rightarrow 0$$

- With the following coordinate system:



- Then, the solution is of the form:

$$\Delta p(x) = A_1 e^{x'/L_p} + A_2 e^{-x'/L_p}$$

Applying the boundary conditions, we have:

$$\Delta p_n(0) = A_1 + A_2$$

$$0 = A_1 e^{x'_c/L_p} + A_2 e^{-x'_c/L_p}$$

- So, we have:

$$\Delta p_n(x') = p_{n0}(e^{qV_A/kT} - 1) \left(\frac{e^{(x'_c - x')/L_p} - e^{-(x'_c - x')/L_p}}{e^{x'_c/L_p} - e^{-x'_c/L_p}} \right), \quad 0 < x' < x'_c$$

- Note: $\sinh(\xi) = \frac{e^\xi - e^{-\xi}}{2}$

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- So:

$$\Delta p_n(x') = p_{n0} (e^{qV_A/kT} - 1) \left(\frac{\sinh[(x'_c - x')/L_P]}{\sinh[x'_c/L_P]} \right), \quad 0 < x' < x'_c$$

- If we write:

$$I = I_0' (e^{qV_A/kT} - 1)$$

- Then

$$I_0' = qA \frac{D_p}{L_p} \frac{n_i^2}{N_D} \frac{\cosh(x'_c/L_p)}{\sinh(x'_c/L_p)}$$

where $\cosh(\xi) = \frac{e^\xi + e^{-\xi}}{2}$

Note: $\sinh(\xi) \rightarrow \xi$ as $\xi \rightarrow 0$ and $\cosh(\xi) \rightarrow 1 + \xi^2$ as $\xi \rightarrow 0$

- **If $x'_c \ll L_p$:**

Narrow Base Diode: I-V Equation

Let $W_N \equiv$ width of n - type region

$W_P \equiv$ width of p - type region

and $W'_N \equiv W_N - x_n \ll L_P$

$W'_P \equiv W_P - x_p \ll L_N$

$$\text{Then, } J = qn_i^2 \left[\frac{D_P}{W'_N N_D} + \frac{D_N}{W'_P N_A} \right] (e^{qV_A/kT} - 1)$$

$$I = qAn_i^2 \left[\frac{D_P}{W'_N N_D} + \frac{D_N}{W'_P N_A} \right] (e^{qV_A/kT} - 1) = I_0 (e^{qV_A/kT} - 1)$$

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Current Flow in a One-Sided pn Junction

- Note that the diode current is dominated by the term associated with the more lightly doped side:

$$\text{p}^+\text{n diode: } I_0 \equiv I_p(x_n) = \begin{cases} qAn_i^2 \left(\frac{D_P}{L_P N_D} \right) & \text{long n - side} \\ qAn_i^2 \left(\frac{D_P}{W'_N N_D} \right) & \text{short n - side} \end{cases}$$

$$\text{pn}^+ \text{ diode: } I_0 \equiv I_N(-x_p) = \begin{cases} qAn_i^2 \left(\frac{D_N}{L_N N_A} \right) & \text{long p - side} \\ qAn_i^2 \left(\frac{D_N}{W'_P N_A} \right) & \text{short p - side} \end{cases}$$

i.e. current flowing across junction is dominated by carriers injected from the more heavily doped side

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Excess Carrier Profiles: Limiting Cases

Long base ($x_c' \rightarrow \infty$):

$$\begin{aligned}\Delta p_n(x') &= p_{n0}(e^{qV_A/kT} - 1) \left(\frac{e^{(x_c' - x')/L_p} - e^{-(x_c' - x')/L_p}}{e^{x_c'/L_p} - e^{-x_c'/L_p}} \right) \\ &= p_{n0}(e^{qV_A/kT} - 1) \left(\frac{e^{x_c'/L_p} e^{-x'/L_p} - e^{-x_c'/L_p} e^{x'/L_p}}{e^{x_c'/L_p} - e^{-x_c'/L_p}} \right) \\ &\cong p_{n0}(e^{qV_A/kT} - 1) e^{-x'/L_p}\end{aligned}$$

2. Short base ($x_c' \rightarrow 0$):

$$\begin{aligned}\Delta p_n(x') &= p_{n0}(e^{qV_A/kT} - 1) \left(\frac{\sinh[(x_c' - x')/L_p]}{\sinh[x_c'/L_p]} \right) \\ &= p_{n0}(e^{qV_A/kT} - 1) \left(\frac{(x_c' - x')/L_p}{x_c'/L_p} \right) = p_{n0}(e^{qV_A/kT} - 1) \left(1 - \frac{x'}{x_c'} \right)\end{aligned}$$

Δp_n is a linear function of x

$\rightarrow J_p$ is constant (no recombination)

Minority-Carrier Charge Storage

- When $V_A > 0$, excess minority carriers are stored in the quasi-neutral regions of a pn junction:

$$\begin{aligned}
 Q_N &= -qA \int_{-x_p}^{-\infty} \Delta n_p(x) dx & Q_P &= qA \int_{x_n}^{\infty} \Delta p_n(x) dx \\
 &= -qA \Delta n_p(-x_p) L_N & &= qA \Delta p_n(x_n) L_P
 \end{aligned}$$

Derivation of Charge Control Model

- Consider a forward-biased pn junction. The total excess hole charge in the n quasi-neutral region is:

$$Q_p = qA \int_{x_n}^{\infty} \Delta p_n(x, t) dx$$

- The minority carrier diffusion equation is (without G_L):

$$\frac{\partial \Delta p_n}{\partial t} = D_p \frac{\partial^2 \Delta p_n}{\partial x^2} - \frac{\Delta p_n}{\tau_p}$$

- Since the electric field is very small,

$$J_p = -qD_p \frac{\partial \Delta p_n}{\partial x}$$

- Therefore: $\frac{\partial(q\Delta p_n)}{\partial t} = -\frac{\partial J_p}{\partial x} - \frac{q\Delta p_n}{\tau_p}$

(Long Base Diode)

- Integrating over the n quasi-neutral region:

$$\frac{\partial}{\partial t} \left[qA \int_{x_n}^{\infty} \Delta p_n dx \right] = -A \int_{J_p(x_n)}^{J_p(\infty)} dJ_p - \frac{1}{\tau_p} \left[qA \int_{x_n}^{\infty} \Delta p_n dx \right]$$

- Furthermore, in a p+n junction:

$$-A \int_{J_p(x_n)}^{J_p(\infty)} dJ_p = -AJ_p(\infty) + AJ_p(x_n) = AJ_p(x_n) \cong i_{DIFF}$$

- So: $\frac{dQ_p}{dt} = i_{DIFF} - \frac{Q_p}{\tau_p}$

Charge Control Model

We can calculate pn-junction current in 2 ways:

- From slopes of $\Delta n_p(-x_p)$ and $\Delta p_n(x_n)$
- From steady-state charges Q_N , Q_P stored in each excess-minority-charge distribution:

$$\frac{dQ_p}{dt} = AJ_p(x_n) - \frac{Q_p}{\tau_p} = 0$$

$$\Rightarrow AJ_p(x_n) = I_p(x_n) = \frac{Q_p}{\tau_p}$$

$$\text{Similarly, } I_n(-x_p) = \frac{-Q_n}{\tau_n}$$

Charge Control Model for Narrow Base

- For a narrow-base diode, replace τ_p and/or τ_n by the **minority-carrier transit time** τ_{tr}
 - time required for minority carrier to travel across the quasi-neutral region

- For holes on narrow n-side:

$$Q_p = qA \int_{x_n}^{W_N} \Delta p_n(x) dx = qA \frac{1}{2} \Delta p_n(x_n) W'_N$$

$$I_p = AJ_p = -qAD_p \frac{d\Delta p_n}{dx} = qAD_p \frac{\Delta p_n(x_n)}{W'_N}$$

$$\Rightarrow \tau_{tr} = \frac{Q_p}{I_p} = \frac{(W'_N)^2}{2D_p}$$

- Similarly, for electrons on narrow p-side: $\tau_{tr} = \frac{(W'_p)^2}{2D_N}$

Summary: Narrow (Short) Base Diode

- If the width of the quasi-neutral region (e.g. x'_c) is **not** much larger than the minority-carrier diffusion length (e.g. L_p), then the solution to the minority-carrier diffusion equation is

$$\Delta p_n(x') = \Delta p_n(x_n) \frac{\sinh\left(\frac{x'_c - x}{L_p}\right)}{\sinh\left(\frac{x'_c}{L_p}\right)}$$

- If $x'_c < 0.1L_p$:

$$\Delta p_n(x') \cong \Delta p_n(x_n) \left(1 - \frac{x'}{x'_c}\right)$$

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- If $L_p \gg x_c'$, negligible recombination occurs
⇒ hole current is constant throughout n-type region

$$J_p = -qD_p \frac{d\Delta p_n}{dx} = qD_p \frac{n_i^2}{N_D} \left(e^{qV_A/kT} - 1 \right) \left(\frac{1}{x_c'} \right)$$

- Compare this to the hole current contribution in the long-base diode:

$$J_p = qD_p \frac{n_i^2}{N_D} \left(e^{qV_A/kT} - 1 \right) \left(\frac{1}{L_p} \right)$$