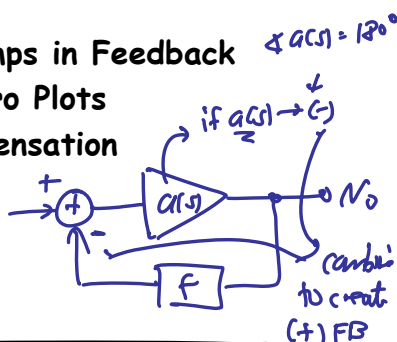


• **Announcements:**

- Evening lecture today, 7 p.m., in 289 Cory
- You should be finished with a draft design of your op amp project by now

• **Today:**

- Stability of Op Amps in Feedback
- Review of Pole/Zero Plots
- Methods for Compensation
 - Narrowbanding
 - Pole-Splitting



Last Time -

Stability of FB Ckt. Using a Single Pole Op Amp

For a single pole op amp: $a(s) = \frac{a_0}{1 - \frac{s}{p_1}}$ op amp transfer function

Thur: closed loop Xfa Fcn

$$A(s) = \frac{a(s)}{1 + a(s)f} = \frac{a_0}{1 + a_0 f} \cdot \frac{1}{1 - \frac{s}{p_1(1 + a_0 f)}}$$

↑
much high 3dB freq.

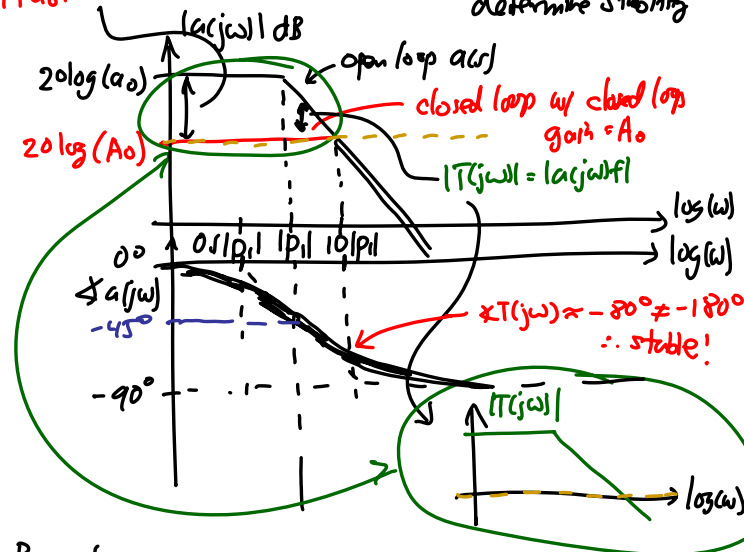
$A_0 =$ closed loop dc gain $\rightarrow (1 + a_0 f) \approx a_0 f \times$ smaller than a_0
 $= \frac{1}{f}$

$T_0 = a_0 f =$ loop gain (defined at dc)

$T(s) = a(s)f =$ loop transmission (defined for general frequencies)

Bode Plot: \rightarrow use to determine

$(1 + a_0 f) \approx a_0 f$ & $a(s)f$ when $|a(s)f| = 1 \leftarrow$ then can determine stability

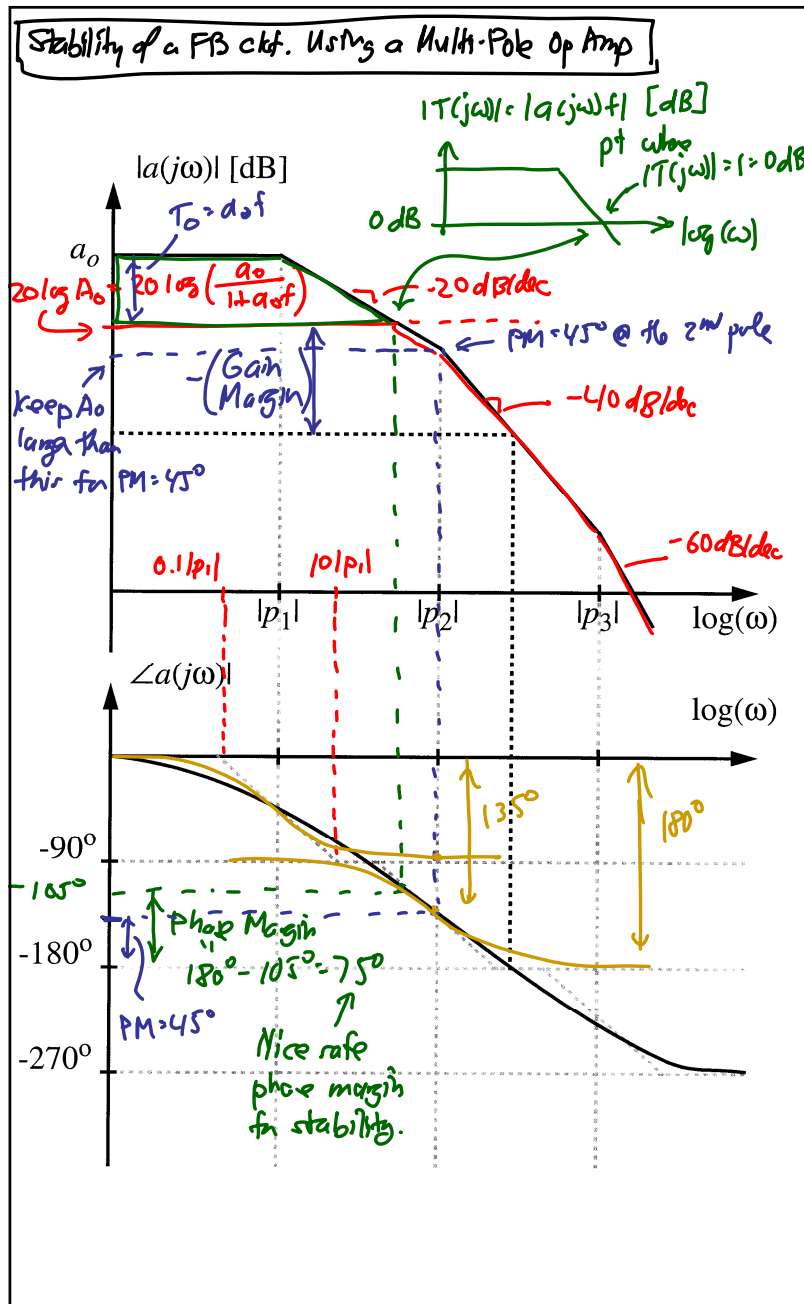


Remarks:

- ① For the case of a single pole op amp, FB can never reach $\angle T(j\omega) = -180^\circ$! (90° is the limit!)
- ② Thus, an op amp FB ckt. w/ $f = \text{const.}$ and using a single-pole op amp is always stable!

↓
But add a few non-dominant poles \rightarrow then instability is possible!

Since now, $\angle T(j\omega)$ can reach -180° !
 \rightarrow Can best visualize this via a Bode plot.



For the more general case where $a(s)$ has multiple poles
 $\Rightarrow A(s)$ has the same additional poles
 \Rightarrow i.e., @ freqs. $> |p_1|(1+a_0f)$, the $A(s)$ curve just follows the $a(s)$ curve

$$A(s) \cong \frac{A_0}{(1 - \frac{s}{p_1(1+a_0f)})(1 - \frac{s}{p_2})(1 - \frac{s}{p_3})}$$

makes sense, because @ freqs. $> |p_1|(1+a_0f)$, the loop transmission $|T(j\omega)| < 1 \rightarrow \therefore$ there isn't really much FB anymore...

Definition.

Phase Margin = $180^\circ + (\angle T(j\omega) \text{ @ the freq. where } |T(j\omega)|=1)$

\Rightarrow Phase Margin must be $> 0^\circ$ for stability

For stability: $\text{Phase Margin} > 0^\circ$

\Rightarrow For safety, though, usually design for

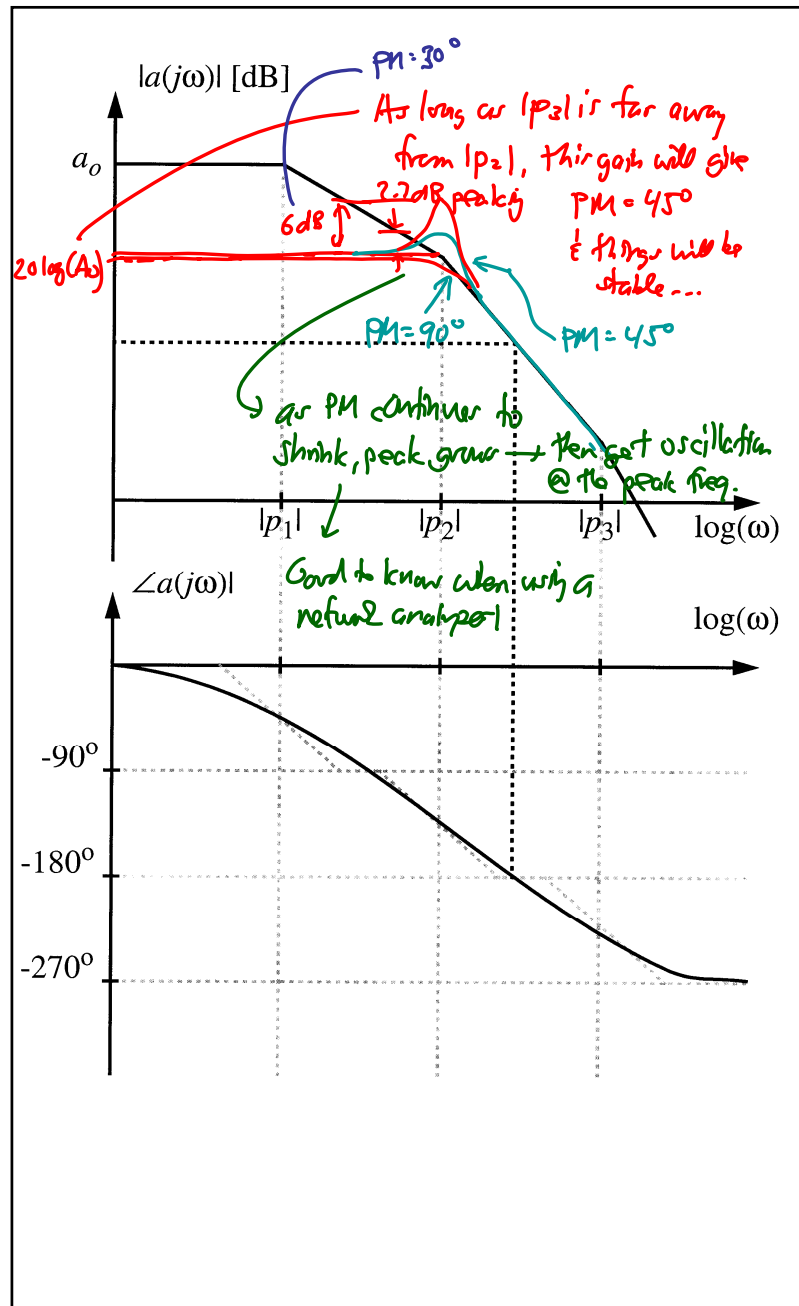
$\text{Phase Margin} \geq 45^\circ$

Design Criterion
(for practical design)

Definition.

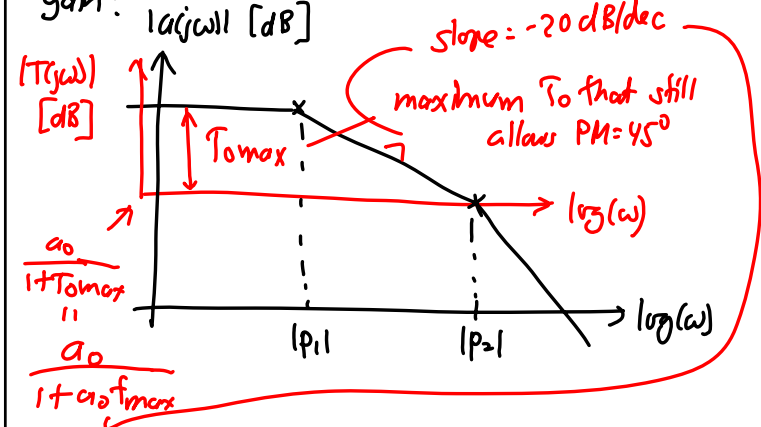
Gain Margin $\equiv |T(j\omega)|$ in dB @ freq. where $\angle T(j\omega) = -180^\circ$

For stability: $\text{Gain Margin} < 0 \text{ dB}$



Compensation of Op Amps I

To compensate, need the distance between p_1 & p_2 to be large enough to encompass the largest desired loop gain!



$$20 (\log |p_2| - \log |p_1|) = 20 \log (T_{0max})$$

$$\frac{|p_2|}{|p_1|} = T_{0max} \rightarrow |p_2| = |p_1| T_{0max}$$

largest desired (expected) loop gain

provided $|p_3| \gg |p_2|$

Need for stability w/ PM = 45° @ all desired closed loop gains

Two Ways to Compensate:

- ① Narrowbanding
- ② Pole-splitting

Basically, there is a minimum separation between p_1 & p_2 that insures stability.

