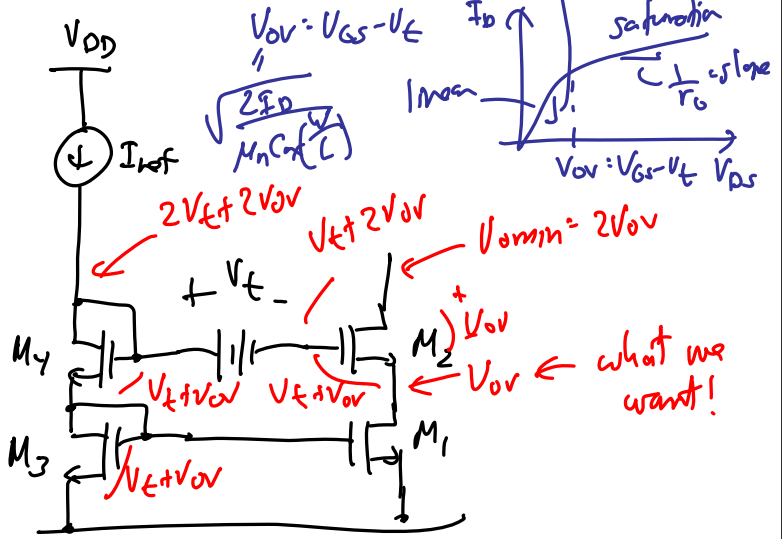


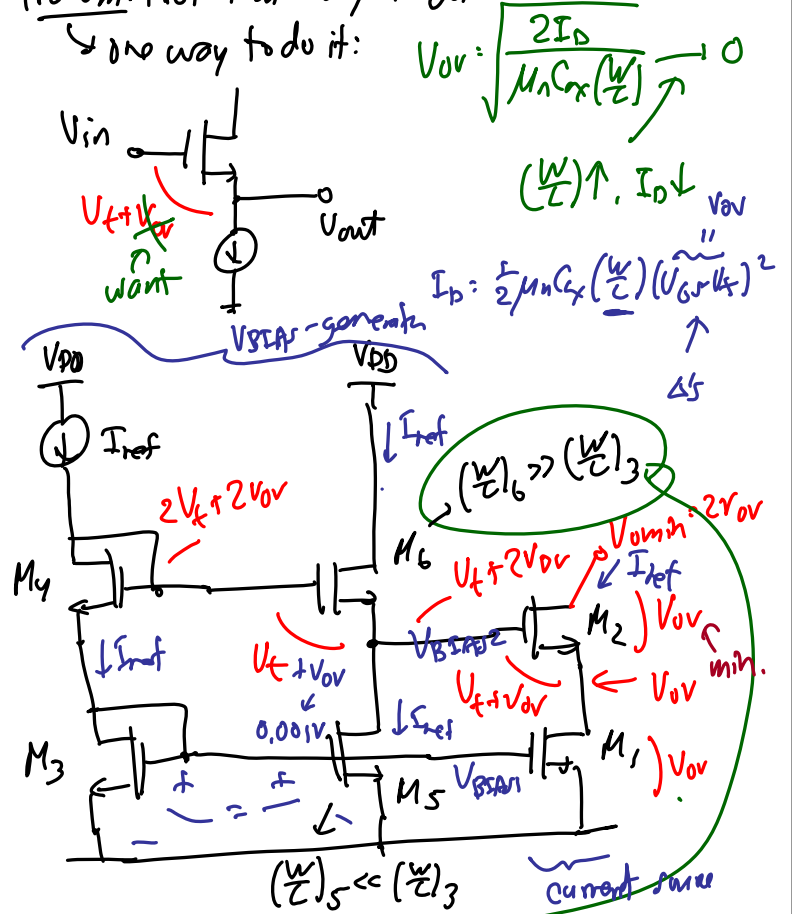
Lecture 10: High Swing Current Sources II

- **Announcements:**
  - ↳ This is the make-up lecture for yesterday's lecture
  - ↳ Reminder: Lab#2 starts next week
  - ↳ No Monday lab section next week due to holiday
  - ↳ Monday lab sections will start Lab#2 Monday the week after next
- **Lecture Topics:**
  - ↳ High Swing Current Sources (cont.)
  - ↳ Current Source Matching Considerations
  - ↳ Op Amp Review

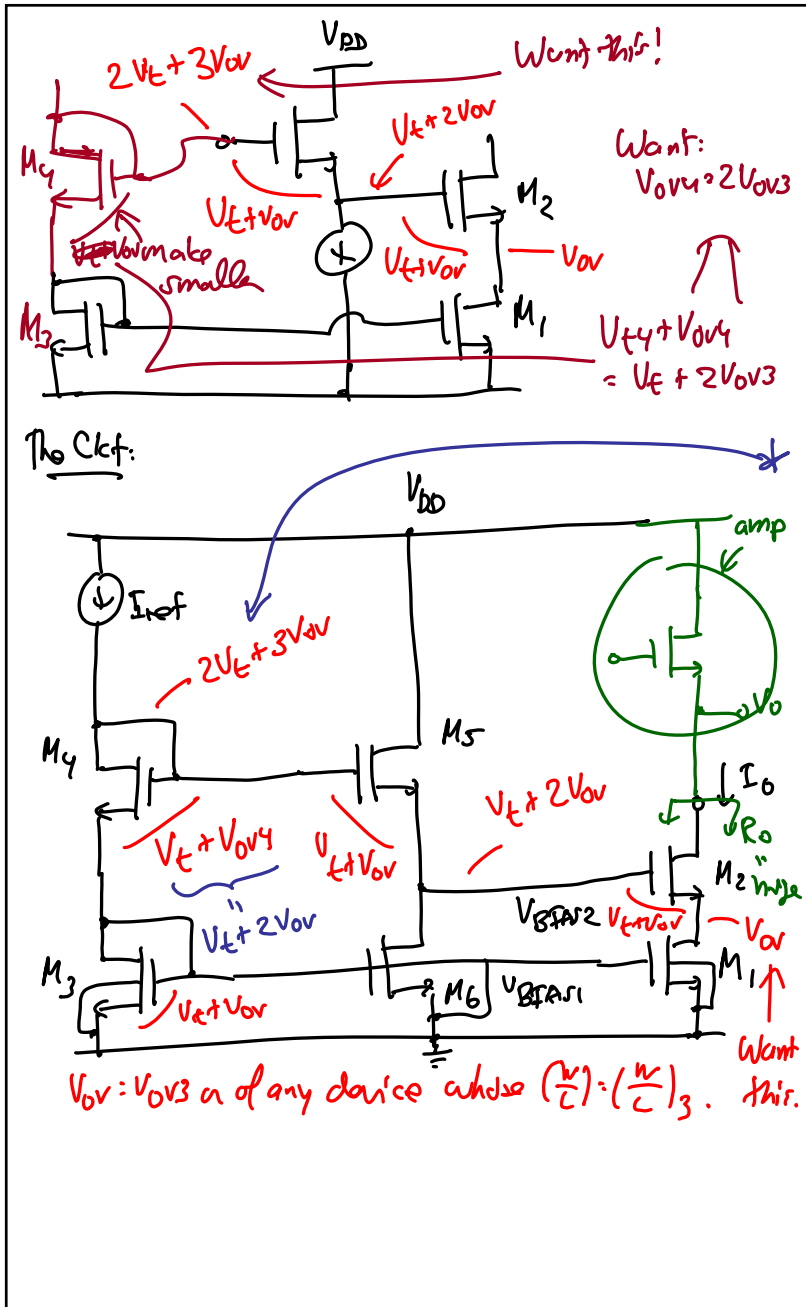
- **Last Time:**
- Looking for current sources that maximize the output swing available for an amplifier



Problem! Not that easy to get an exact level shift.  
 ↳ no way to do it:



Problem: Don't like this.  
 ↳  $(\frac{W}{L})_6$  must be big to send  $V_{ov} = 0!$   
 ↳ if not  $\rightarrow V_{ov1} < V_{ov1}$   
 ↳ linear!  $\rightarrow$  Bad!  
 Another Option: just accept a  $V_t + V_{ov}$  level shift.



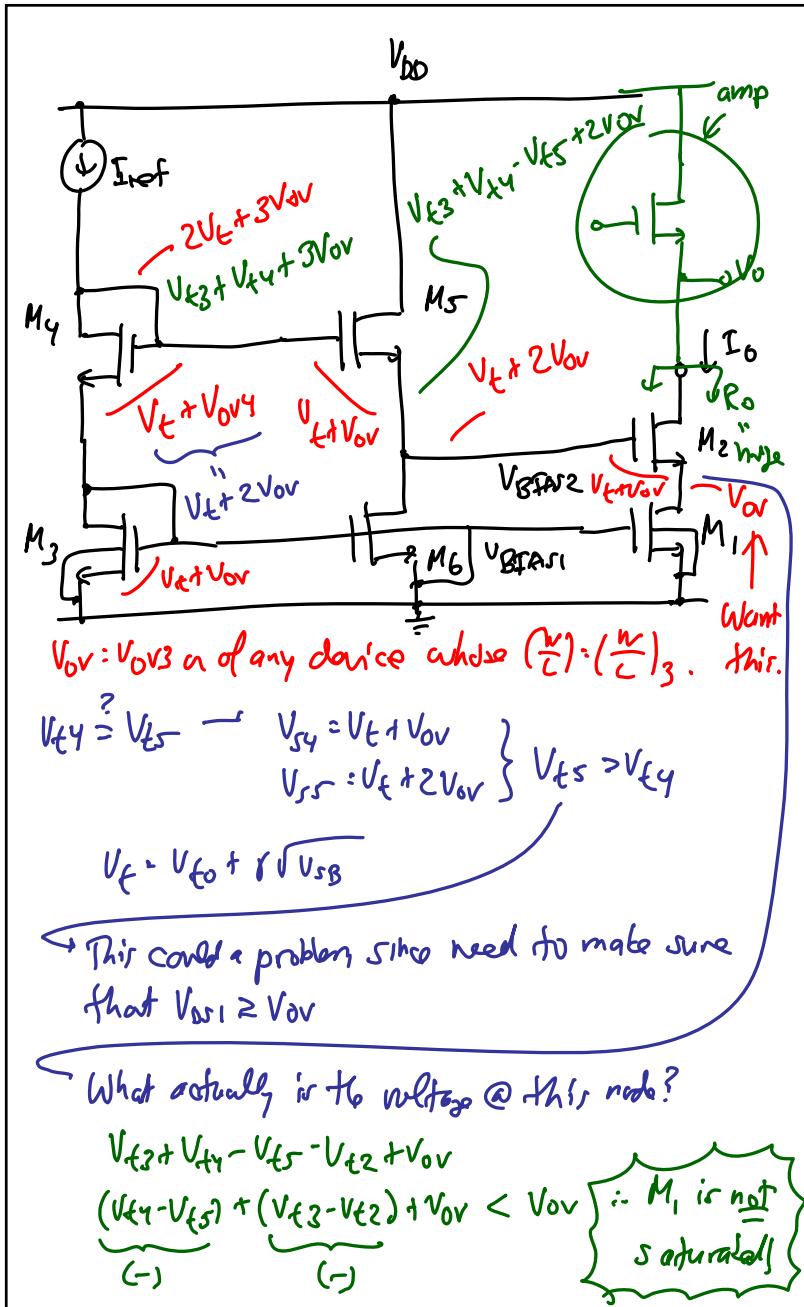
$$I_{D3} = \frac{1}{2} \mu_n C_{ox} \left(\frac{w}{L}\right)_3 (V_{ov3})^2$$

$$I_{D4} = \frac{1}{2} \mu_n C_{ox} \left(\frac{w}{L}\right)_4 (2V_{ov3})^2$$

$$I_{D3} = I_{D4} = I_{ref}$$

$$\frac{1}{2} \mu_n C_{ox} \left(\frac{w}{L}\right)_3 (V_{ov3})^2 = \frac{1}{2} \mu_n C_{ox} \left(\frac{w}{L}\right)_4 (2V_{ov3})^2$$

$$\left(\frac{w}{L}\right)_4 = \frac{1}{4} \left(\frac{w}{L}\right)_3 \leftarrow \text{ignores Body Effect}$$
 ... and  $\left(\frac{w}{L}\right)_1 = \left(\frac{w}{L}\right)_2 = \left(\frac{w}{L}\right)_3 = \left(\frac{w}{L}\right)_5 = \left(\frac{w}{L}\right)_6$ 
 Problem: Body effect in  $M_4, M_5, M_2$   
 ↳ will increase their  $V_t$ 's!



$V_{s3} = 0V$   
 $V_{s2} = V_{ov}$  }  $V_{t3} < V_{t2}$

Big Problem!  
 $V_{t3} + V_{t4} - V_{t5} - V_{t2} + V_{ov}$   
 $(V_{t4} - V_{t5}) + (V_{t3} - V_{t2}) + V_{ov} < V_{ov} \therefore M_1 \text{ is not saturated!}$

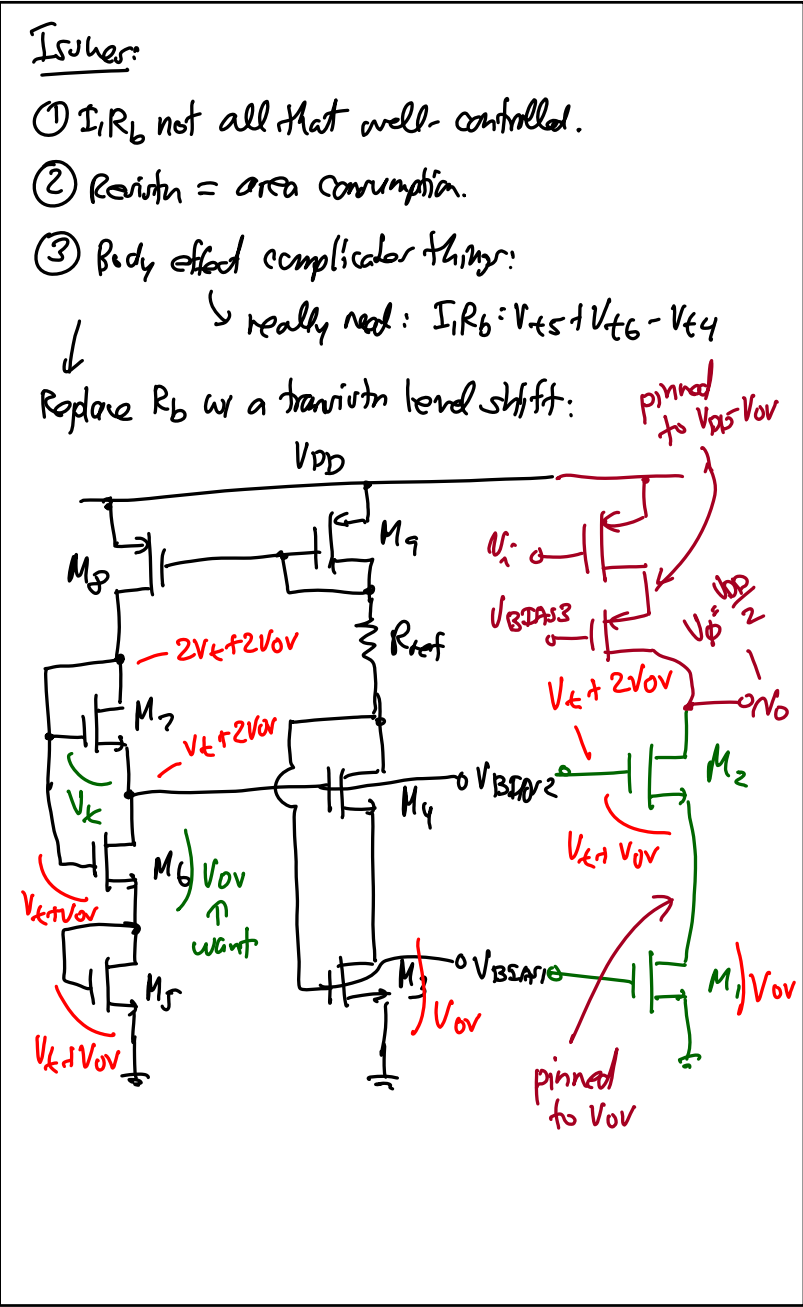
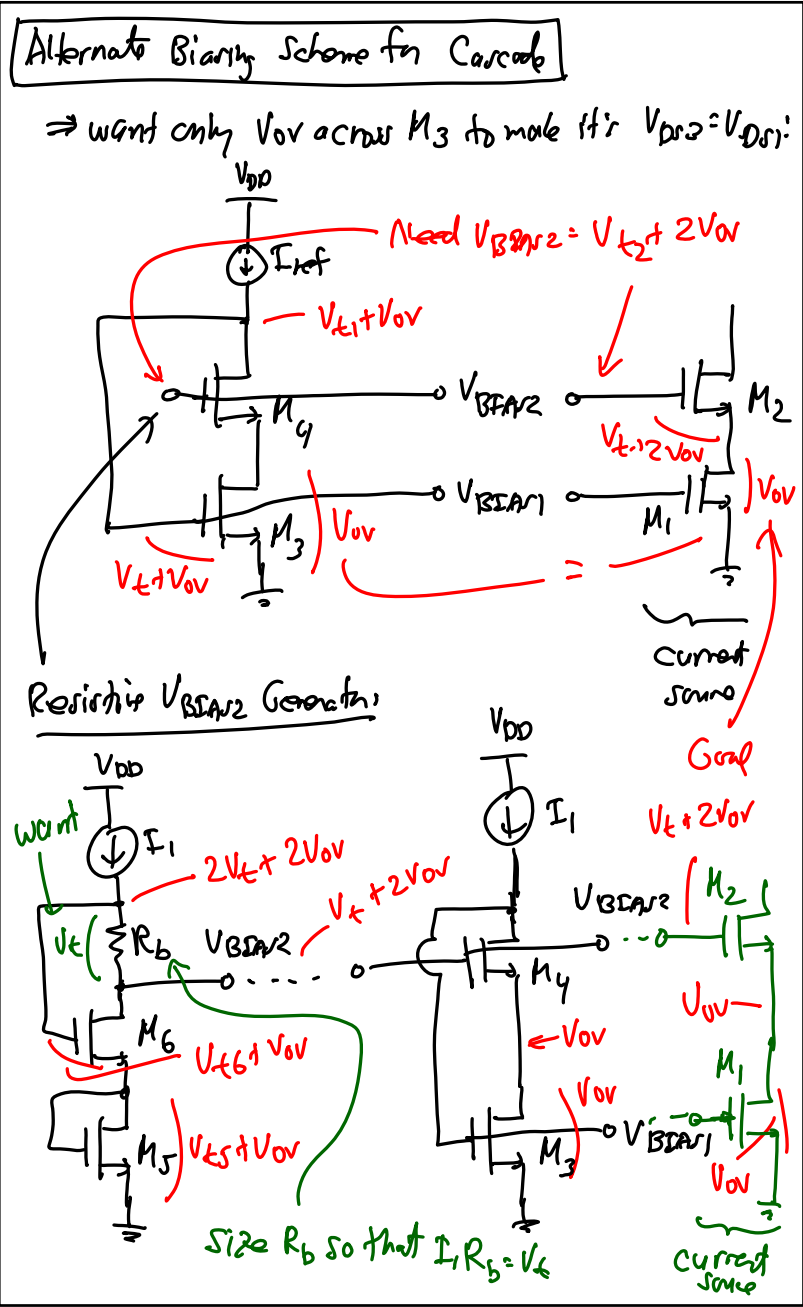
linear!  $\rightarrow v_o = \text{small}$   
 $r_o = \text{small} \rightarrow \text{bad current source!}$

Solutions:

- ① Tie the wells of  $M_4, M_5, M_2$  to their sources.
- ② Bias  $M_4$  so that  $V_{GS4} \geq V_t + 2V_{ov}$   
 e.g.,  $V_{GS4} = V_t + 3V_{ov}$

$(\frac{w}{l})_4 = \frac{1}{9} (\frac{w}{l})_3$  ← Safety margin against Body effect

Issue:  $I_D = \frac{1}{2} \mu_n C_{ox} (\frac{w}{l}) (V_{GS} - V_t)^2 (1 + \lambda V_{DS})$   
 IF  $V_{DS1} \neq V_{DS3}$   $\uparrow$  as channel length  $\downarrow$   
 $I_D = \frac{(1 + \lambda V_{DS1})}{(1 + \lambda V_{DS3})} I_{ref} \rightarrow I_D \neq I_{ref}$   
 Solution: Use alternate biasing scheme.



Design:

Approach 1: Want  $V_{GS} = V_t$ , so must make  $(\frac{W}{L})_2$  large,

so that:

$$V_{OV2} = \sqrt{\frac{2I_D}{\mu_n C_{ox} (\frac{W}{L})_2}} \rightarrow 0, \text{ then}$$

↓  
Solution → Problem: too much chip area!

Approach 2: → recognize that devices in the  $V_{BIAS}$ -generation don't all need to be saturated → some can be linear!