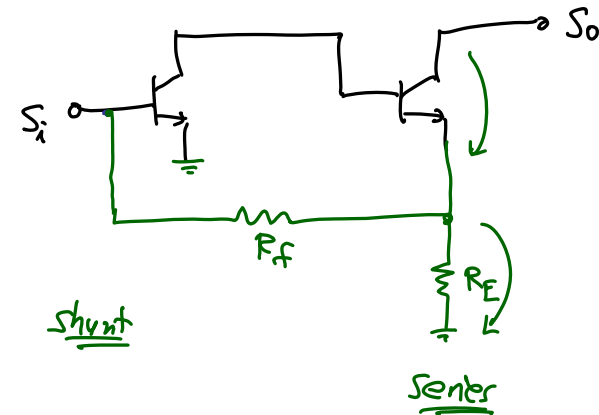
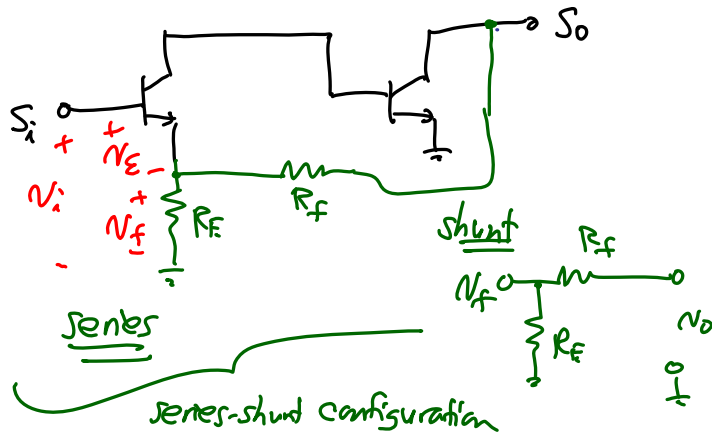


Lecture 26w: Feedback Z and Loading

- Announcements:
- This lecture will be 2 hours (2nd lecture to make up for missing Thursday)
- Video of last half hour will be posted
- HW#12 online and due Tuesday, next week
- Lab#3 (your project) due on Friday, May 10, at 5 p.m. in the EE140/240A Homework Box
- Passed out Feedback Inspection Handout
- Pre-Lecture on Feedback Loading online
- Lecture Topics:
 - ↳ Effect of FB on Z_i and Z_o
 - ↳ Feedback Loading
 - ↳ Open-Loop Amp w/ Feedback Loading
 - ↳ Feedback By Inspection
- -----
- Last Time:
- Recognizing feedback configurations



Feedback Configurations

<u>Input</u>		<u>Output</u>	
<u>Variable</u>	<u>Connection</u>	<u>Connection</u>	<u>Variable</u>
(21) voltage	series	series	current (21)
(22) current	shunt	shunt	voltage (22)

Effect of FB on Z_i & Z_o

Ex. Series-Shunt FB

Assumption: FB network has ideal impedances
i.e., it does not load the basic amplifier

Basic Amplifier: $V_E \rightarrow V_O$

Feedback Network

Find the T.F. -

$$\left. \begin{aligned} V_O &= A_N V_E \\ V_E &= V_i - V_{fb} \\ V_{fb} &= fV_O \end{aligned} \right\} \Rightarrow \frac{V_O}{V_i} = \frac{A_N}{1 + A_N f} \quad (\text{as expected})$$

loop gain

Find Z_i : $\frac{V_x}{i_x}$

$$V_x = V_E + V_{fb}$$

$$= V_E + fV_O = V_E + A_N f V_E = V_E (1 + A_N f)$$

$$i_x = \frac{V_E}{Z_{i_a}}$$

$$Z_i = \frac{V_x}{i_x} = \frac{V_E (1 + A_N f)}{\frac{V_E}{Z_{i_a}}} = Z_{i_a} (1 + A_N f) = Z_i'$$

loop gain

\therefore when use series connection @ input

Input impedance raised by $(1 + A_N f)$!

makes for a better voltage amplifier!

Find Z_o : $\frac{V_x'}{i_x'}$ (w/ input shunted)

$$V_E + V_{fb} = 0 = V_E + fV_x' \rightarrow V_E = -fV_x' \quad \text{shunt}$$

$$i_x' = \frac{V_x' - A_N V_E}{Z_{o_a}} = \frac{V_x' + A_N f V_x'}{Z_{o_a}} = \frac{V_x'}{i_x'} \cdot \frac{Z_{o_a}}{1 + A_N f} = Z_o$$

loop gain

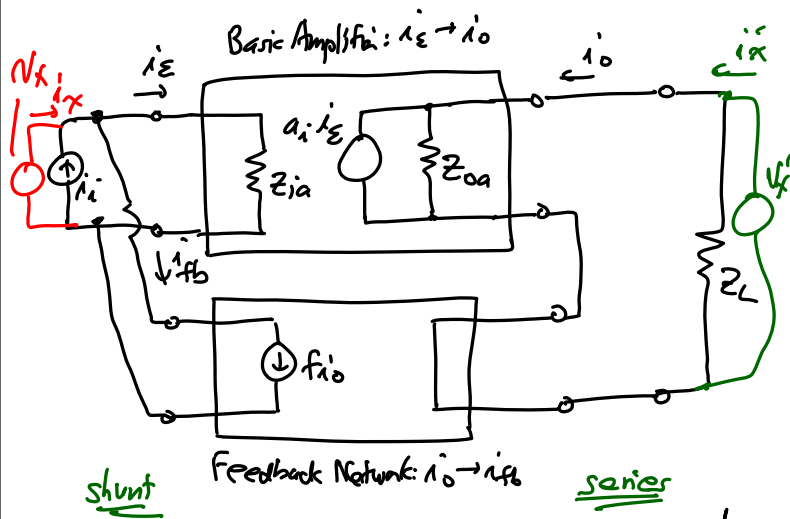
Output impedance lowered by a factor of $(1 + A_N f)$!

again, makes for a better voltage amplifier!

Overall, series-shunt FB improves the characteristics of a $v \rightarrow v$ amplifier: $z_i \uparrow, z_o \downarrow$ due to FB

Ex. Shunt-Series FB

\Rightarrow Again, assume the FB network does not load the amplifier



Find the T.F. -

$$i_o = a_i i_e$$

$$i_e = i_x - i_{fb} = i_x - f i_o$$

$$\frac{i_o}{i_x} = \frac{a_i}{1 + a_i f}$$

current gain

loop gain

This is a universal form.

Find $z_i = \frac{v_x}{i_x}$:

$$\frac{v_x}{i_x} = \frac{z_{ia}}{1 + a_i f} = z_i$$

loop gain

shunt

\Rightarrow Again, a shunt connection reduces the impedance by $(1 + a_i f)$!

Find $z_o = \frac{v_x}{i_x}$:

$$\frac{v_x}{i_x} = z_{oa}(1 + a_i f) = z_o$$

series connection raises the impedance by $(1 + a_i f)$!

everything together makes for a better $i \rightarrow i$ amplifier when using shunt-series FB!

Summary:

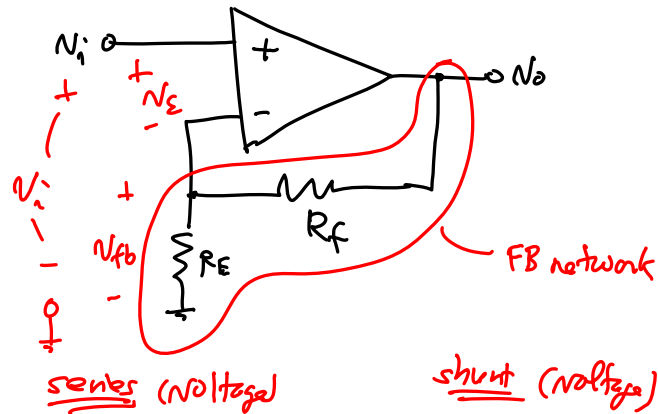
① series connection: $z \rightarrow z(1 + T)$

② shunt connection: $z \rightarrow \frac{z}{1 + T}$

$T = \text{loop gain}$

Determine the FB loading of an Amplifier

Example: Non-Inverting Amplifier



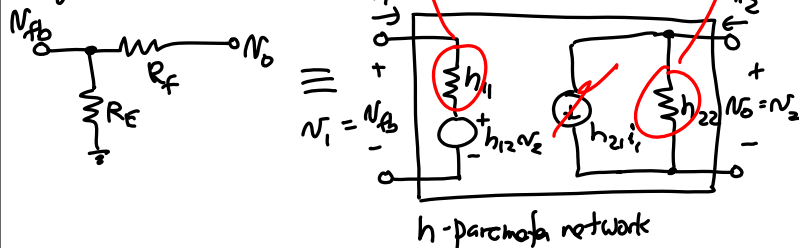
Objective: Use $A_o = \frac{a_v}{1 + a_v f}$ to get A_o .

In order to use this equation, we must know

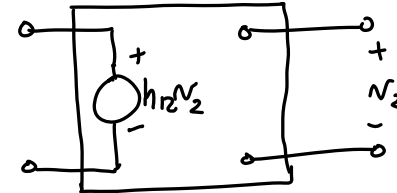
(i) $a_v \triangleq$ gain of the amplifier

(ii) $f \triangleq$ gain of the feedback (also, called the feedback factor)

In general:



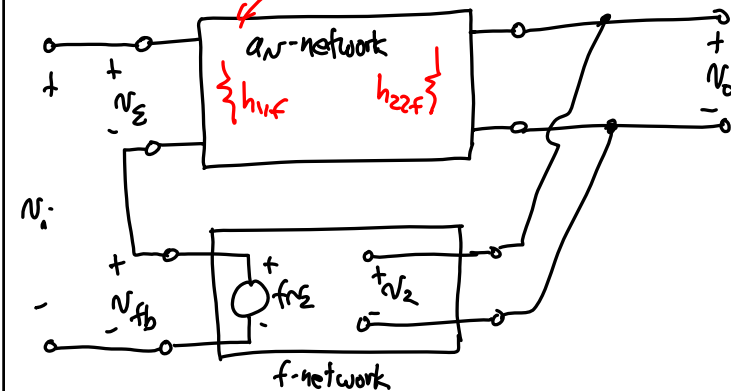
But to simplify things, we would like to be able to represent the feedback network by just:



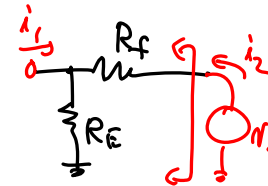
Where: ① The small h_{21} is neglected.

② All impedances have been moved out of the f-network and moved to the a_v -network.

Pictorially: open loop gain w FB loading



The FB Network: (find h-parameter representation)



h-parameter Network (just a reminder)

Port Equations:

$$V_1 = h_{11}i_1 + h_{12}V_2$$

$$i_2 = h_{21}i_1 + h_{22}V_2$$

Elements:

$$h_{11} = \left. \frac{V_1}{i_1} \right|_{V_2=0} \quad h_{12} = \left. \frac{V_1}{V_2} \right|_{i_1=0}$$

$$h_{21} = \left. \frac{i_2}{i_1} \right|_{V_2=0} \quad h_{22} = \left. \frac{i_2}{V_2} \right|_{i_1=0}$$

$h_{22f} = \left. \frac{i_2}{V_2} \right|_{i_1=0} = \frac{1}{R_E + R_F}$ ← This is the loading @ port 2, i.e., at the amplifier output port.

$f \cdot h_{12f} = \left. \frac{V_1}{V_2} \right|_{i_1=0} = \frac{R_E}{R_E + R_F} = f$

$h_{11f} = \left. \frac{V_1}{i_1} \right|_{V_2=0} = R_E \parallel R_F$ ← This is the loading @ port 1, i.e., the input port of the amplifier.

So we have:

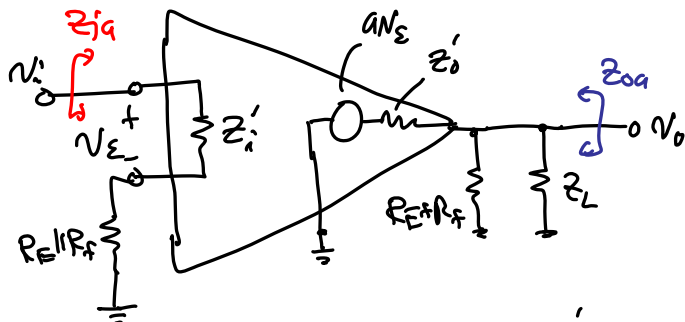
More R_i in feedback to the amplifier

Determine " A_{v_f} " from this.

Use the box in blue to determine " a_v "

in $A_o = \frac{a_v}{1+a_v f}$; $z_i = z_{ia}(1+a_v f)$...

Determine the " a_v " gain:



$$V_o = a_{vE} \left\{ \frac{(R_E + R_F) \parallel z_L}{(R_E + R_F) \parallel z_L + z_o'} \right\}; V_E = V_i \left(\frac{z_i'}{z_i' + R_E \parallel R_F} \right)$$

$$\therefore \left. \frac{V_o}{V_i} \right|_{FB \text{ loading}} = \left(\frac{z_i'}{z_i' + R_E \parallel R_F} \right) a \left(\frac{(R_E + R_F) \parallel z_L}{(R_E + R_F) \parallel z_L + z_o'} \right) = a_v$$

We have: $f = \frac{R_E}{R_E + R_F}$

Get closed loop gain A_o : \rightarrow for large a_v - if not large, use this

$$A_o = \frac{V_o}{V_i} = \frac{a_v}{1+a_v f} \approx \frac{1}{f} = 1 + \frac{R_F}{R_E}$$

What about R_i & R_o ?

\Rightarrow first, for the amplifier w/ FB loading:
open-loop

$$z_{ia} = z_i' + R_E \parallel R_F \rightarrow z_i = (z_i' + R_E \parallel R_F)(1+a_v f)$$

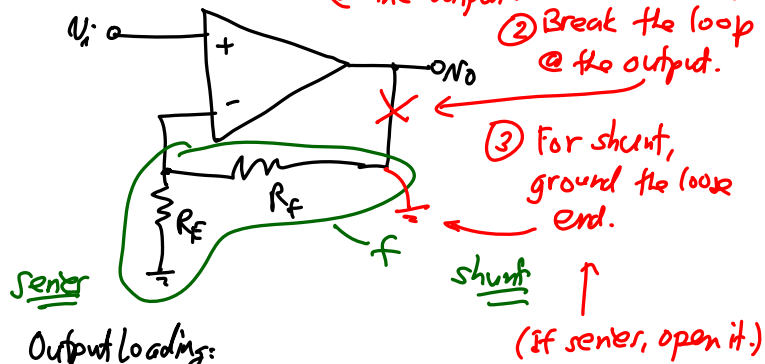
$$z_{oa} = z_o' \parallel (R_E + R_F) \parallel z_L \rightarrow z_o = \frac{z_o' \parallel (R_E + R_F) \parallel z_L}{(1+a_v f)}$$

Freq. Response:

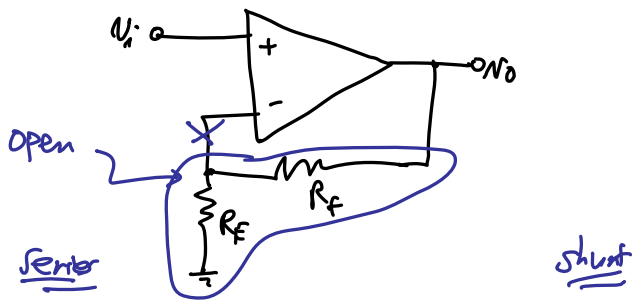
$$\omega_{-3dB} |_{\text{closed-loop}} = \left\{ \omega_{-3dB} |_{\text{open-loop w/ FB loading}} \right\} \times (1+a_v f)$$

To determine loading by FB:

Input Loading: ① Determine the feedback type @ the output. (Here, it's shunt.)
② Break the loop @ the output.



Output Loading:



- ① Determine the feedback type @ the input.
(Here, it's series.)
- ② Break the loop @ the input.
- ③ For series, open the loose end.
↓
(If shunt, short it.)