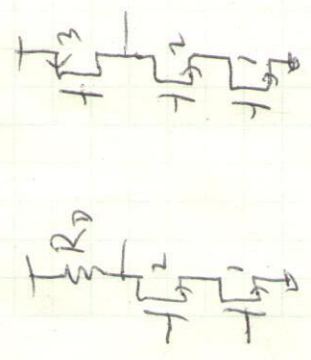


Mittner Friday in class
 1 prof (2 sides) notes
 no calculators

Homeworks 1-4
 Labs 1, 3 (not condence)

Cascode
 A_v
 C_{in}
 biasing

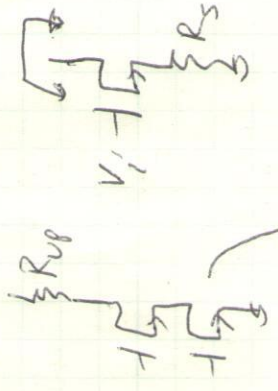


$R_D \ll S_{m2} r_{o2} r_{o1}$
 $A_v = -g_{m1} R_D$

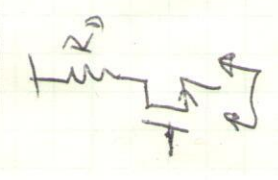
What about C_{in} ?

$C_{in} = C_{SS1} + (1 - A_{gd1}) C_{SD11}$
 $A_{gd1} \text{ calc: } g_{m1}$
 $R_o = r_{o1} \parallel R_{S2,up}$

Last time



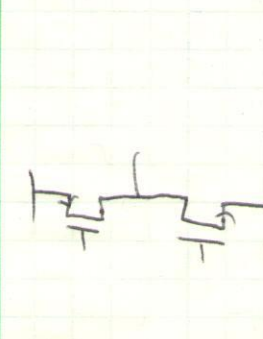
$R_o = (1 + g_{m2} r_{o2}) R_s + r_{o2}$
 $= (1 + g_{m2} R_s) r_{o2} + R_s$
 $\approx \begin{cases} g_{m2} r_{o2} R_s & R_s \gg \frac{1}{g_{m2}} \\ 2 r_{o2} & R_s = \frac{1}{g_{m2}} \\ r_{o2} & R_s \ll \frac{1}{g_{m2}} \end{cases}$
 $R_s = r_{o2} \Rightarrow R_o = g_{m2} r_{o2} r_{o1}$
 $G_m = g_{m1}$
 $A_v = -G_m R_o = -g_{m1} (S_{m2} r_{o2} r_{o1} \parallel R_{up})$



$v_d = i_s R_D$
 v_s, i_s
 find $R_{S,up} = \frac{v_s}{i_s}$
 KCL @ v_s : $i_s + g_m (0 - v_s) + \frac{1}{r_o} (v_d - v_s) = 0$
 $i_s + \frac{1}{r_o} (i_s R_D) = (g_m + \frac{1}{r_o}) v_s$
 $R_{S,up} = \frac{v_s}{i_s} = (1 + \frac{R_D}{r_o}) \frac{1}{g_m (1 + \frac{1}{g_m r_o})} \approx \frac{1}{g_m} (1 + \frac{R_D}{r_o})$

$R_D \ll r_o$
 $R_D = r_o$
 $R_D \gg r_o$

$R_{sup} = \begin{cases} \frac{1}{g_m} \\ \frac{2}{g_m} \\ \frac{R_D}{g_m r_o} \end{cases}$



 V_D
 V_{in}

$C_{in} \approx C_{gs1} + 2C_{gd1}$
 $A_v \approx -g_{m1} R_D$

$C_{in} \approx C_{gs1} + 3C_{gd1}$
 $A_v \approx -g_{m1} r_{o3}$

decouples gain & input capacitance (Compared to CS)
 Some cost in swing

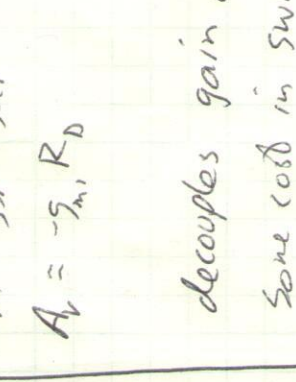
$R_D = R_{up} \parallel R_{down}$
 $R_{down} \approx g_{m2} r_{o2} r_{o1}$
 $R_{up} \approx g_{m3} r_{o3} r_{o4}$
 $A_v = -g_{m1} R_D \approx \frac{1}{2} (g_{m1} r_o)^2$

input capacitance:
 $A_{vCD1} = -g_{m1} (r_{o11} \parallel \frac{R_{up}}{g_{m2} r_{o2}}) \approx -\frac{g_{m1} r_o}{2}$

So, same input cap as simple common source
 but much higher gain ($g_{m1} r_o$ bigger)

$R_D \ll r_o$
 $R_D = r_o$
 $R_D \gg r_o$

$r_{o3} \approx r_{o2}$
 $A_{vCD1} \approx -g_{m1} \frac{2}{g_{m2}}$
 ≈ -2

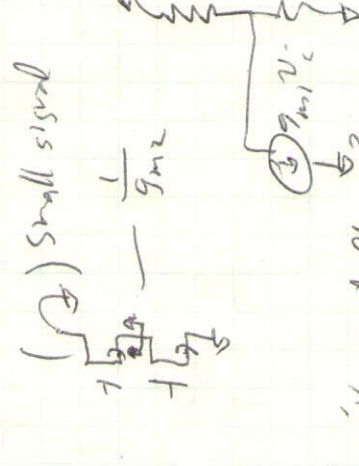


 V_{D1}
 V_{D2}
 V_{in}

Real resistor $\Rightarrow R_D \ll r_{o2}$ txf
 $A_{vCD1} \approx -\frac{1}{g_{m2}}$

$G_m = \frac{i_o}{V_i} |_{V_D=0}$

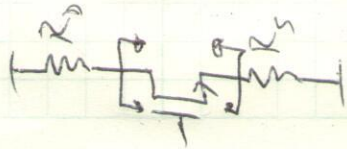
R_{up} since $v_D=0$



 Small signal
 $\frac{1}{g_{m2}}$
 i_o
 r_{o1}
 $g_{m1} v_i$

which way will current flow?
 current divider says $\frac{r_{o1}}{r_{o1} + \frac{1}{g_{m2}}}$ goes to i_o

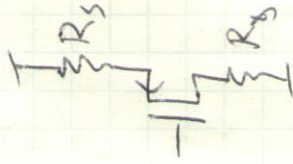
$\Rightarrow G_m \approx g_{m1}$



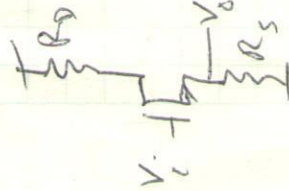
$$R_o = (1 + g_m R_s) r_o$$

$$R_o = \frac{1}{g_m} \left(1 + \frac{R_D}{r_o} \right)$$

or R_i



G_m for source follower w/ drain load

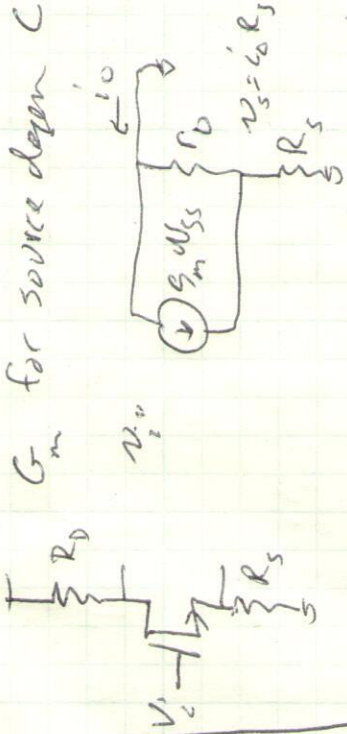


KCL @ v_s : $g_m v_i + g_m v_s + \frac{1}{r_o} (i_o R_D) = 0$

$$i_o \left[1 + \frac{R_D}{r_o} \right] = -g_m v_i$$

$$G_m = \frac{i_o}{v_i} = \frac{-g_m}{1 + \frac{R_D}{r_o}}$$

G_m for source degn CS

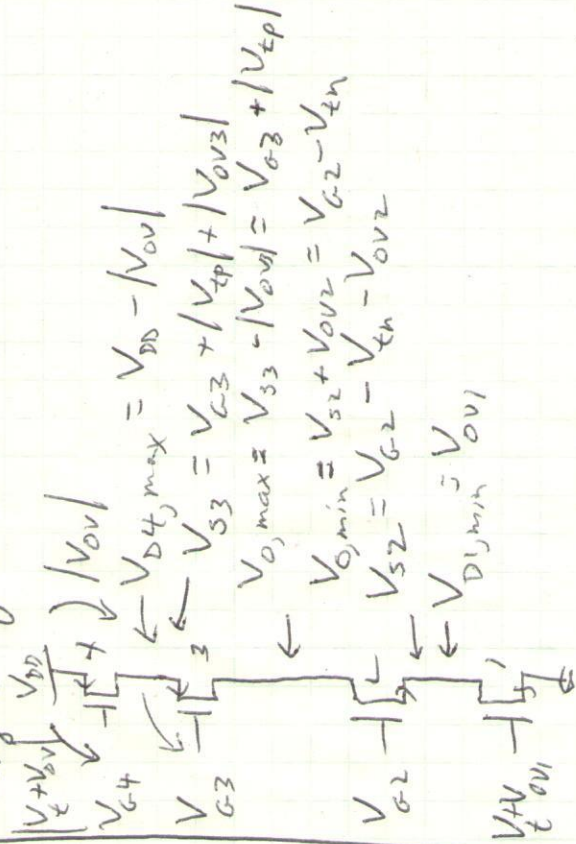


KCL @ v_d $i_o = g_m (v_i - i_o R_s) + \frac{1}{r_o} (0 - i_o R_s)$

$$i_o \left[1 + g_m R_s + \frac{R_s}{r_o} \right] = g_m v_i$$

$$G_m = \frac{i_o}{v_i} = \frac{g_m}{1 + g_m R_s + \frac{R_s}{r_o}} = \frac{g_m}{1 + g_m R_s \left(1 + \frac{1}{g_m r_o} \right)}$$

Biasing for quadratic devices in saturation



$$V_{D1, \max} = V_{DD} - |V_{ov1}|$$

$$V_{S3} = V_{G3} + |V_{tp}| + |V_{ov3}|$$

$$V_{O, \max} = V_{S3} - |V_{ov1}| = V_{G3} + |V_{tp}|$$

$$V_{O, \min} = V_{S2} + V_{ov2} = V_{G2} - V_{th}$$

$$V_{S2} = V_{G2} - V_{th} - V_{ov2}$$

$$V_{D1, \min} = V_{ov1}$$