

EE143 – Fall 2016 Microfabrication Technologies

Lecture 5: Thermal Oxidation Reading: Jaeger Chapter 3

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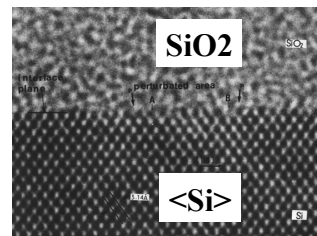
1



Properties of SiO₂

Thermal SiO₂ is amorphous.
Weight Density = 2.20 gm/cm³
Molecular Density = 2.3E22 molecules/cm³

Crystalline SiO₂ (Quartz) = 2.65 gm/cm³



- (1) Excellent Electrical Insulator
Resistivity > 1E20 ohm-cm Energy Gap ~ 9 eV
- (2) High Breakdown Electric Field > 10MV/cm
- (3) Stable and Reproducible Si/SiO₂ Interface

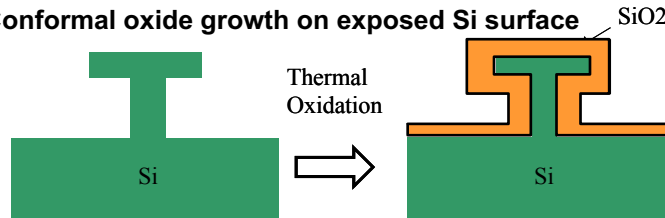


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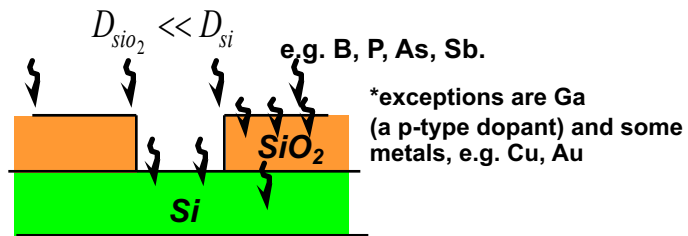


Properties of SiO₂ (cont'd)

(4) Conformal oxide growth on exposed Si surface



(5) SiO₂ is a good diffusion mask for common dopants



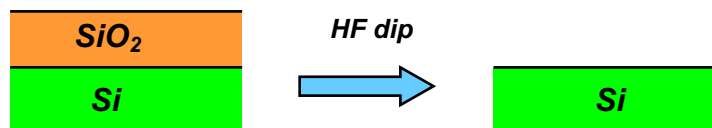
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Properties of SiO₂ (cont'd)

(6) Very good etching selectivity between Si and SiO₂.

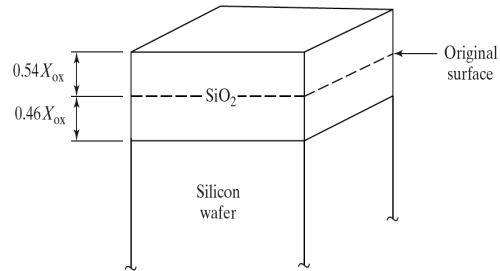


Cal

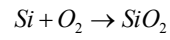
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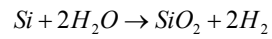
Thermal Oxidation of Silicon



Dry Oxidation



Wet Oxidation



Growth Occurs 54% above and 46% below original surface as silicon is consumed

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Thermal Oxidation Equipment



Horizontal Furnace



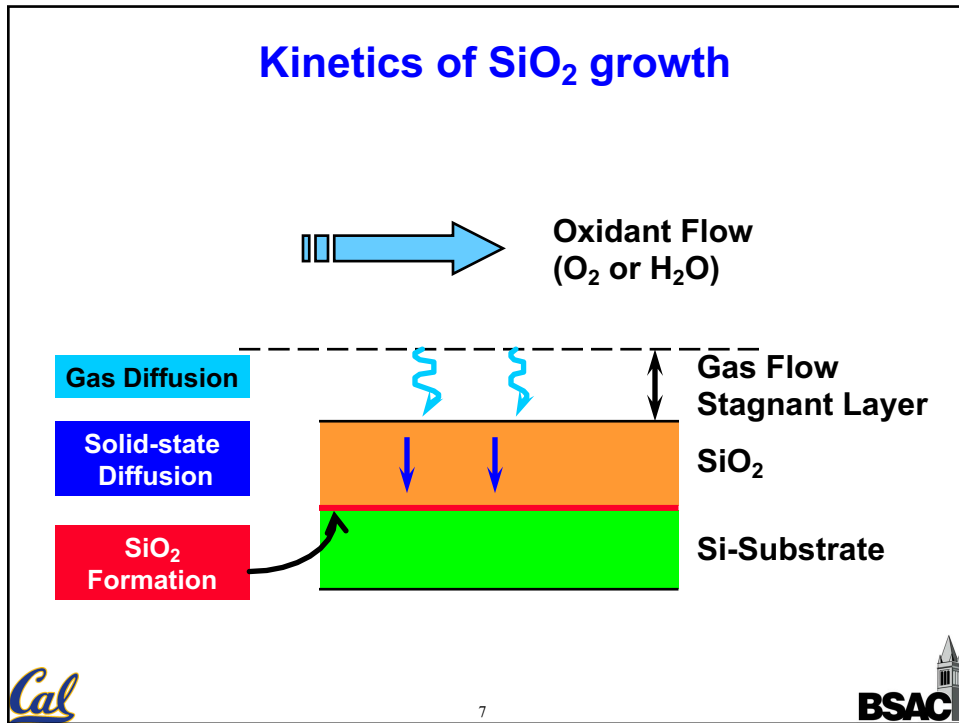
Vertical Furnace

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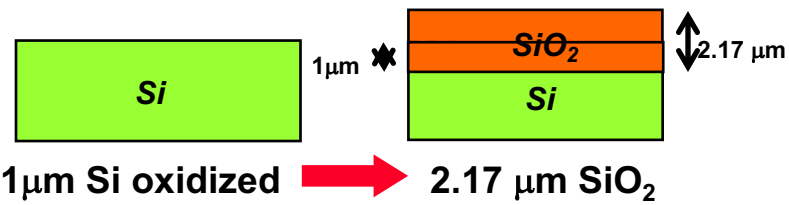
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Kinetics of SiO₂ growth



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Silicon consumption during oxidation



$$X_{si} = X_{ox} \cdot \frac{N_{ox}}{N_{si}}$$

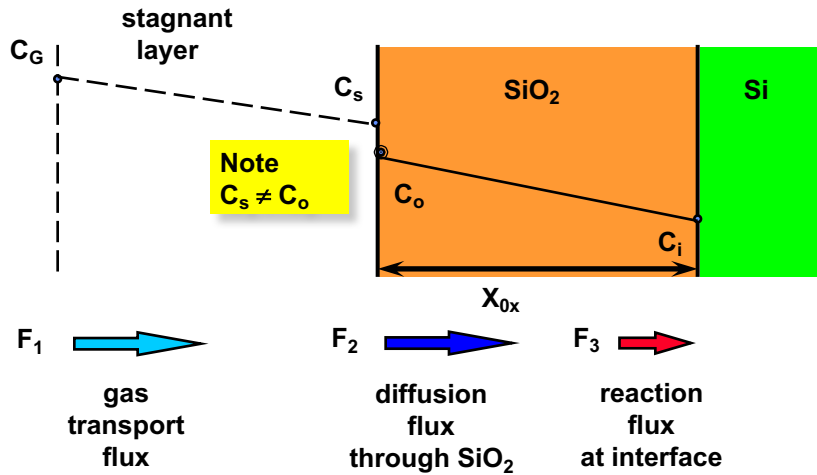
← molecular density of SiO₂
← atomic density of Si

$$= X_{ox} \cdot \frac{2.3 \times 10^{22} \text{ molecules / cm}^3}{5 \times 10^{22} \text{ atoms / cm}^3} = 0.46 X_{ox}$$



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The Deal-Grove Model of Oxidation



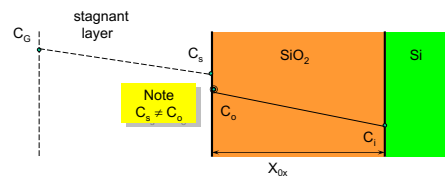
- F : oxygen flux – the number of oxygen molecules that crosses a plane per unit area per second



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The Deal-Grove Model of Oxidation (cont'd)



F_1 → F_2 → F_3 →

★ $F_1 = h_G(C_G - C_s)$
 → Mass transfer coefficient [cm/sec].

★ $F_2 = -D \frac{\partial C}{\partial x}$ "Fick's Law of Solid-state Diffusion"
 $\cong D \cdot \left(\frac{C_o - C_i}{X_{ox}} \right)$

★ $F_3 = k_s \cdot C_i$
 → Diffusivity [cm²/sec]
 → Oxidation reaction rate constant



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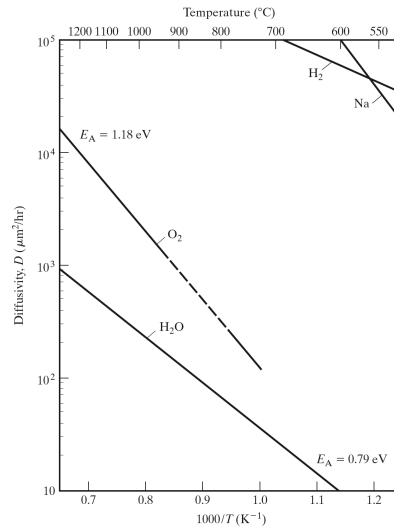
Diffusivity: the diffusion coefficient

$$D = D_0 \exp\left(-\frac{E_A}{kT}\right) \quad \text{Arrhenius equation}$$

E_A = activation energy

k = Boltzmann's constant = 1.38×10^{-23} J/K

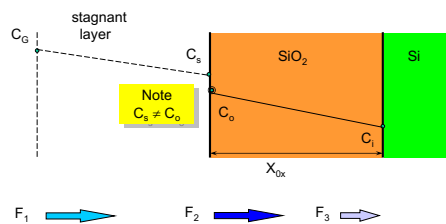
T = absolute temperature



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The Deal-Grove Model of Oxidation (cont'd)



- C_S and C_O are related by Henry's Law
- C_G is a controlled process variable (proportional to the input oxidant gas pressure)

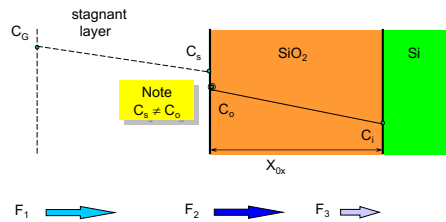
Only C_O and C_I are the 2 unknown variables
which can be solved from the steady-state condition:
 $F_1 = F_2 = F_3$ (2 equations)



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The Deal-Grove Model of Oxidation (cont'd)



Note
 $C_s \neq C_o$

$$C_o = H \cdot P_s \quad \text{Henry's Law}$$

Henry's constant \nearrow \nwarrow partial pressure of oxidant at surface [in gaseous form].

$$= H \cdot (kT \cdot C_s) \quad \text{from ideal gas law } PV = NkT$$

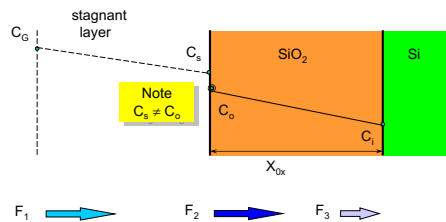
$$\therefore C_s = \frac{C_o}{HkT}$$

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The Deal-Grove Model of Oxidation (cont'd)



Note
 $C_s \neq C_o$

Define

$$C_A \equiv (HkT \cdot C_G)$$

$$F_1 = \frac{h_G}{HkT} (C_A - C_o)$$

Similarly, we can set up equations for F_2 and F_3

Using the steady-state condition:

$$\underbrace{F_1 = F_2 = F_3}_{\text{(1) (2)}} \quad \text{We therefore can solve for } C_o \text{ and } C_i$$

Cal

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The Deal-Grove Model of Oxidation (cont'd)

We have: $F_2 \cong D \cdot \left(\frac{C_o - C_i}{X_{ox}} \right)$ $F_3 = k_s \cdot C_i$

At equilibrium: $F_1 = F_2 = F_3$

Solving, we get:

$$C_i = \frac{C_A}{1 + \frac{k_s}{h} + \frac{k_s X_{ox}}{D}} \quad C_o = C_i \cdot \left(1 + \frac{k_s X_{ox}}{D} \right)$$

$$F \quad (= F_1 = F_2 = F_3) = k_s \cdot C_i = \frac{k_s C_A}{1 + \frac{k_s}{h} + \frac{k_s X_{ox}}{D}}$$

where $h = h_g / HkT$



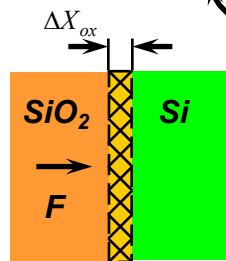
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The Deal-Grove Model of Oxidation (cont'd)

We can convert flux into growth thickness from:

$$\frac{F}{N_1} = \left(\frac{dX_{ox}}{dt} \right)$$



Oxidant molecules/unit volume required to form a unit volume of SiO₂.

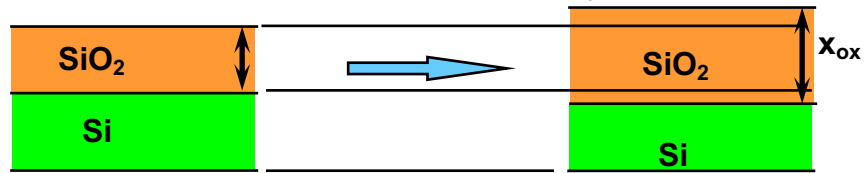


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The Deal-Grove Model of Oxidation (cont'd)

Initial Condition: At $t = 0$, $X_{ox} = X_i$



Solution $X_{ox}^2 + AX_{ox} = B(t + \tau)$

$$A \equiv 2D \left(\frac{1}{k_s} + \frac{1}{h_g} \right)$$

Note: $h_g \gg k_s$ for typical oxidation condition

$$B \equiv \frac{2DC_A}{N_1}$$

$$\tau = \frac{X_i^2 + AX_i}{B}$$



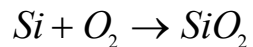
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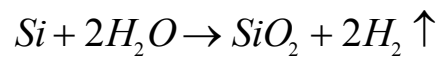
Dry / Wet Oxidation

Note: "dry" and "wet" oxidation have different N_1 factors

$$N_1 = 2.3 \times 10^{22} / \text{cm}^3 \quad \text{for } O_2 \text{ as oxidant}$$



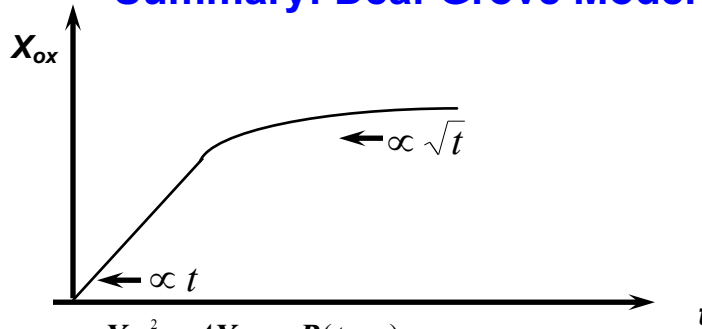
$$N_1 = 4.6 \times 10^{22} / \text{cm}^3 \quad \text{for } H_2O \text{ as oxidant}$$



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Summary: Deal-Grove Model



$$X_{ox}^2 + AX_{ox} = B(t + \tau)$$

$$2X_{ox} \frac{dx_{ox}}{dt} + A \frac{dx_{ox}}{dt} = B$$

$$\therefore \frac{dx_{ox}}{dt} = \frac{B}{A + 2X_{ox}}$$

Oxide Growth Rate slows down with increase of oxide thickness

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Solution: Oxide Thickness Regimes

$$X_{ox} = \frac{A}{2} \left\{ \sqrt{1 + \left(\frac{t + \tau}{A^2/4B} \right)} - 1 \right\}$$

(Case 1) Large t [large X_{ox}]

$$X_{ox} \rightarrow \sqrt{Bt}$$

(Case 2) Small t [Small X_{ox}]

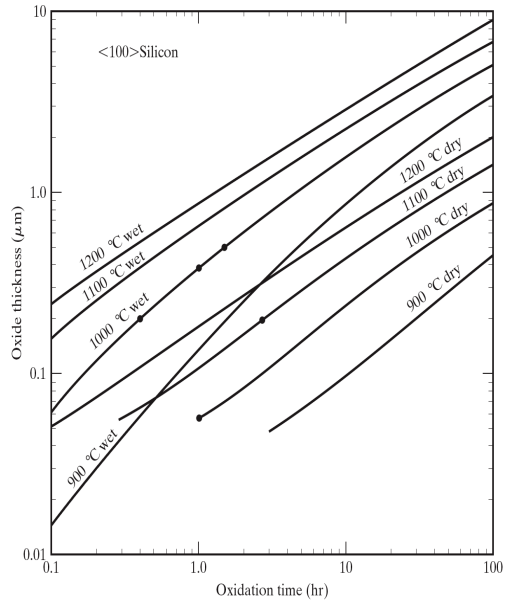
$$X_{ox} \rightarrow \frac{B}{A} t$$

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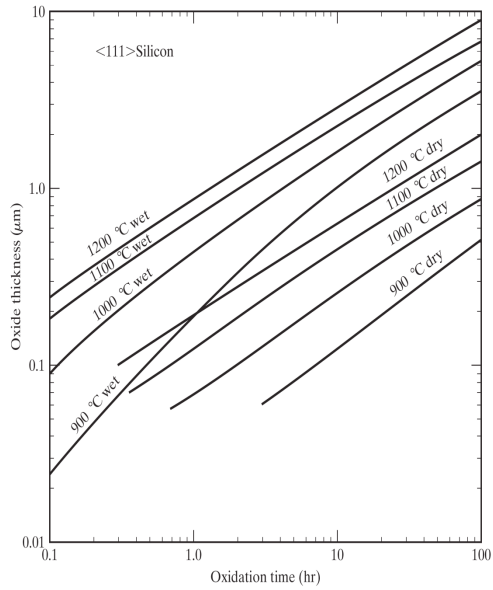
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Thermal Oxidation on <100> Silicon



Thermal Oxidation on <111> Silicon



Thermal Oxidation Example

A $\langle 100 \rangle$ silicon wafer has a 2000-Å oxide on its surface

(a) How long did it take to grow this oxide at 1100° C in dry oxygen?

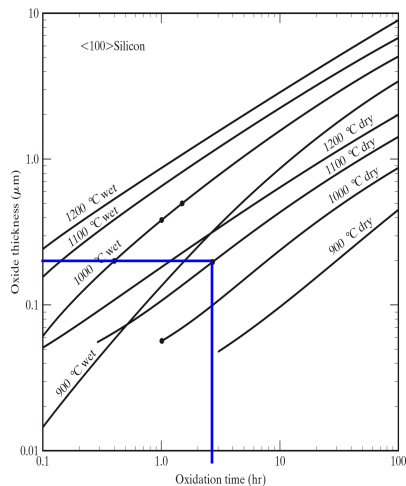
(b) The wafer is put back in the furnace in wet oxygen at 1000° C. How long will it take to grow an additional 3000 Å of oxide?



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Thermal Oxidation Example Graphical Solution



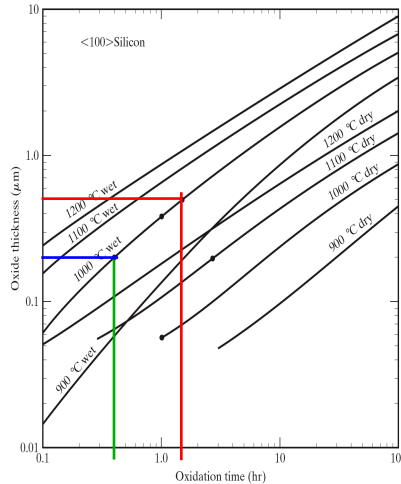
(a) According to Fig. 3.6, it would take **2.8 hr** to grow **0.2 μm** oxide in dry oxygen at 1100° C.



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Thermal Oxidation Example Graphical Solution



(b) The total oxide thickness at the end of the oxidation would be **0.5 μm** which would require **1.5 hr** to grow if there was no oxide on the surface to begin with. However, the wafer “thinks” it has already been in the furnace **0.4 hr**. Thus the additional time needed to grow the 0.3 μm oxide is $1.5 - 0.4 = 1.1$ hr.



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Thermal Oxidation Example Mathematical Solution

(a) From Table 3.1,

$$B = 7.72 \times 10^2 \exp\left(\frac{-1.23}{kT}\right) \frac{\mu\text{m}^2}{\text{hr}} \quad \frac{B}{A} = 3.71 \times 10^6 \exp\left(\frac{-2.00}{kT}\right) \frac{\mu\text{m}}{\text{hr}} \quad X_i = 25 \text{ nm}$$

$$\text{For } T = 1373 \text{ K, } B = 0.0236 \frac{\mu\text{m}^2}{\text{hr}} \text{ and } \frac{B}{A} = 0.169 \frac{\mu\text{m}}{\text{hr}}$$

$$\tau = \frac{(0.025 \mu\text{m})^2}{0.0236 \frac{\mu\text{m}^2}{\text{hr}}} + \frac{0.025 \mu\text{m}}{0.169 \frac{\mu\text{m}}{\text{hr}}} = 0.174 \text{ hr}$$

$$t = \frac{(0.2 \mu\text{m})^2}{0.0236 \frac{\mu\text{m}^2}{\text{hr}}} + \frac{0.2 \mu\text{m}}{0.169 \frac{\mu\text{m}}{\text{hr}}} - 0.174 \text{ hr} = 2.70 \text{ hr}$$



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Thermal Oxidation Example Mathematical Solution

(b) From Table 3.1,

$$B = 3.86 \times 10^2 \exp\left(\frac{-0.78}{kT}\right) \frac{\mu\text{m}^2}{\text{hr}} \quad \frac{B}{A} = 9.70 \times 10^7 \exp\left(\frac{-2.05}{kT}\right) \frac{\mu\text{m}}{\text{hr}} \quad X_i = 0$$

$$\text{For } T = 1273 \text{ K, } B = 0.314 \frac{\mu\text{m}^2}{\text{hr}} \text{ and } \frac{B}{A} = 0.742 \frac{\mu\text{m}}{\text{hr}}$$

$$\tau = \frac{(0.2 \mu\text{m})^2}{0.314 \frac{\mu\text{m}^2}{\text{hr}}} + \frac{0.2 \mu\text{m}}{0.742 \frac{\mu\text{m}}{\text{hr}}} = 0.398 \text{ hr}$$

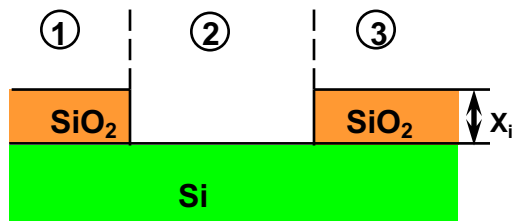
$$t = \frac{(0.5 \mu\text{m})^2}{0.314 \frac{\mu\text{m}^2}{\text{hr}}} + \frac{0.5 \mu\text{m}}{0.742 \frac{\mu\text{m}}{\text{hr}}} - 0.398 \text{ hr} = 1.07 \text{ hr}$$

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Effect of X_i on Wafer Topography

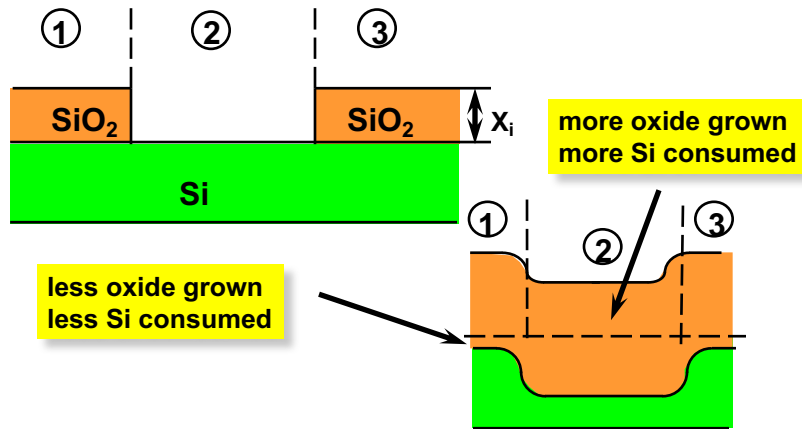


Cal

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Effect of X_i on Wafer Topography



Cal

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Factors Influencing Thermal Oxidation

- Temperature
- Ambient Type (Dry O_2 , Steam, HCl)
- Ambient Pressure
- Substrate Crystallographic Orientation
- Substrate Doping

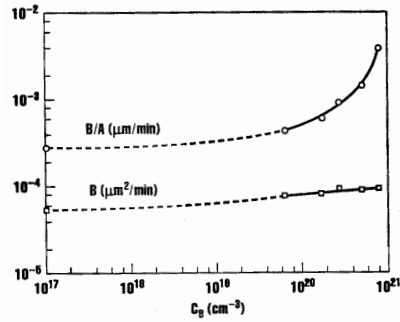
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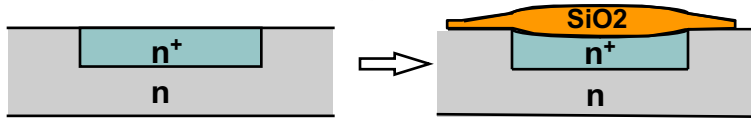
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High Doping Concentration Effect

Coefficients for dry oxidation at 900°C
as function of surface Phosphorus concentration



Dry oxidation, 900°C



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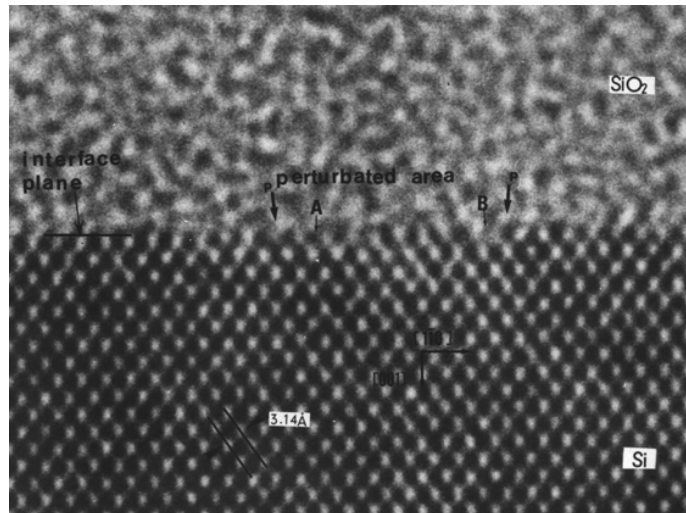
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Transmission Electron Micrograph of Si/SiO₂ Interface

Amorphous SiO₂

Crystalline Si

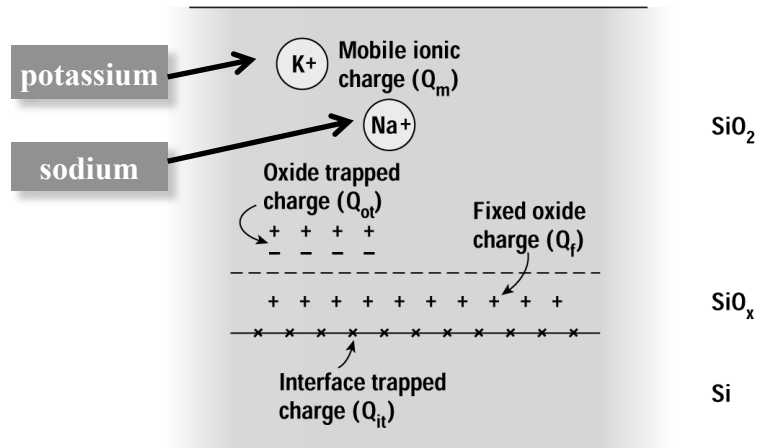


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Thermal Oxide Charges

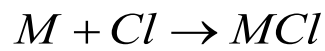
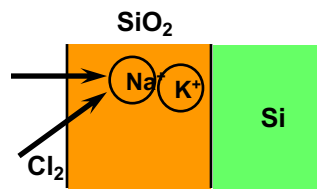


Oxide Quality Improvement

- To minimize Interface Charges Q_f and Q_{it}
- Use inert gas ambient (Ar or N_2) when cooling down at end of oxidation step
- A final annealing step at $400\text{-}450^\circ\text{C}$ is performed with $10\%\text{H}_2+90\%\text{N}_2$ ambient (“forming gas”) after the IC metallization step.

Oxidation with Chlorine-containing Gas

- Introduction of halogen species during oxidation
e.g. add ~1- 5% HCl or TCE (trichloroethylene) to O₂
 - reduction in metallic contamination
 - improved SiO₂/Si interface properties



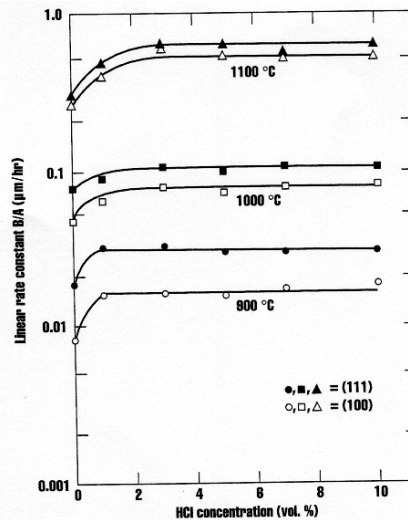
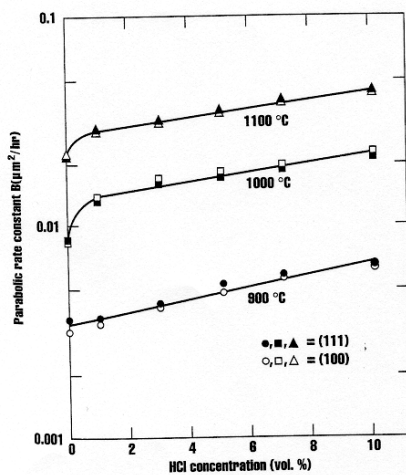
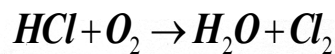
Na⁺ or K⁺ in SiO₂ are mobile!



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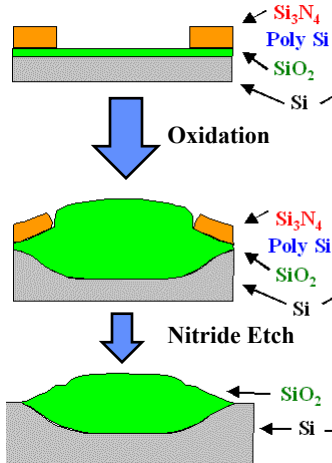
Effect of HCl on Oxidation Rate



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Local Oxidation of Si (LOCOS)



~100 Å SiO_2 (thermal) - pad oxide
to release mechanical stress
between nitride and Si.



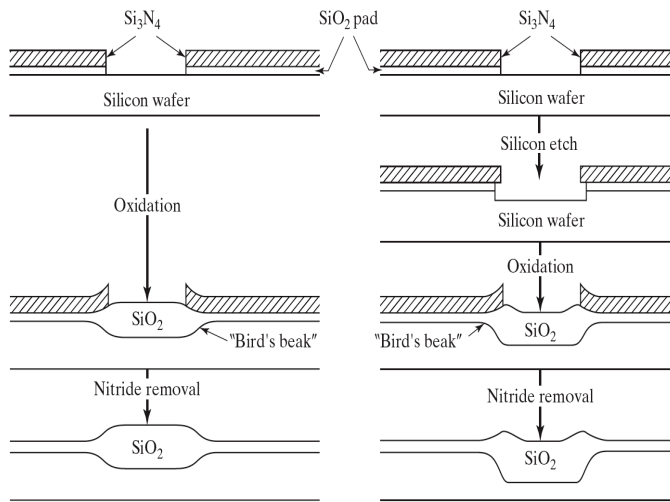
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Local Oxidation of Silicon (LOCOS)

Standard process suffers for significant bird's beak

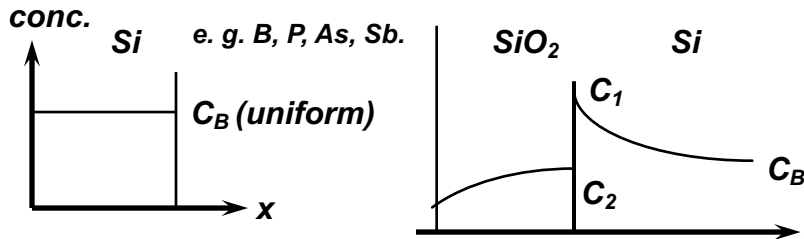
Fully recessed process attempts to minimize bird's beak



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Dopant Redistribution during Thermal Oxidation



Segregation Coefficient

$$\begin{aligned}
 m &\equiv \frac{\text{equilibrium dopant conc. in Si}}{\text{equilibrium dopant conc. in SiO}_2} \\
 \text{Fixed ratio} \nearrow &= \frac{C_1}{C_2} \quad (\text{can be } > 1 \text{ or } < 1)
 \end{aligned}$$

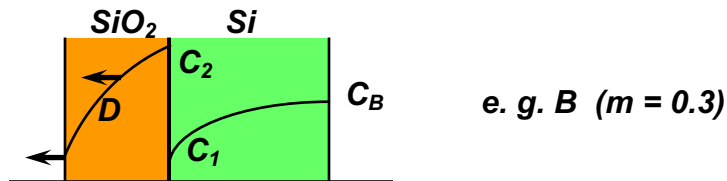


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Four Cases of Interest

(A) $m < 1$ and dopant diffuses slowly in SiO_2



flux loss through SiO_2 surface not considered here.

\Rightarrow B will be depleted near Si interface.

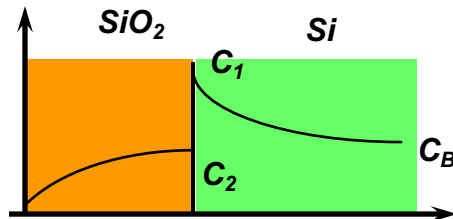


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Four Cases of Interest

(B) $m > 1$, slow diffusion in SiO_2 .



e.g. P, As, Sb

⇒ dopant piling up near Si interface
for P, As & Sb

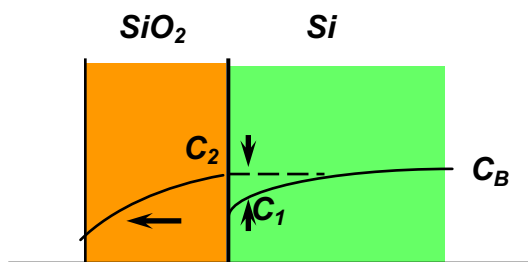
Cal

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Four Cases of Interest

(C) $m < 1$, fast diffusion in SiO_2



e. g.
B,
oxidize with
presence of H_2

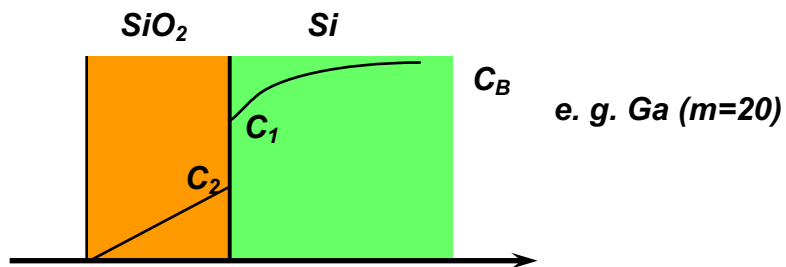
Cal

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Four Cases of Interest

(D) $m > 1$, fast diffusion in SiO_2

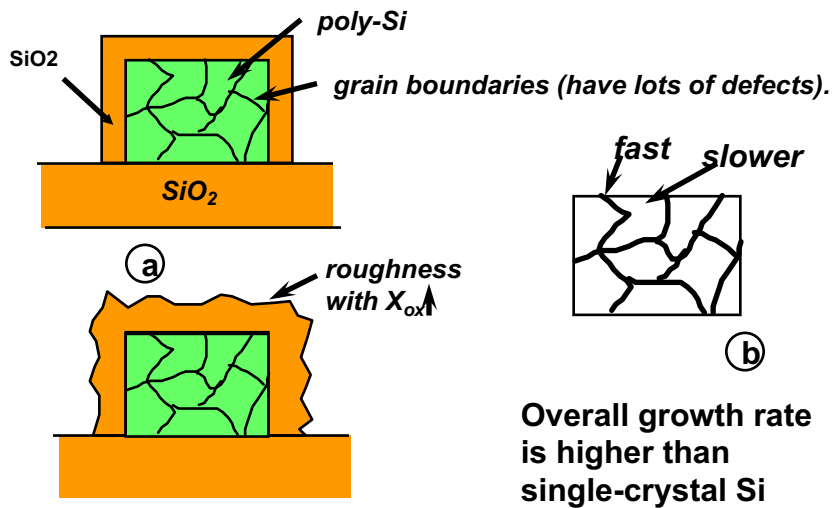


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Polycrystalline Si Oxidation

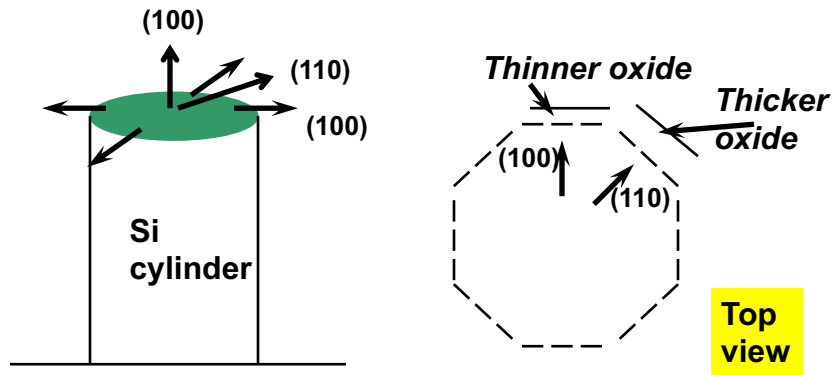


Cal

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2-Dimensional oxidation effects



Mechanical stress created by SiO_2 volume expansion also affects oxide growth rate