

# **EE16B, Spring 2018 UC Berkeley EECS**

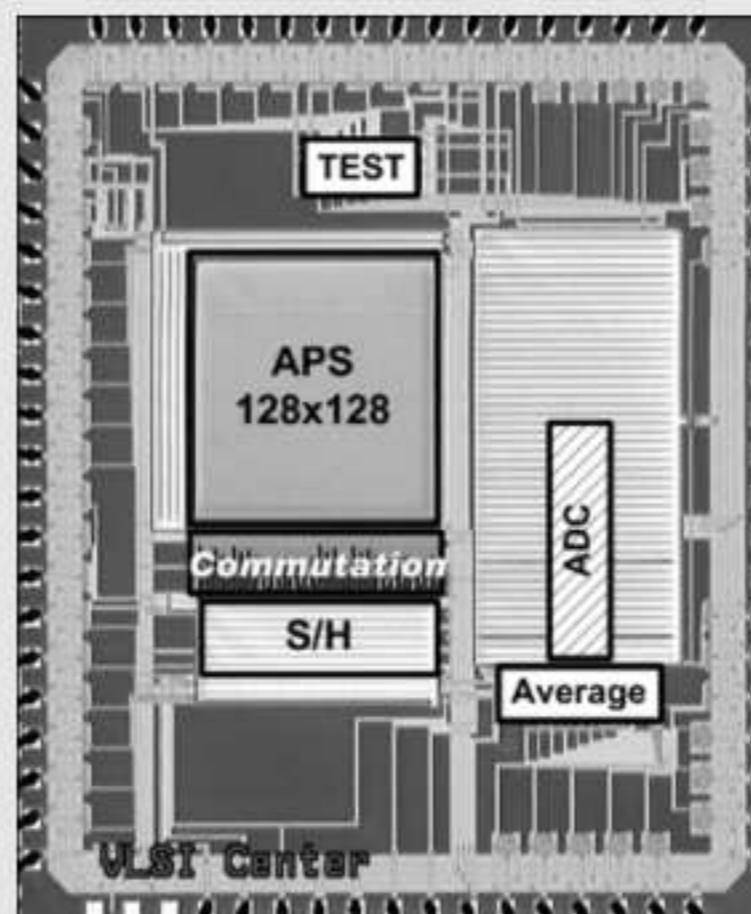
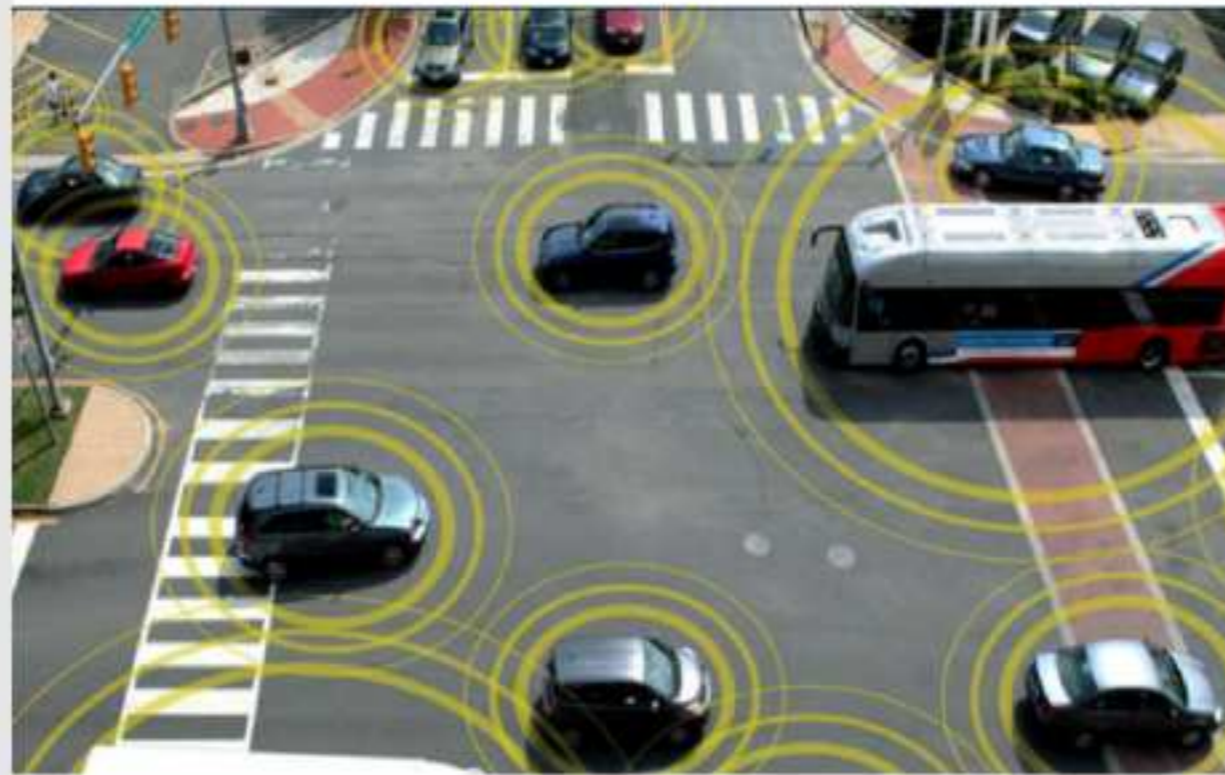
**Maharbiz and Roychowdhury**

**Lecture 4A: Overview Slides**

**State Space Representations**

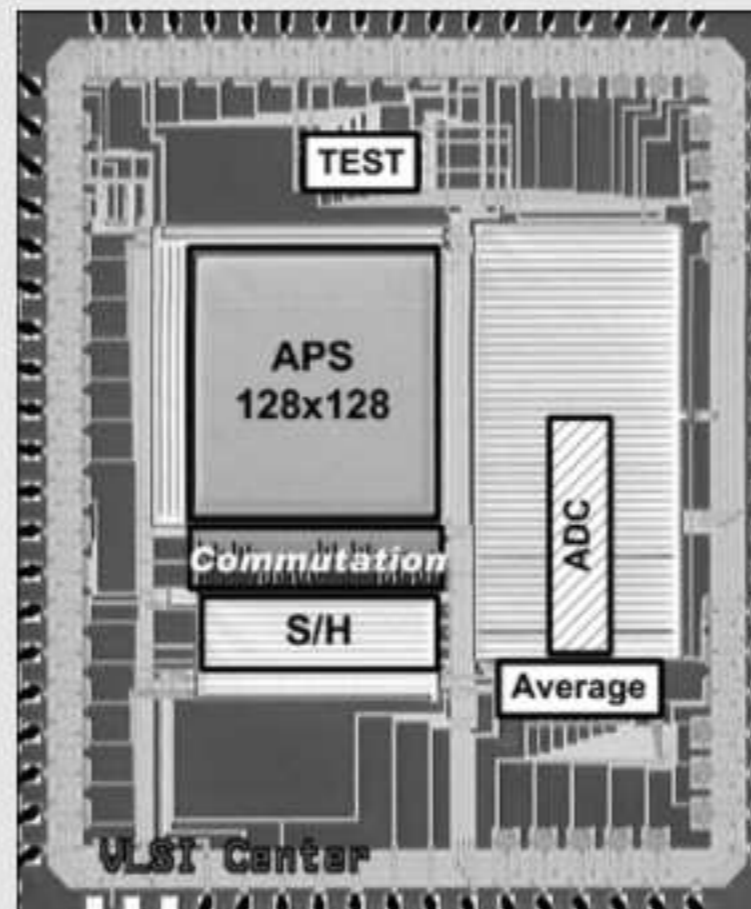
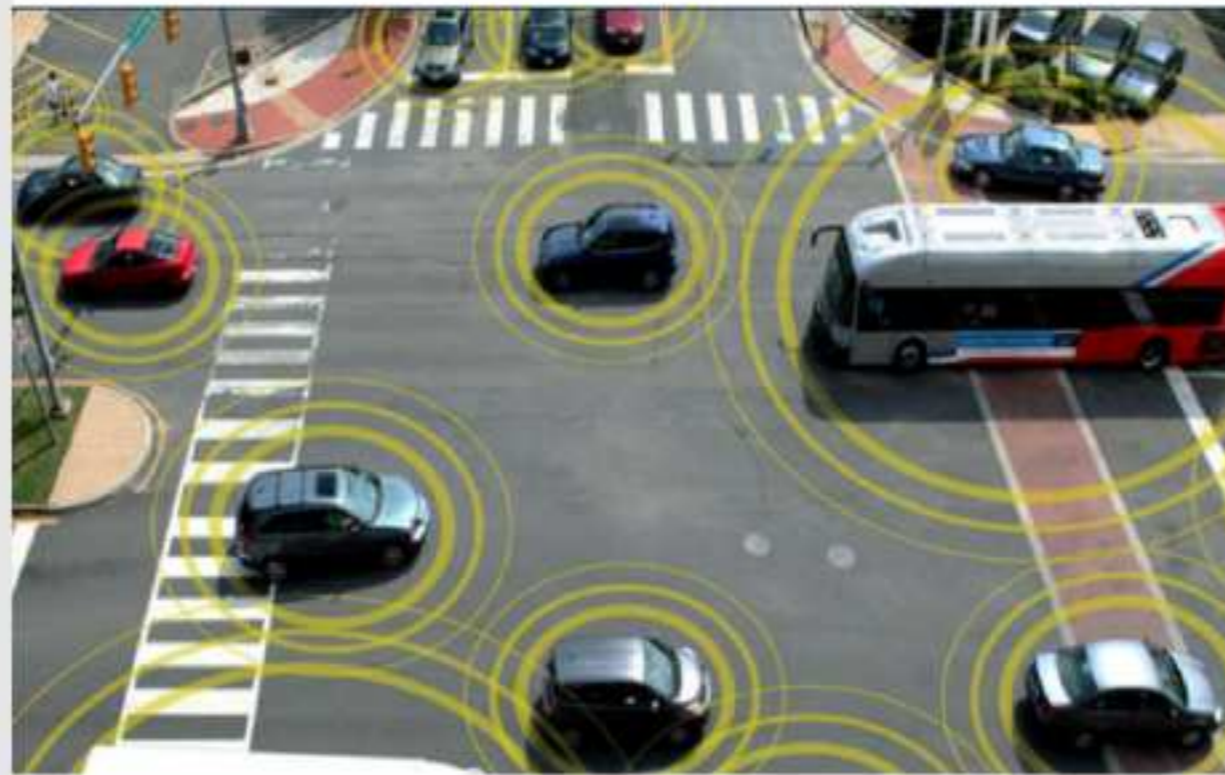
# Systems

- Previously: circuits
- **Now: systems**
  - circuits + more: a broader concept



# Systems

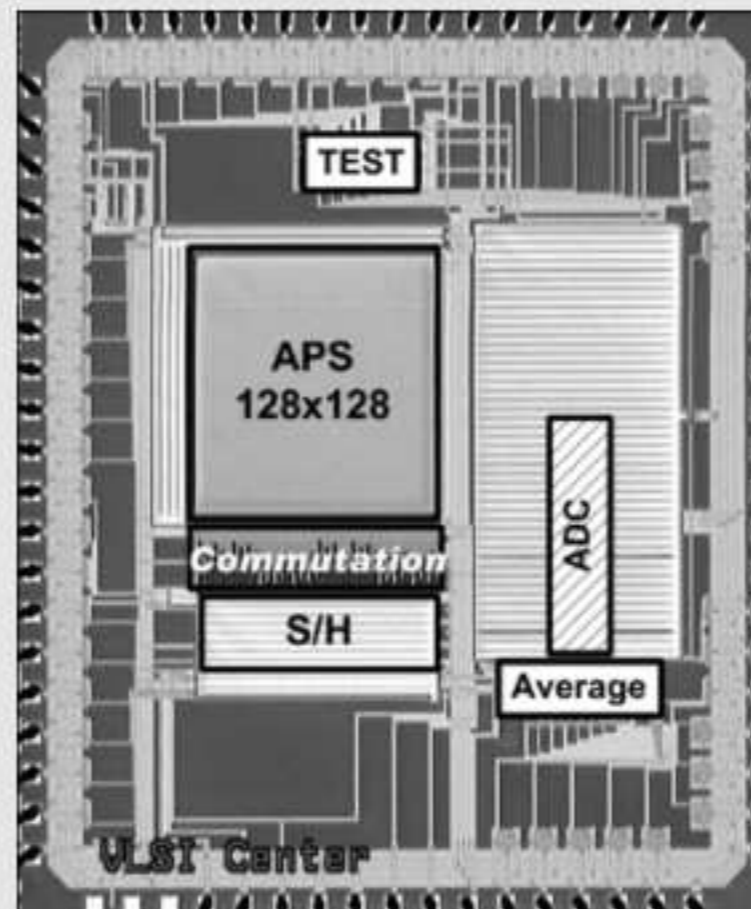
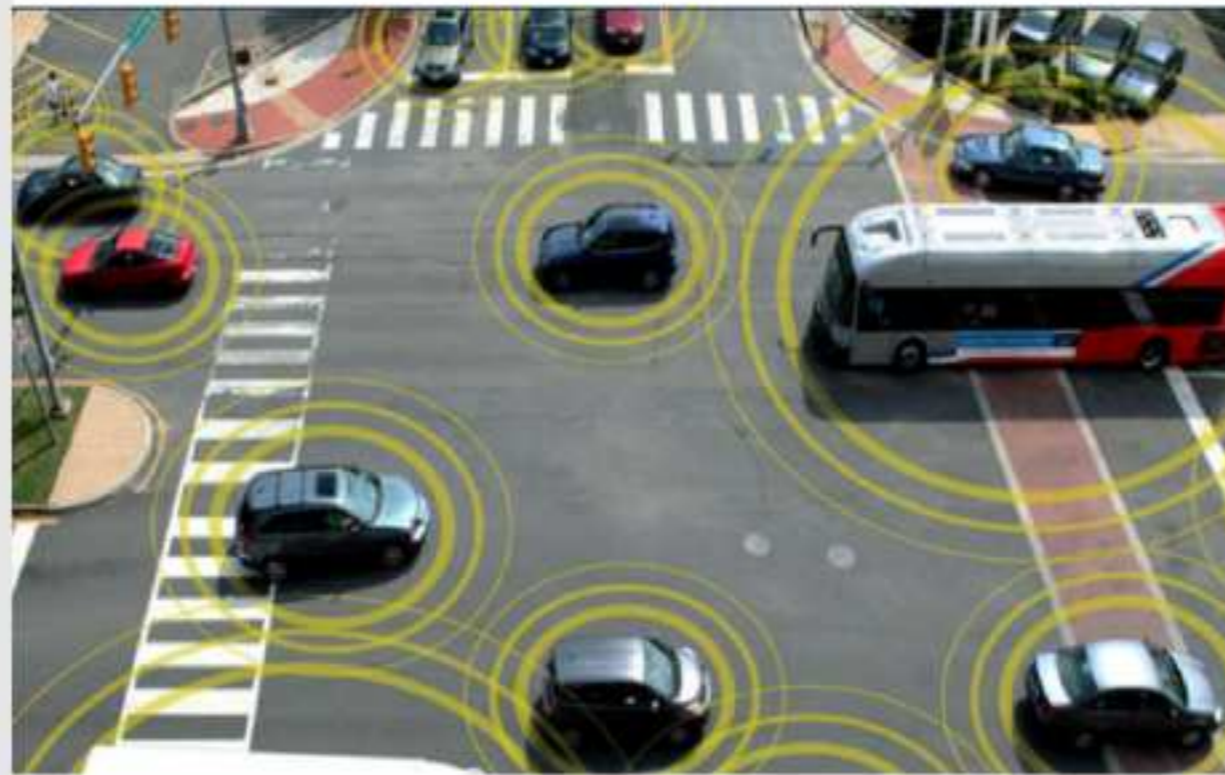
- Previously: circuits
- **Now: systems**
  - circuits + more: a broader concept



- **Can be enormously complex**
- **multi-domain**
  - EE (control, comm., computing, ...)
  - mech., chem., optical, ...

# Systems

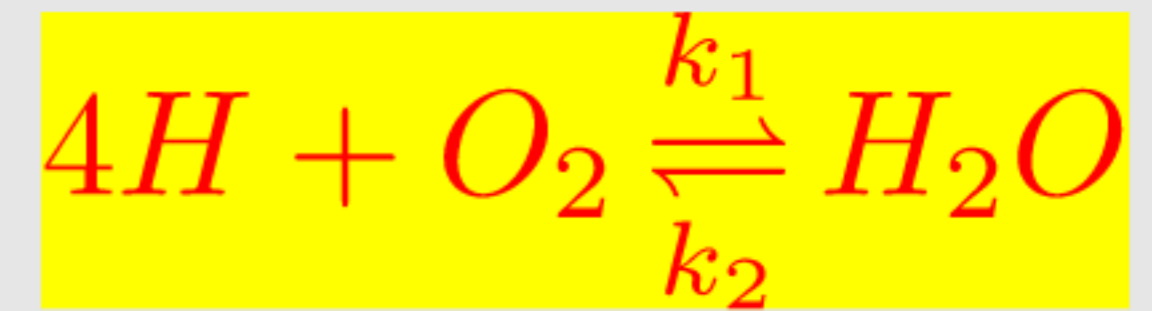
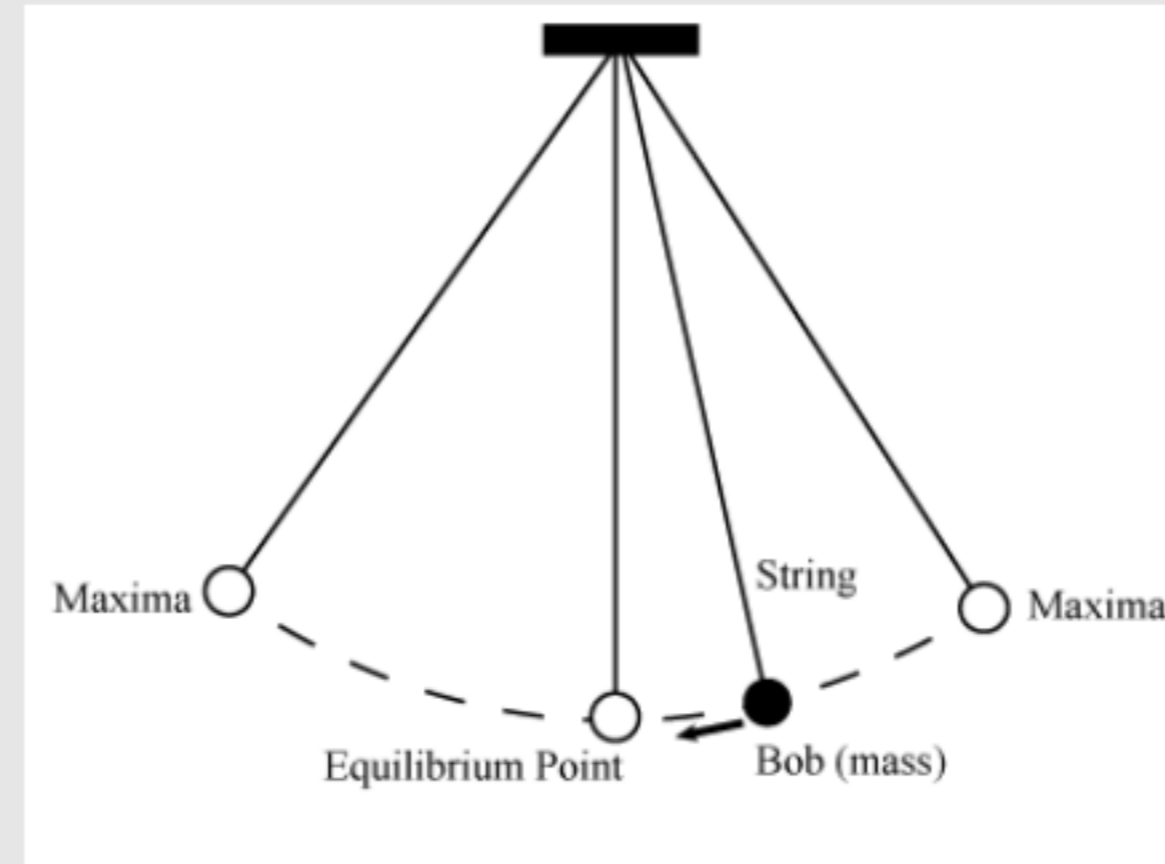
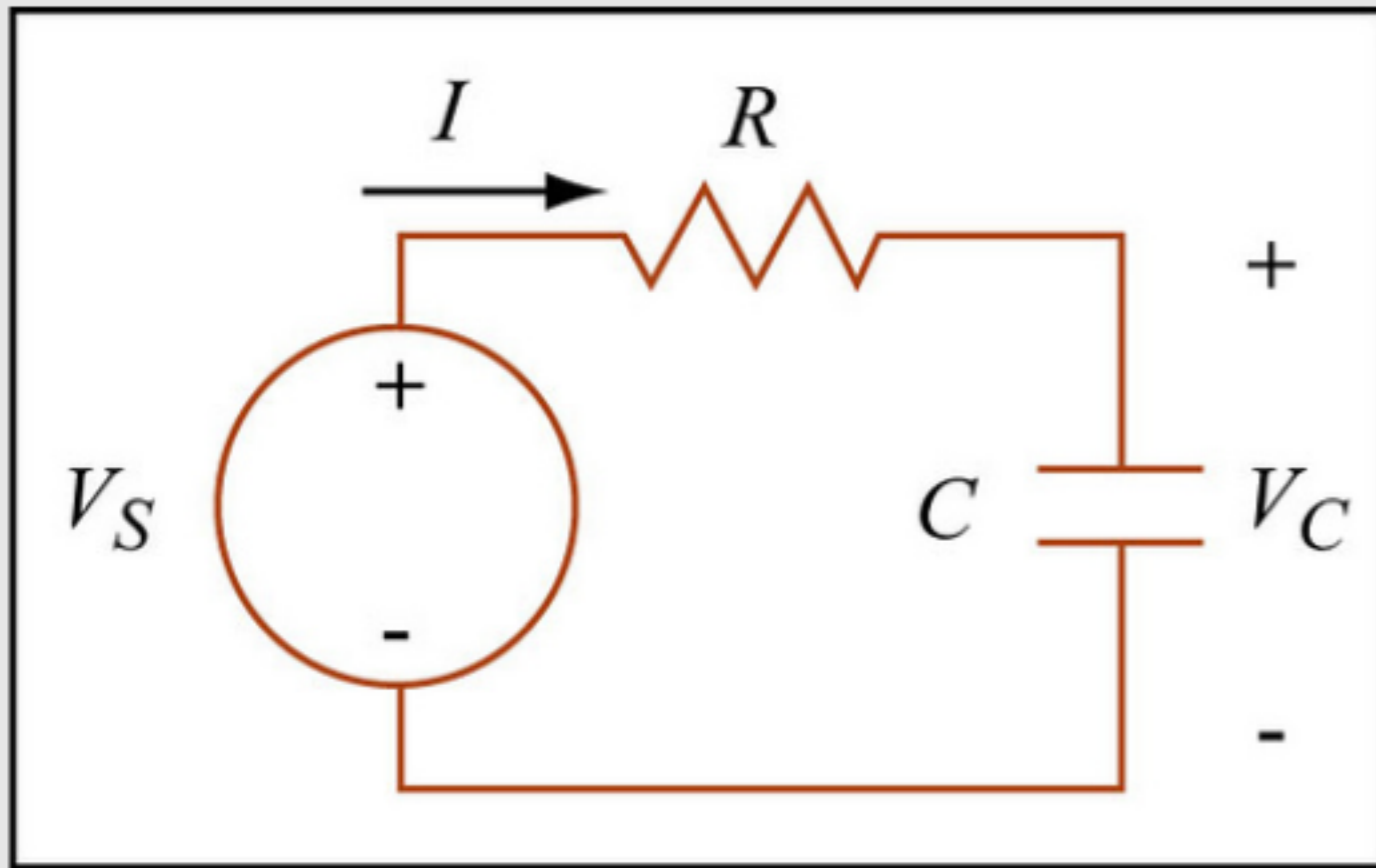
- Previously: circuits
- **Now: systems**
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- **Can be enormously complex**
- **multi-domain**
  - EE (control, comm., computing, ...)
  - mech., chem., optical, ...
- **hierarchy of sub-systems**

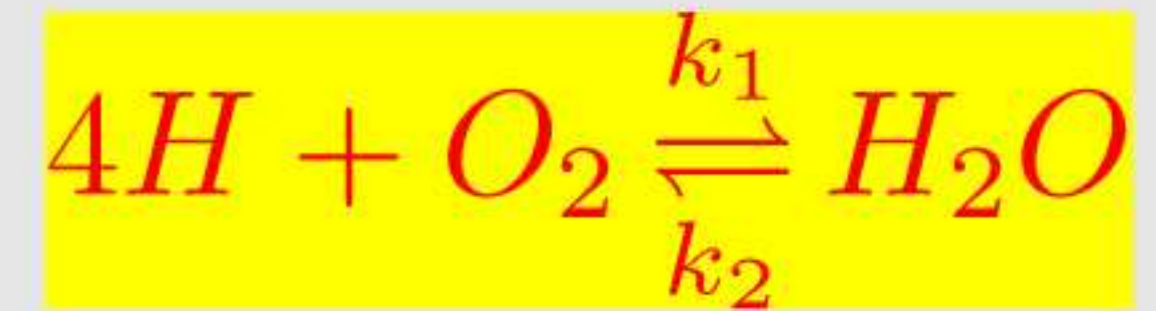
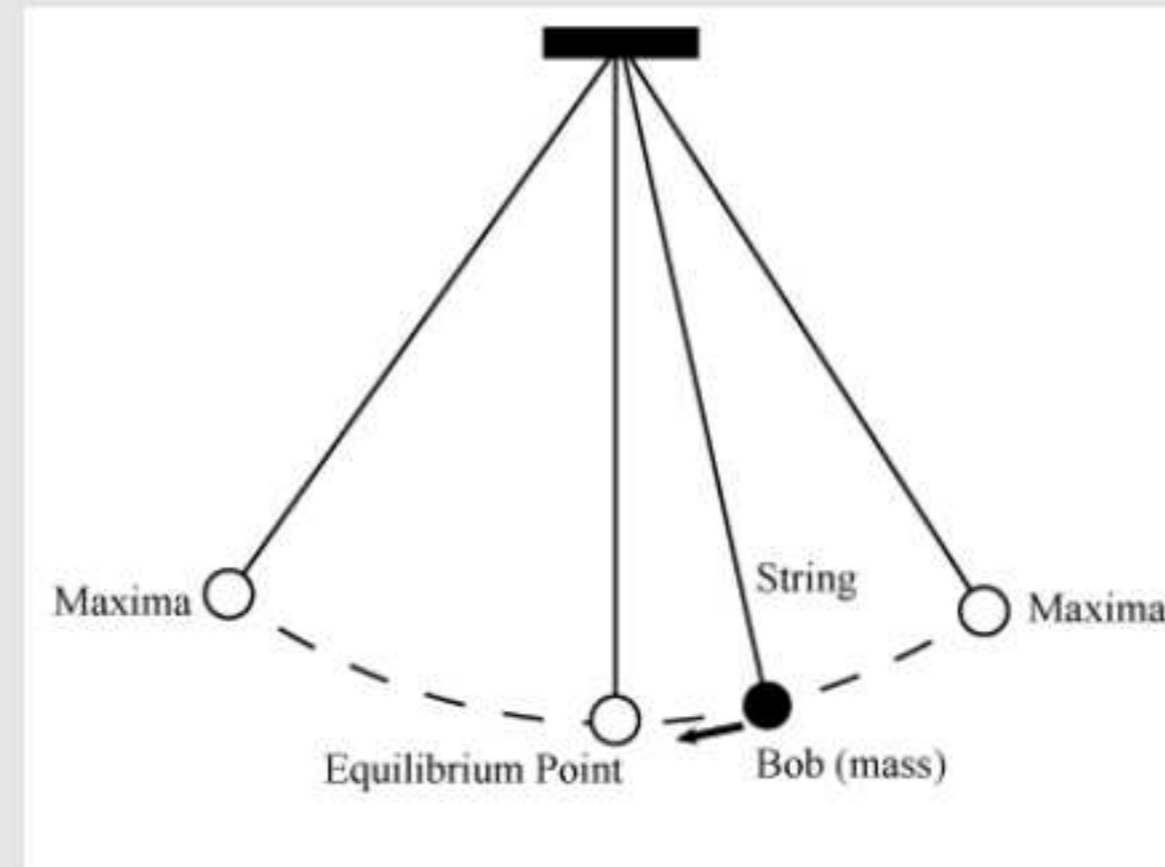
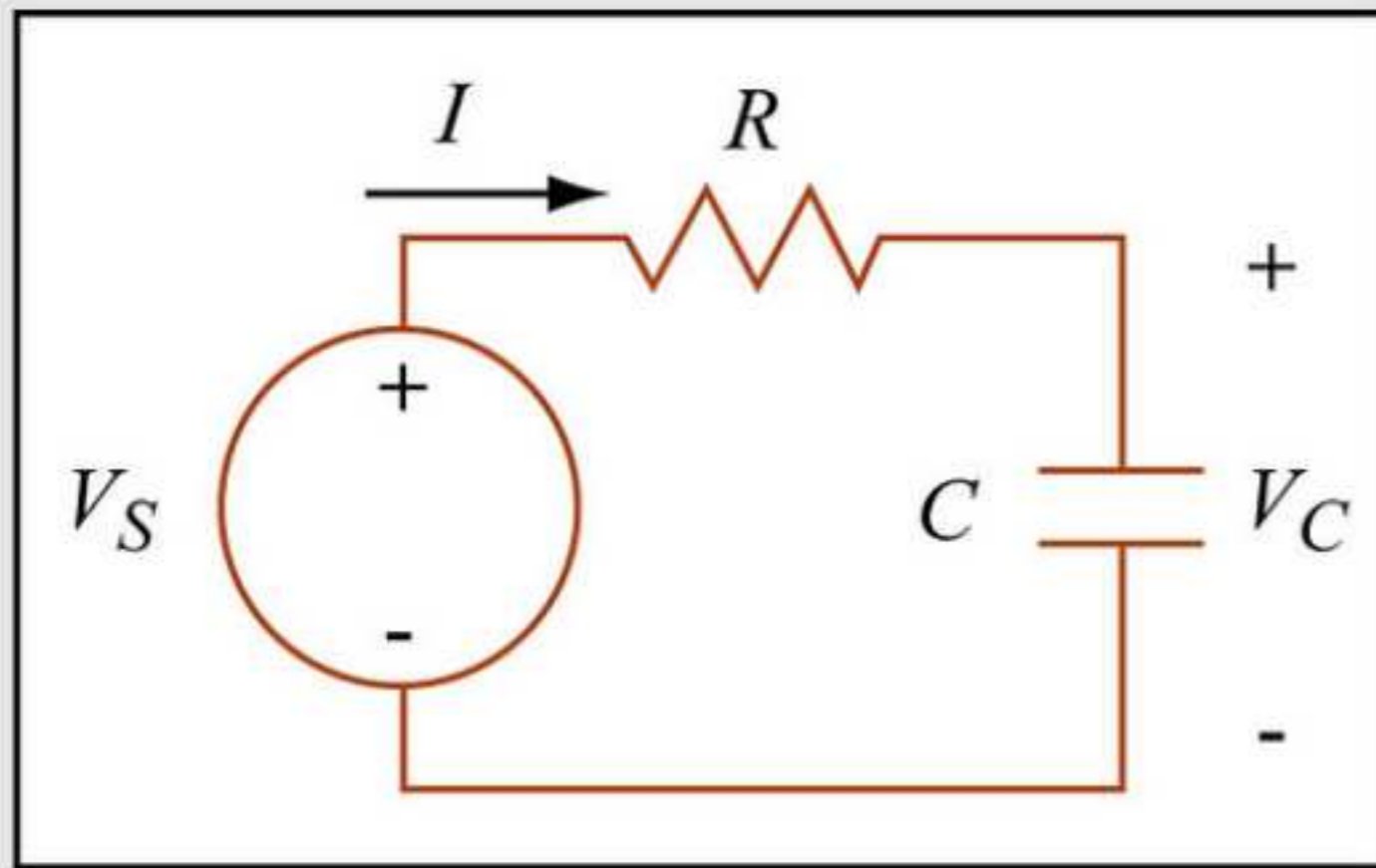
# Simpler Systems

- ... easier to understand and to work with

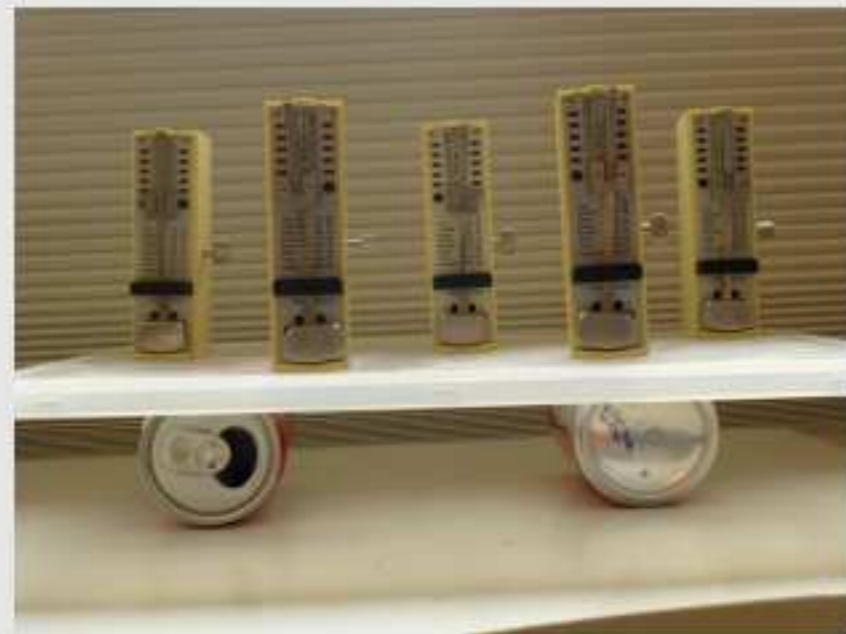


# Simpler Systems

- ... easier to understand and to work with



- Even small and simple systems can do interesting things



# A Note about Intuition vs Math

- Proper intuition: extremely important
  - quickly make **mental leaps** to solve problems and design new things
    - ... **avoiding confusion** that can arise from masses of detail

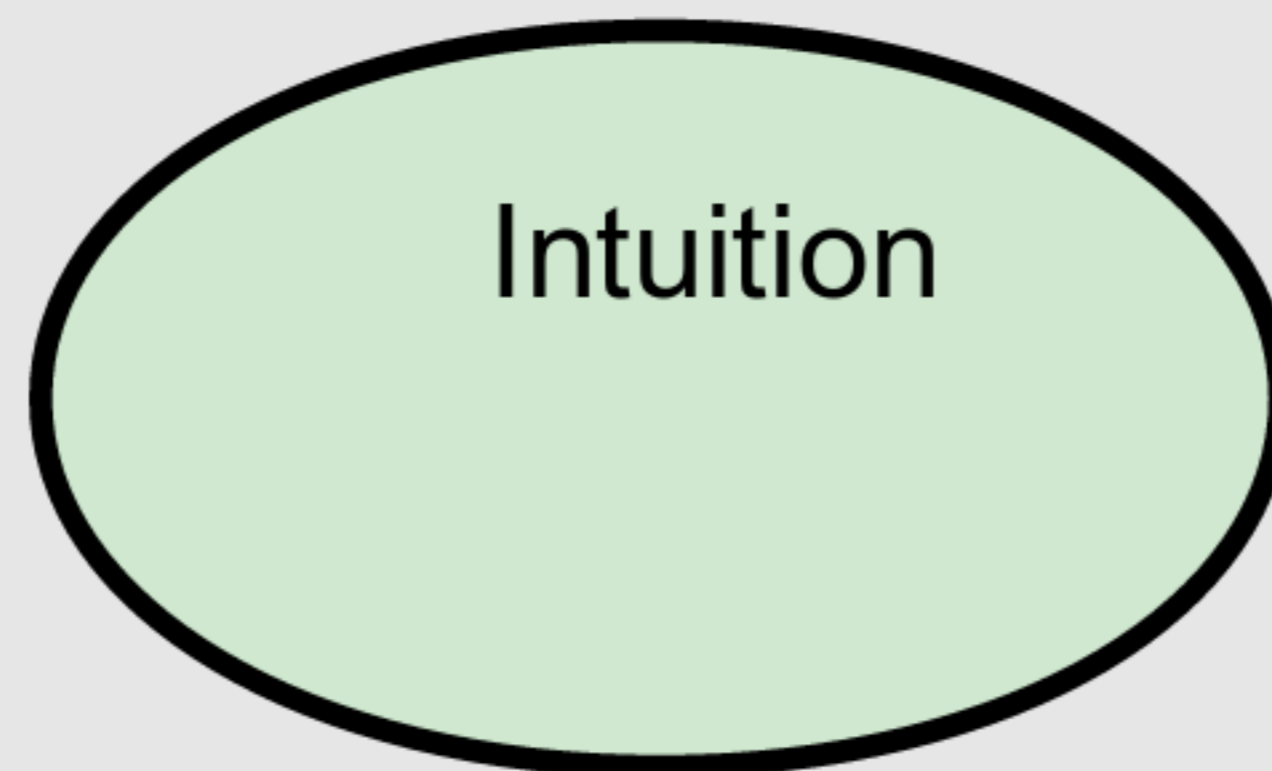
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- **Intuition doesn't arise magically**
  - mathematics: essential for **in-depth** understanding
    - math + experience and practice → intuition



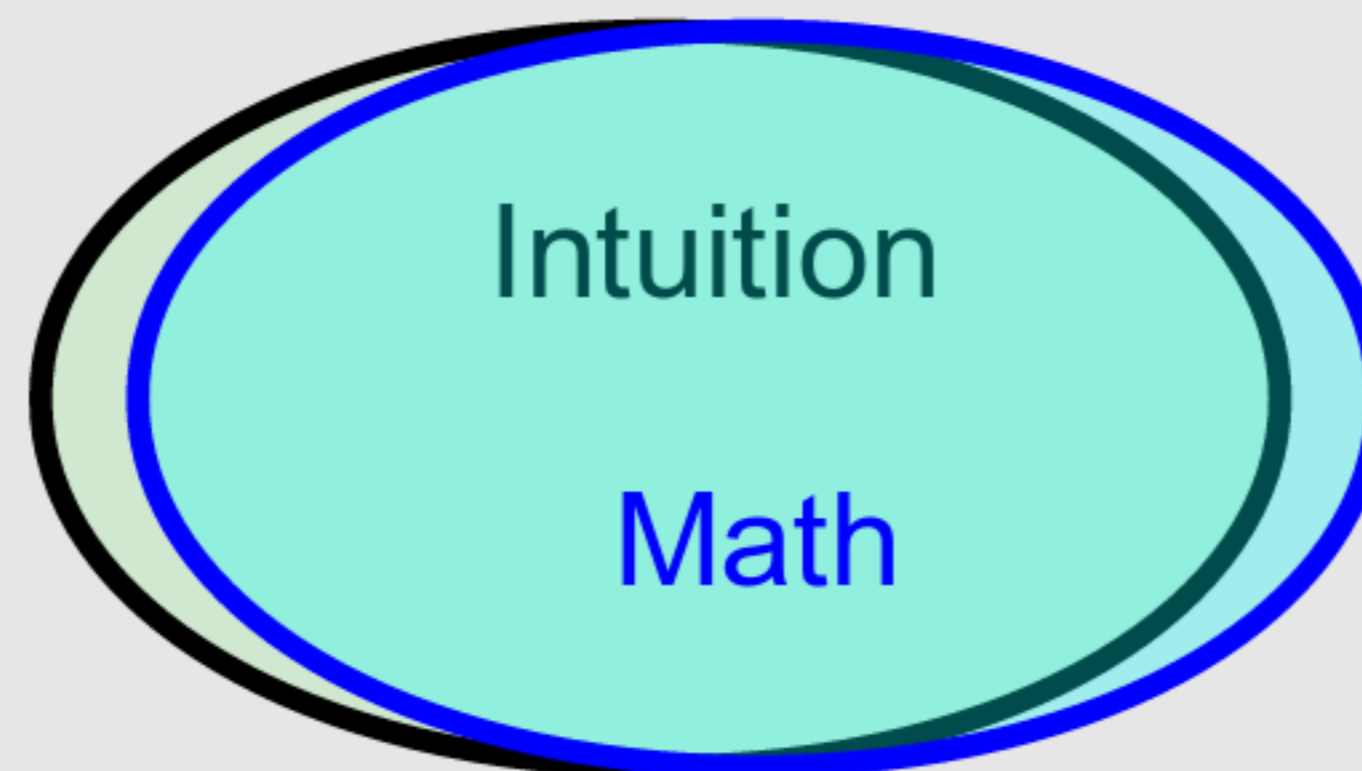
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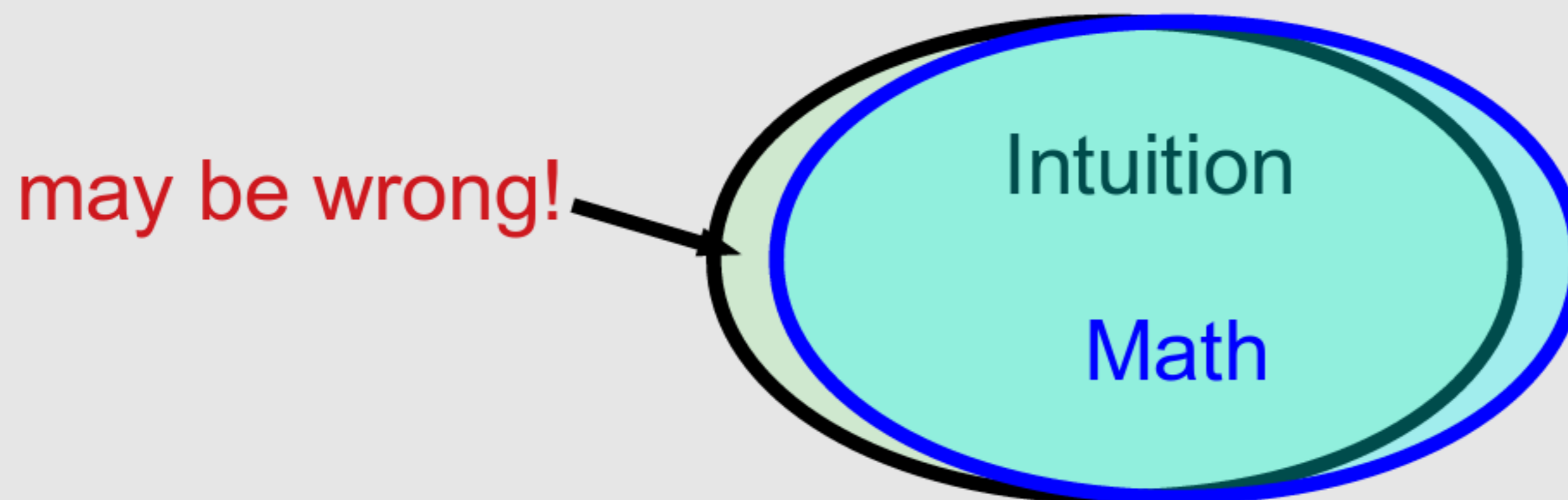
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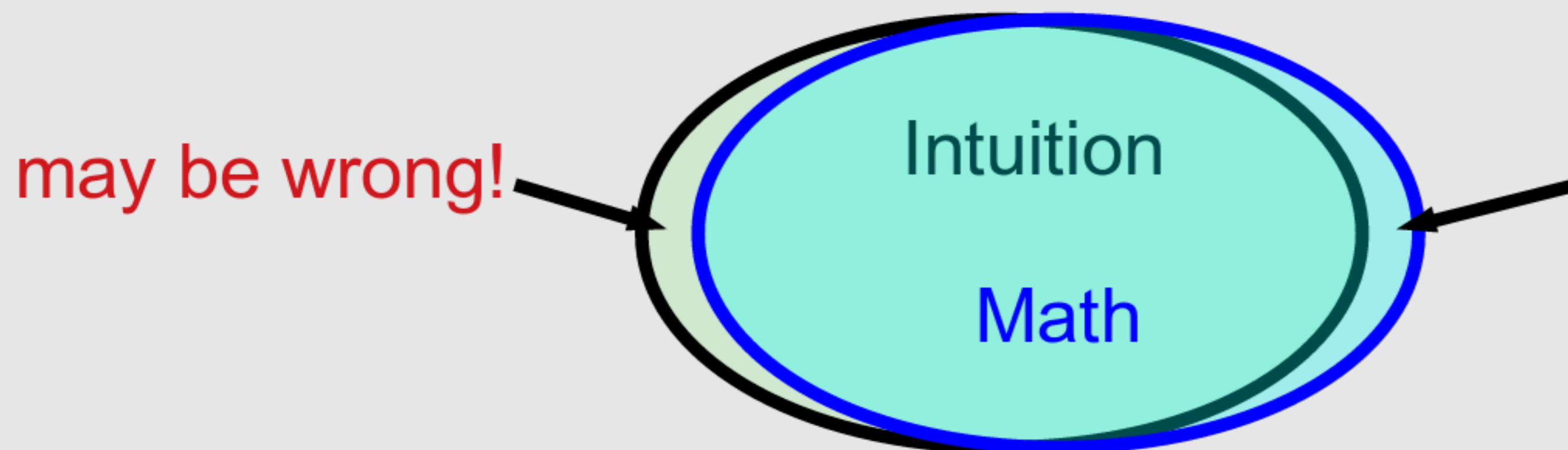
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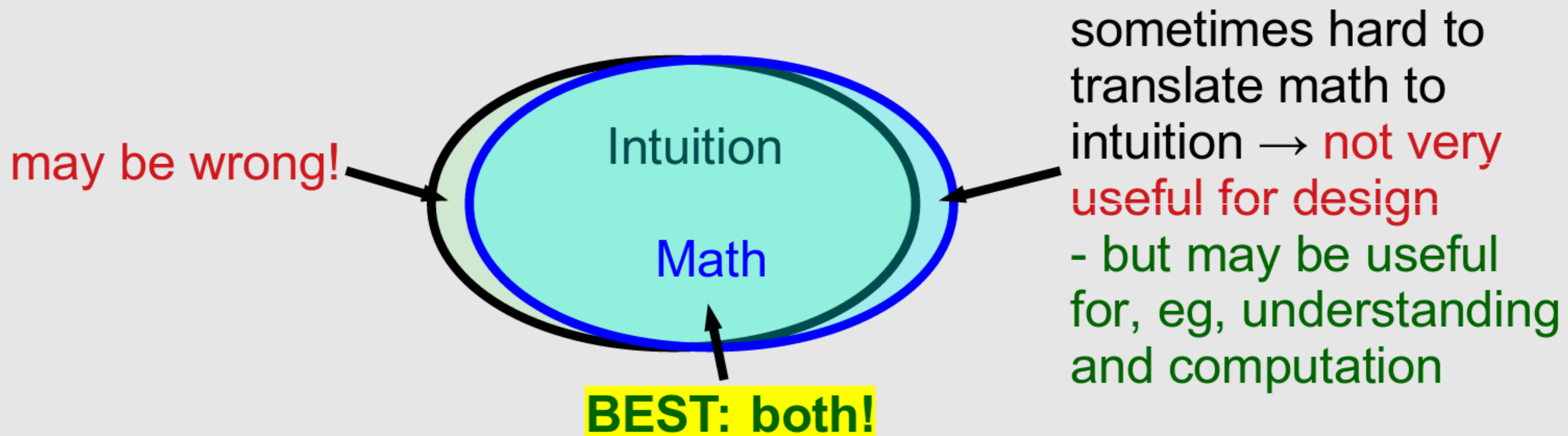
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sometimes hard to translate math to intuition → **not very useful for design** - but may be useful for, eg, understanding and computation

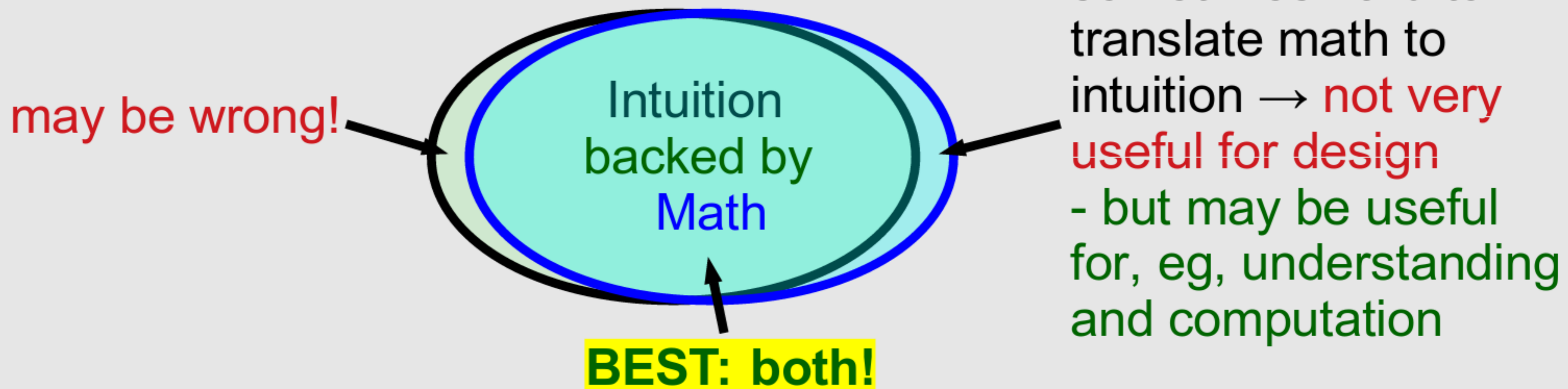
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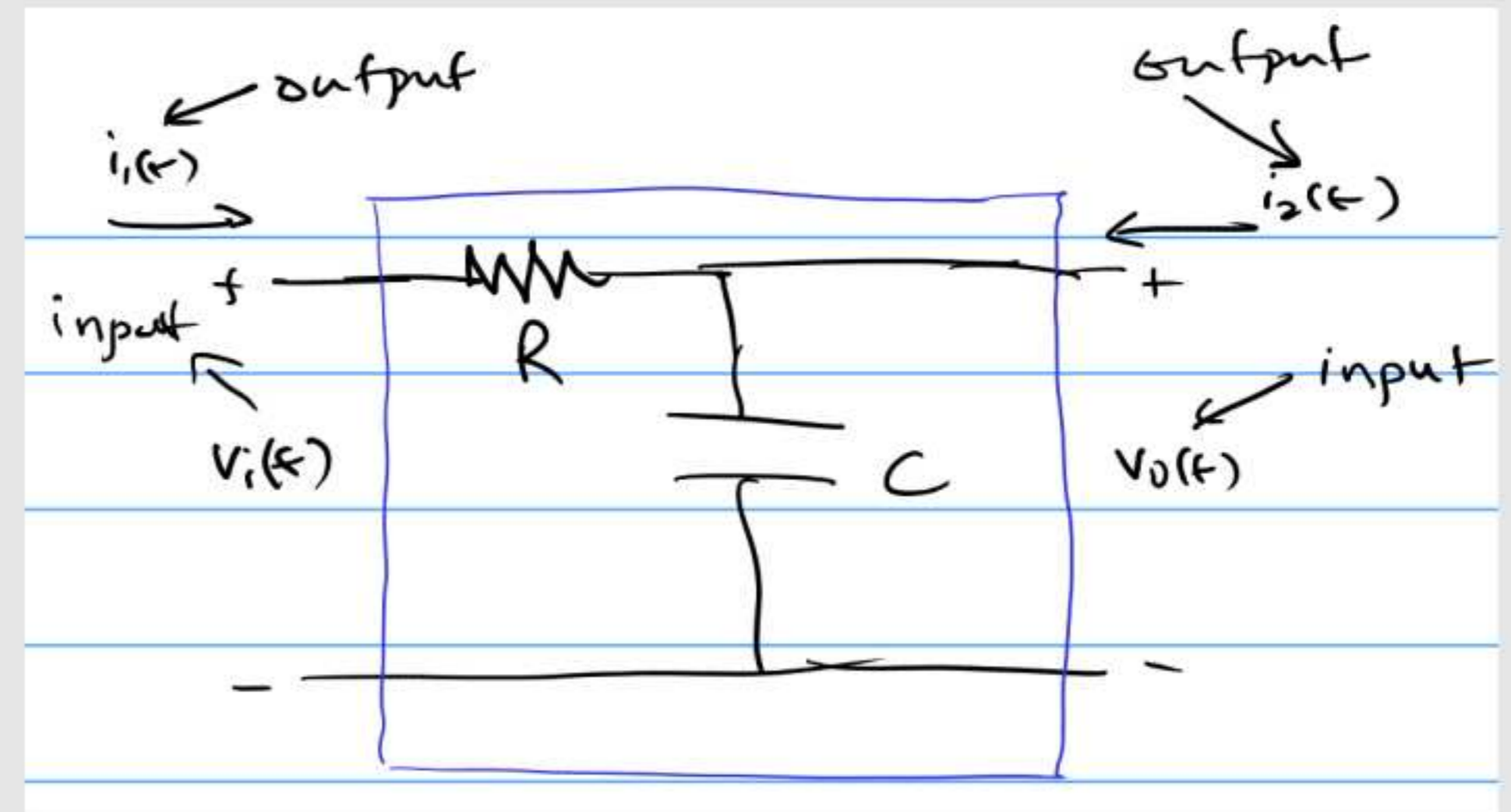
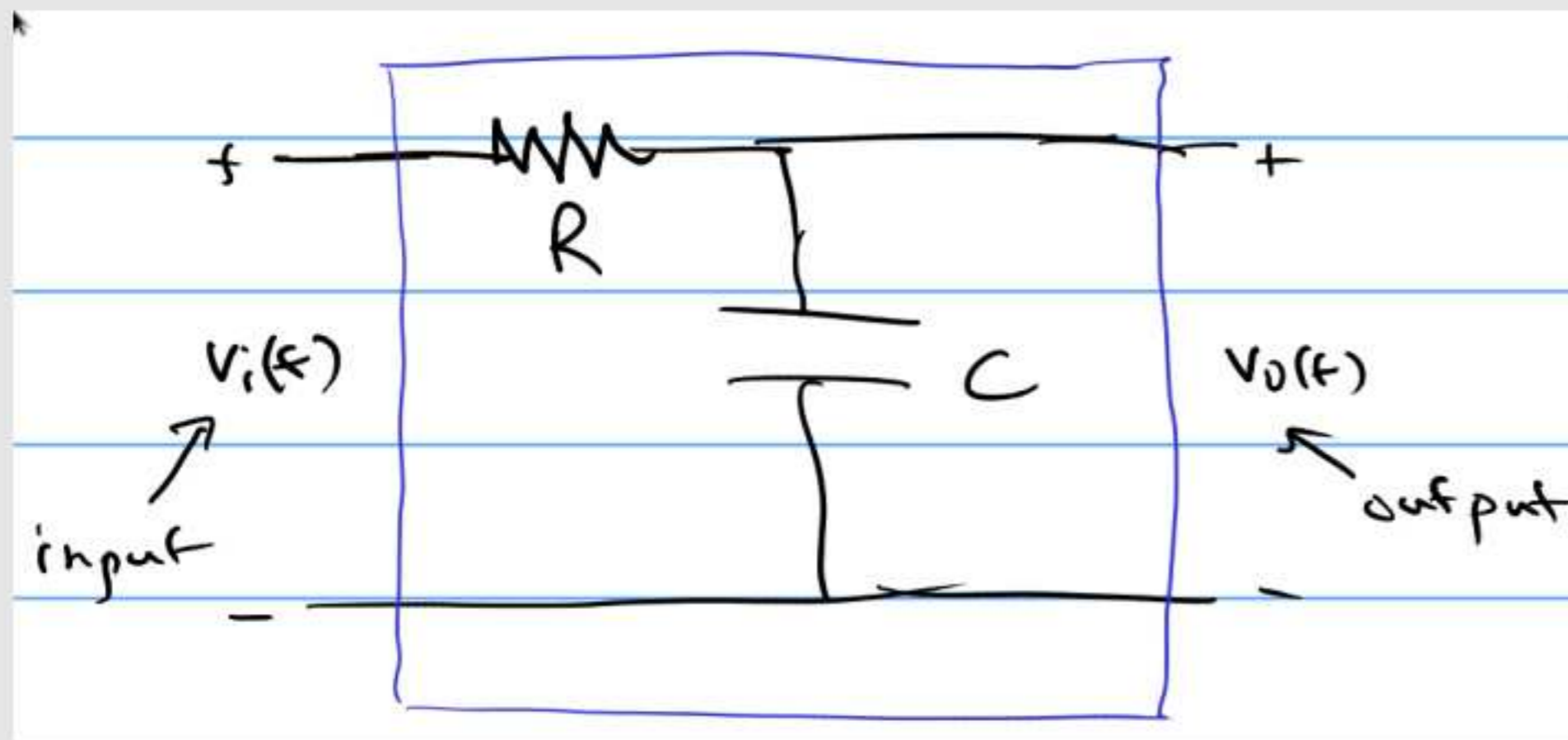
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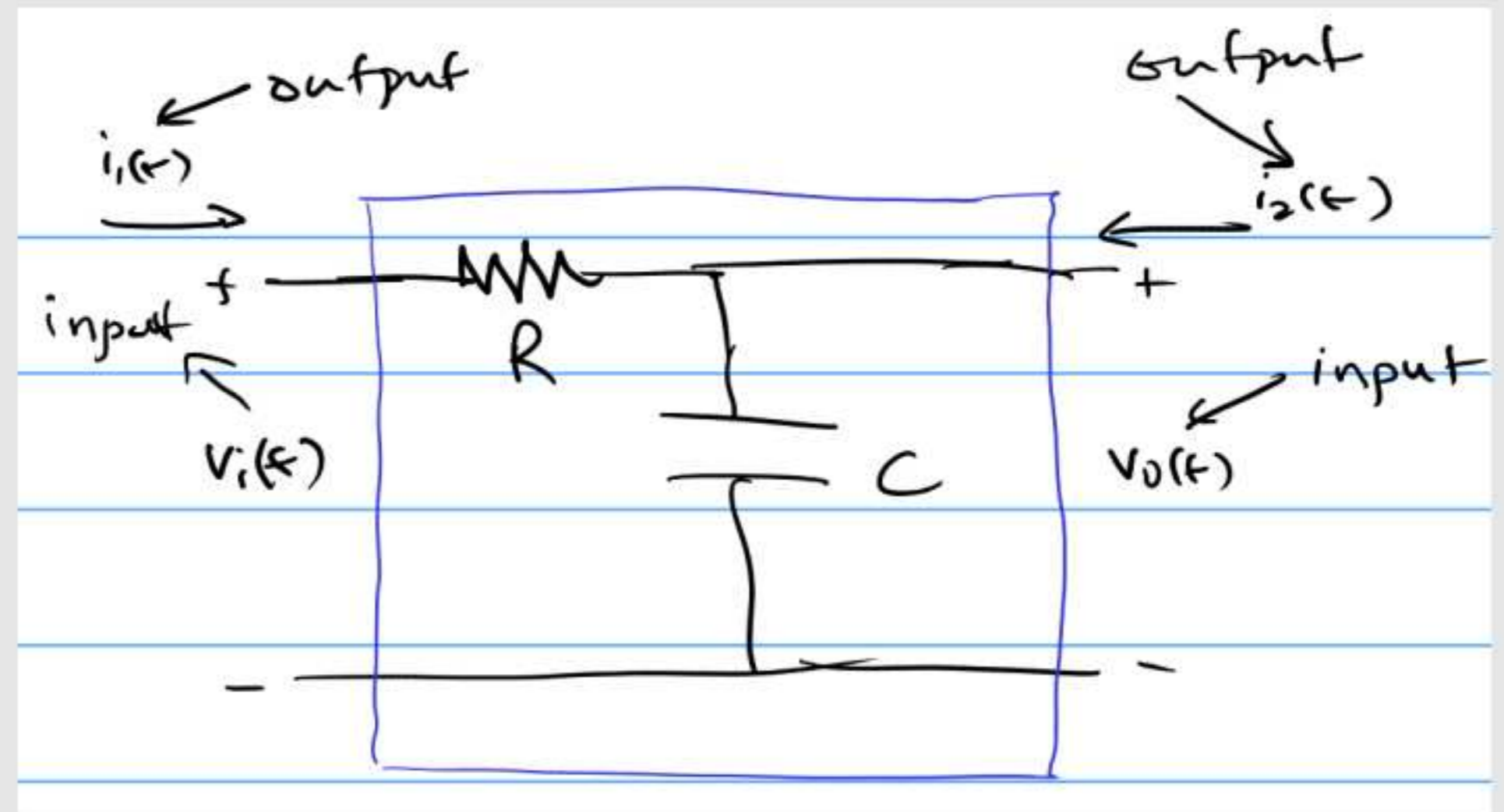
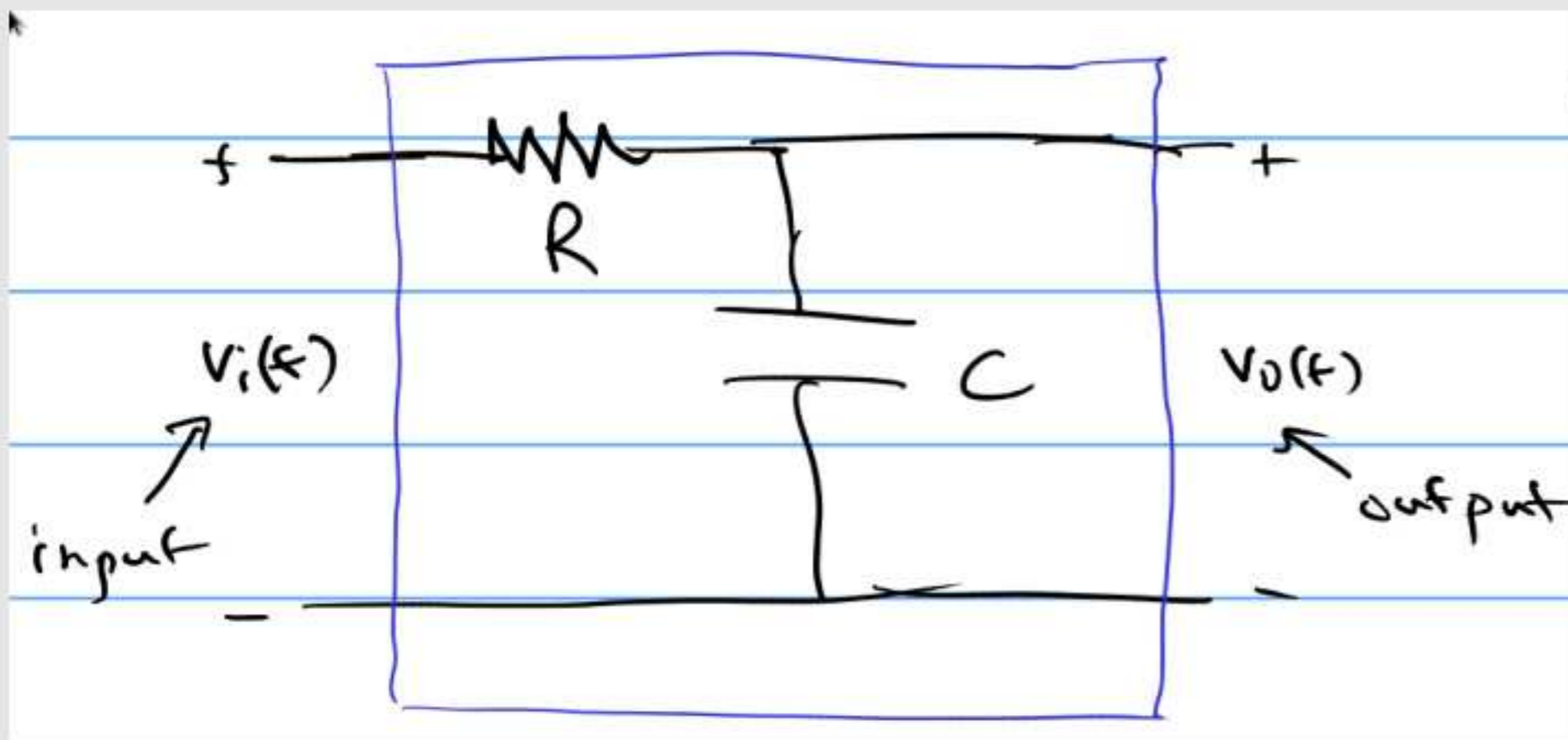


# Inputs and Outputs as **VECTORS**

- (move to xournal)



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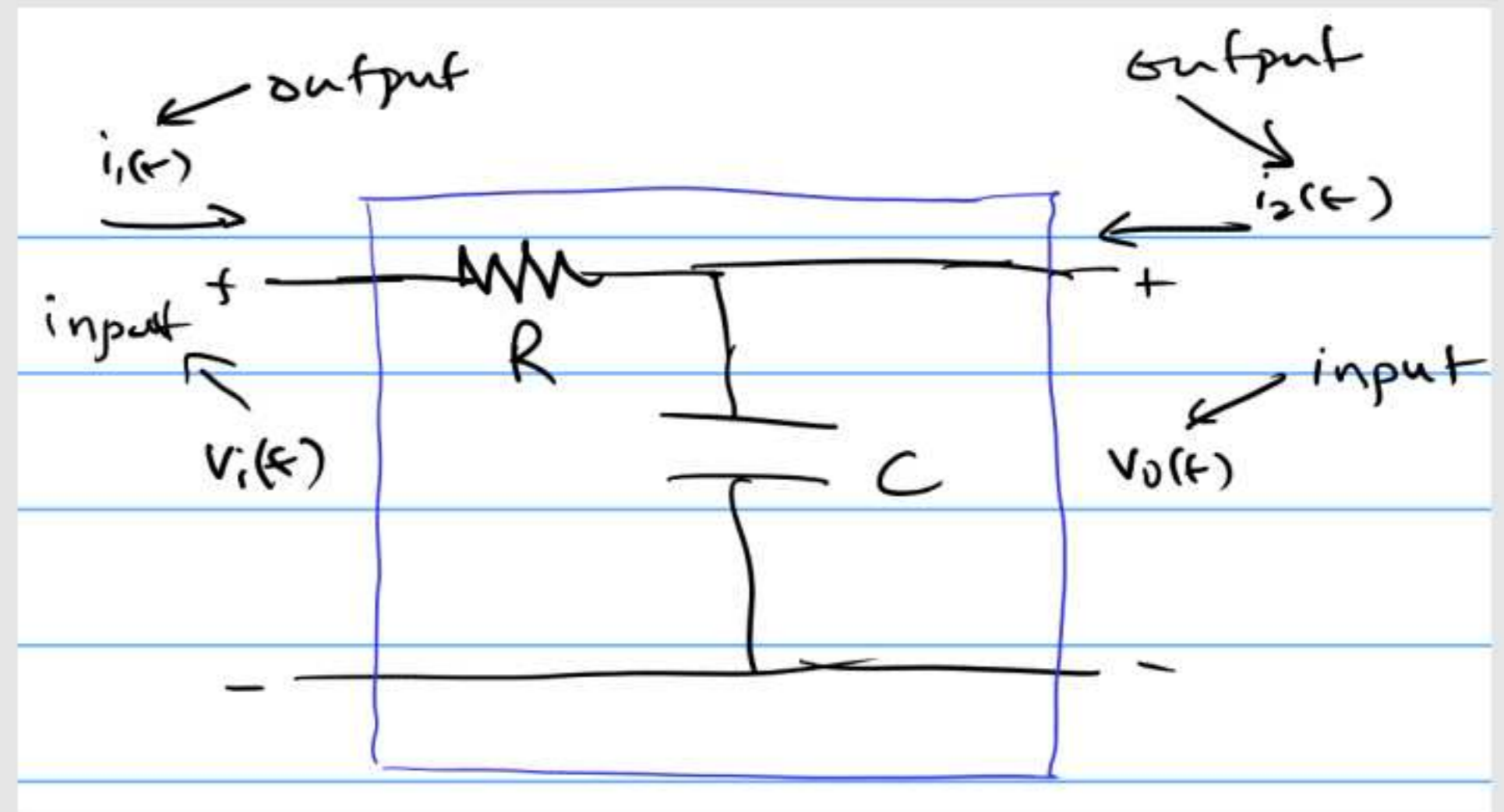
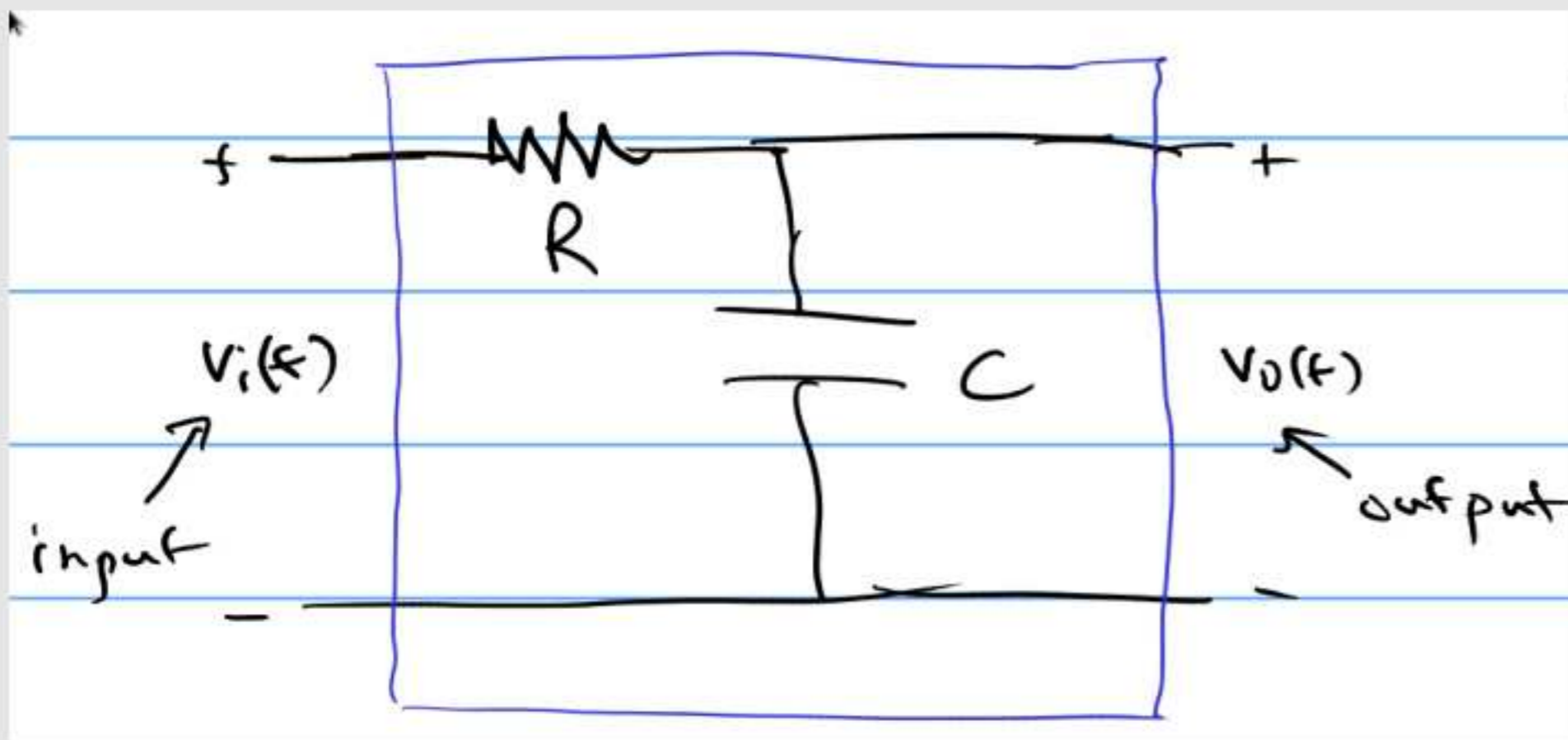


$$\vec{y}(t) = \begin{bmatrix} v_1(t) \\ v_2(t) \end{bmatrix}; \quad \vec{u}(t) = \begin{bmatrix} i_1(t) \\ i_2(t) \end{bmatrix}$$

vector of inputs
vector of outputs



# Inputs and Outputs as **VECTORS**



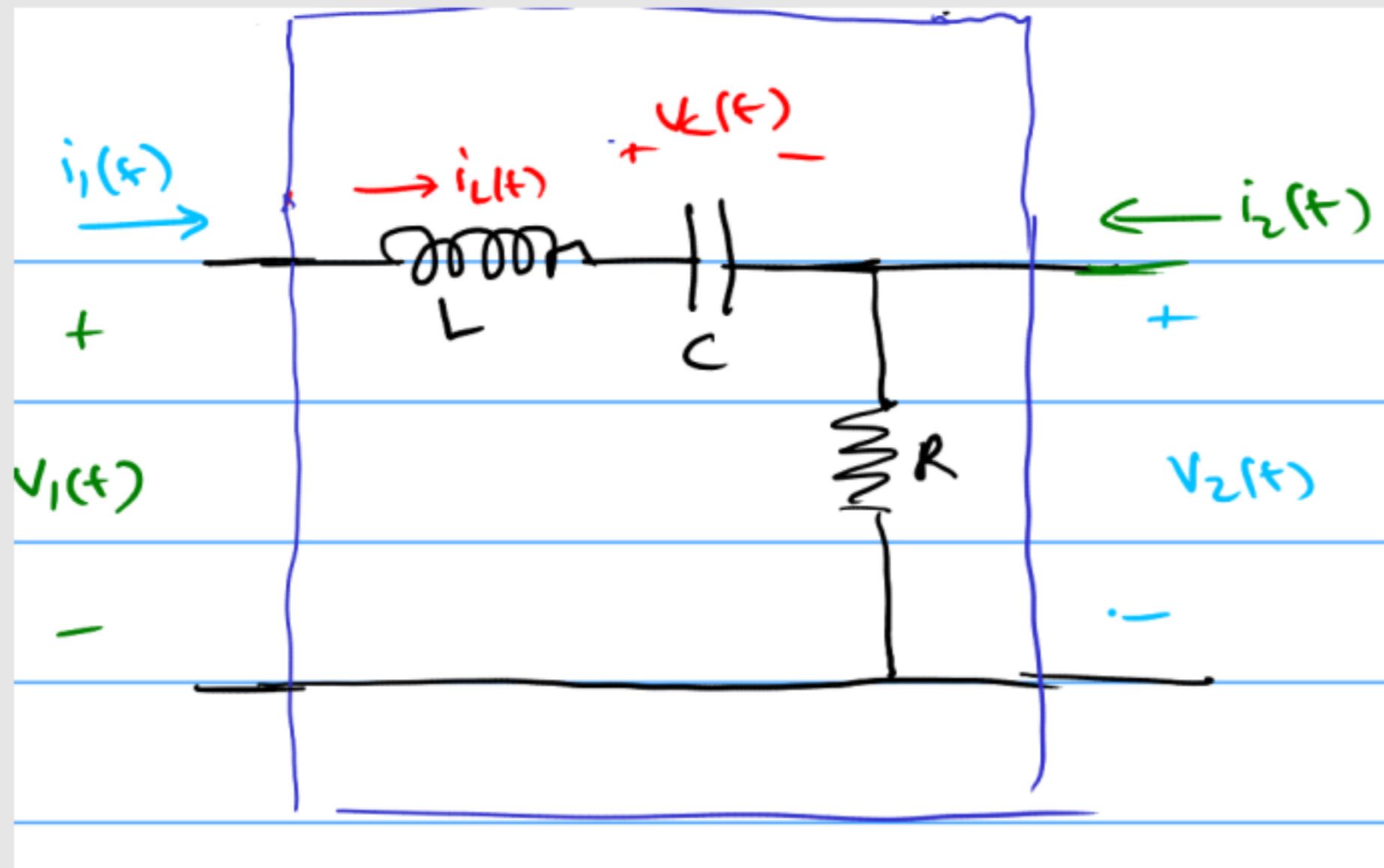
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Annotations: "vector of inputs" points to  $\vec{u}(t)$  and "vector of outputs" points to  $\vec{y}(t)$ .

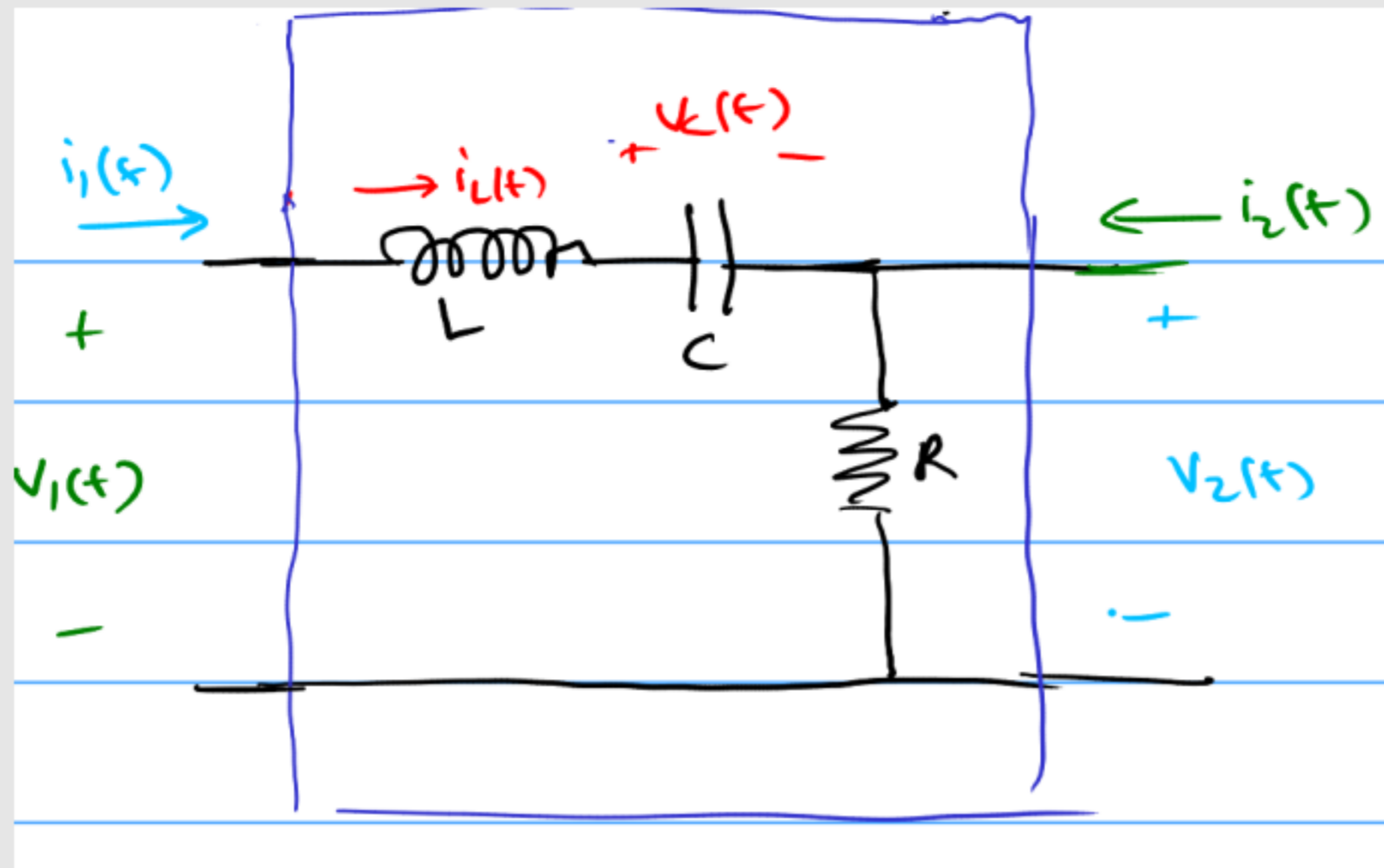
INPUTS AND OUTPUTS CAN BE ORGANIZED AS VECTORS

# The Internal State

- (move to xournal)



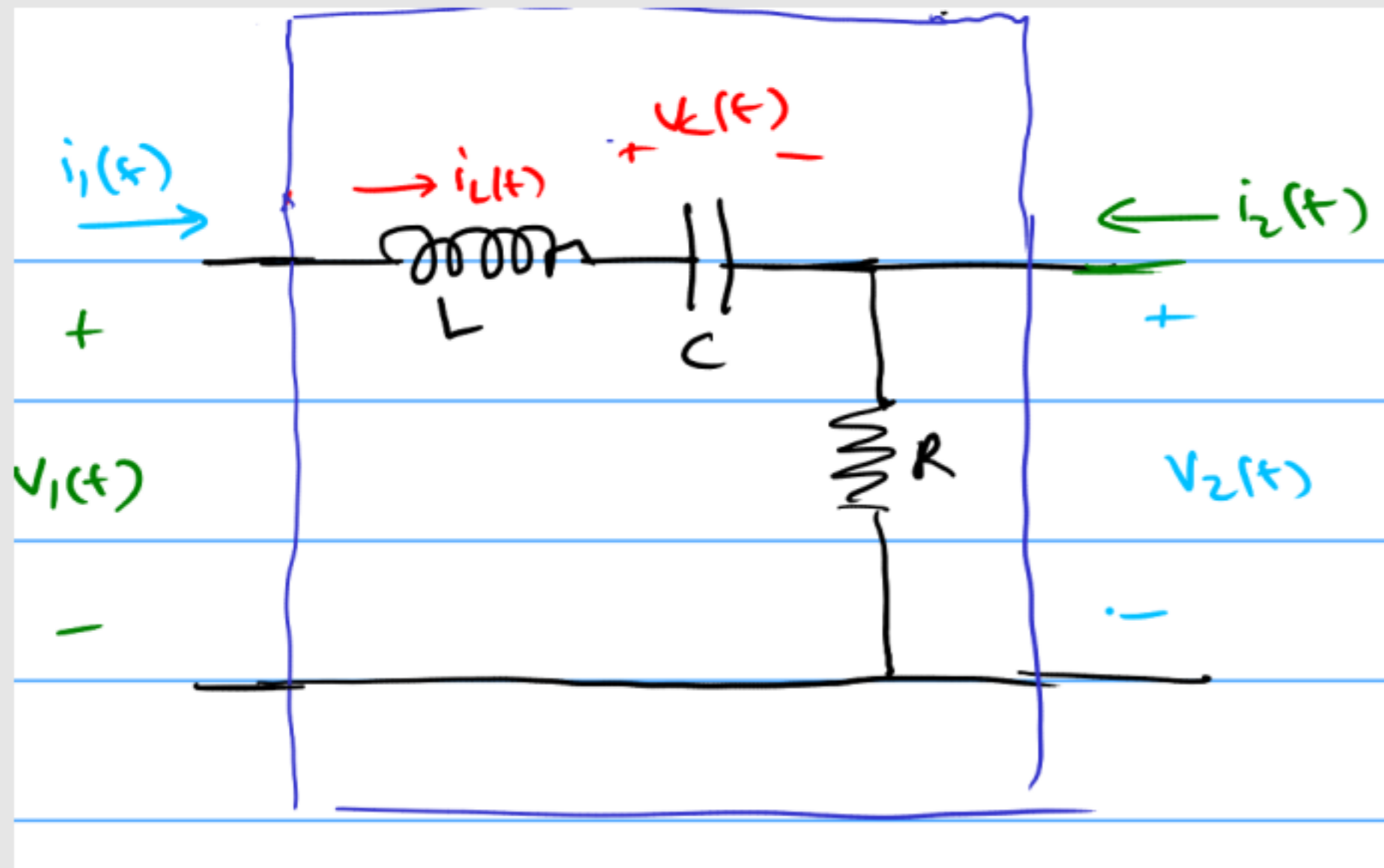
# The Internal State



$$\vec{w}(t) = \begin{bmatrix} v_1(t) \\ i_2(t) \end{bmatrix} \quad \vec{y}(t) = \begin{bmatrix} v_2(t) \\ i_1(t) \end{bmatrix}$$

$$\vec{x}(t) = \begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix}$$

# The Internal State



$$\vec{w}(t) = \begin{bmatrix} v_1(t) \\ i_2(t) \end{bmatrix} \quad \vec{y}(t) = \begin{bmatrix} v_2(t) \\ i_1(t) \end{bmatrix}$$

$$\vec{x}(t) = \begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix}$$

- Internal voltages/currents (unknowns): the **state**
  - also written as a vector:  $\vec{x}(t)$

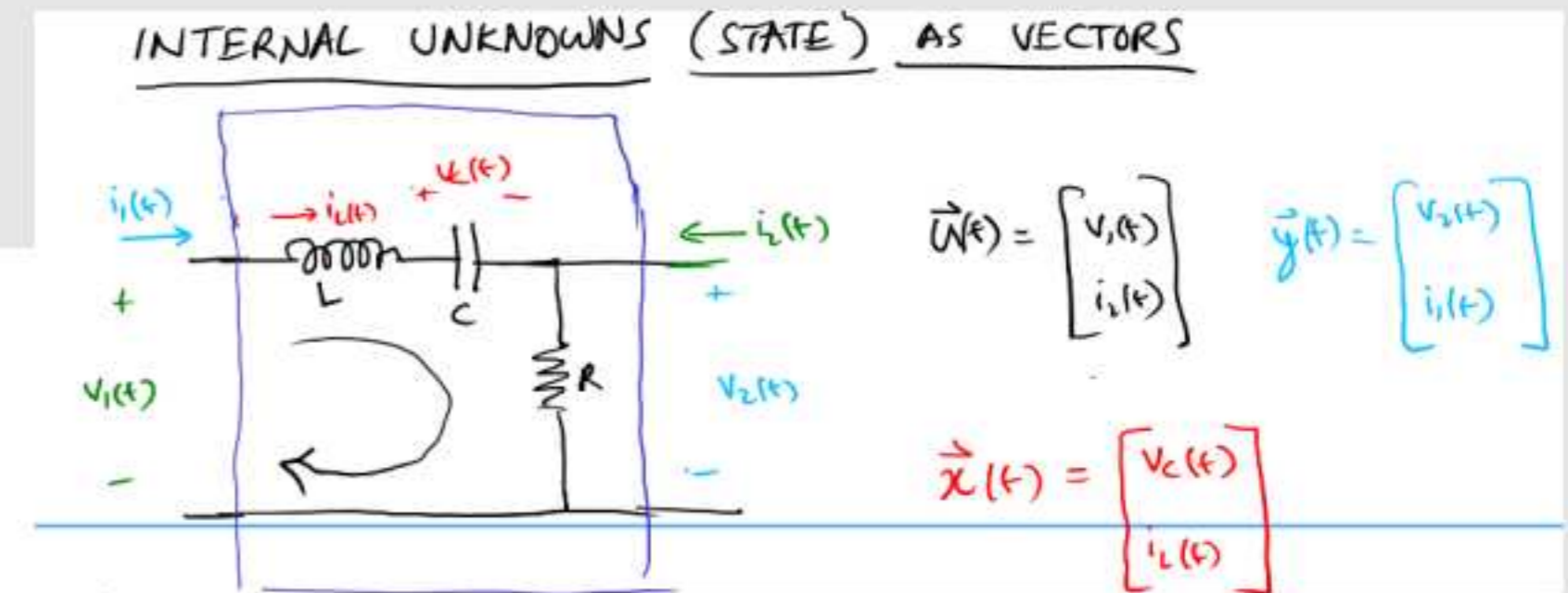
# The System's Equations

- (move to xournal)

## EQUATIONS

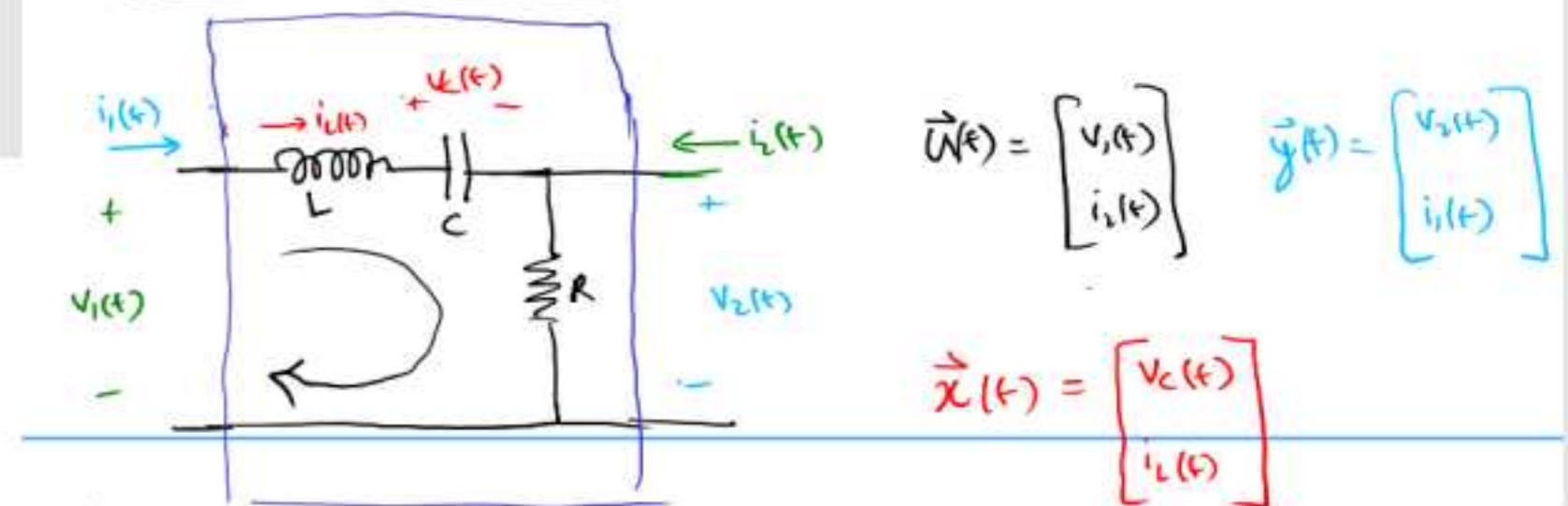
capacitor + KCL :  $C \frac{dv_c(t)}{dt} - i_L(t) = 0$

KVL :  $L \frac{di_L(t)}{dt} + v_c(t) + R(i_L(t) + i_2(t)) - v_1(t) = 0$



# The System's Equations

INTERNAL UNKNOWN(S) (STATE) AS VECTORS



## EQUATIONS

capacitor + KCL :  $C \frac{dv_C(t)}{dt} - i_L(t) = 0$

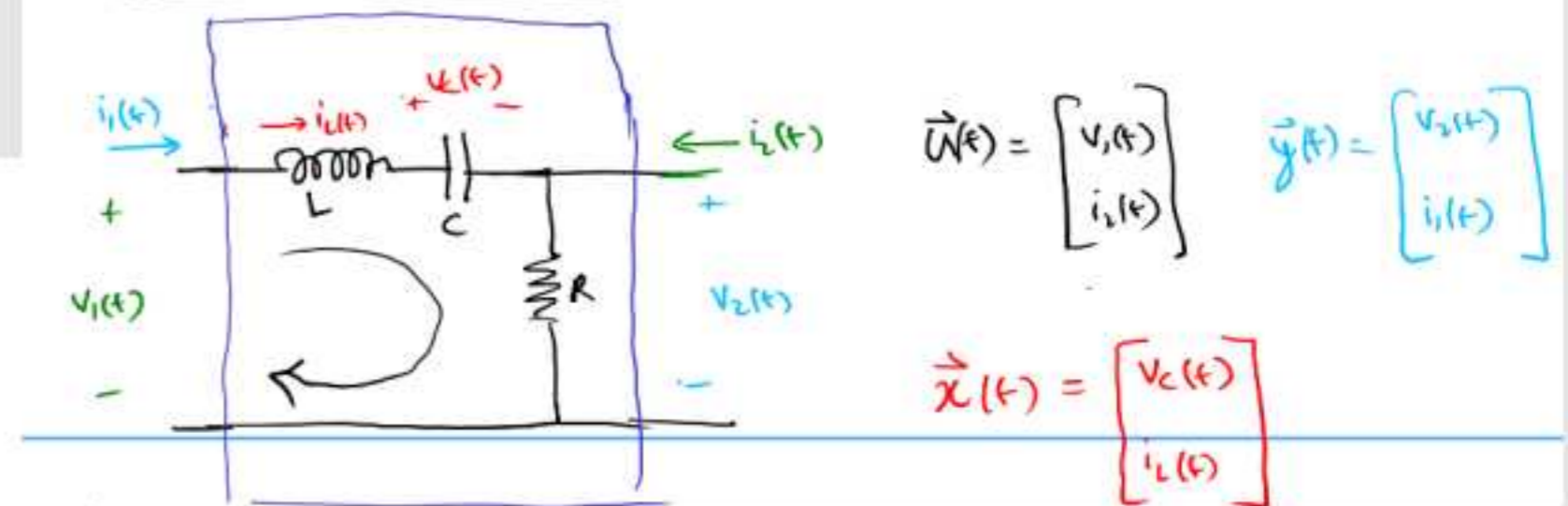
KVL :  $L \frac{di_L(t)}{dt} + v_C(t) + R(i_L(t) + i_2(t)) - v_1(t) = 0$

$$\underbrace{\begin{bmatrix} C & 0 \\ 0 & L \end{bmatrix}}_A \frac{d}{dt} \underbrace{\begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix}}_{\vec{x}(t)} + \underbrace{\begin{bmatrix} 0 & -1 \\ 1 & R \end{bmatrix}}_B \underbrace{\begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix}}_{\vec{x}(t)} + \underbrace{\begin{bmatrix} 0 & 0 \\ -1 & R \end{bmatrix}}_C \underbrace{\begin{bmatrix} v_1(t) \\ i_2(t) \end{bmatrix}}_{\vec{u}(t)} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$$\frac{d}{dt} \begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix} = \begin{bmatrix} 0 & 1/C \\ -1/L & -R/L \end{bmatrix} \begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix} + \begin{bmatrix} 0 & 0 \\ 1/L & -R/L \end{bmatrix} \begin{bmatrix} v_1(t) \\ i_2(t) \end{bmatrix}$$

# The System's Equations

INTERNAL UNKNOWN(S) (STATE) AS VECTORS



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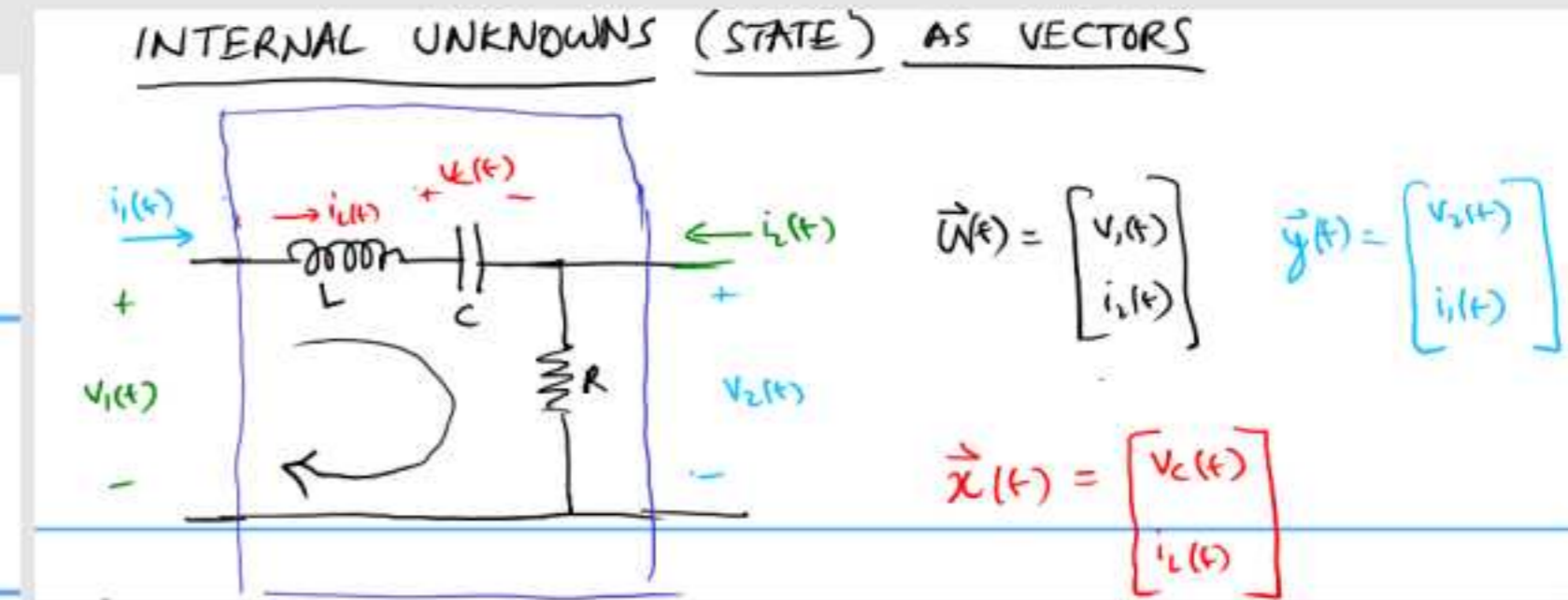
- can be written using the input and state vectors

# The Outputs

- (move to xournal)

$$v_2(t) = R(i_L(t) + i_2(t))$$

$$i_1(t) = i_L(t)$$

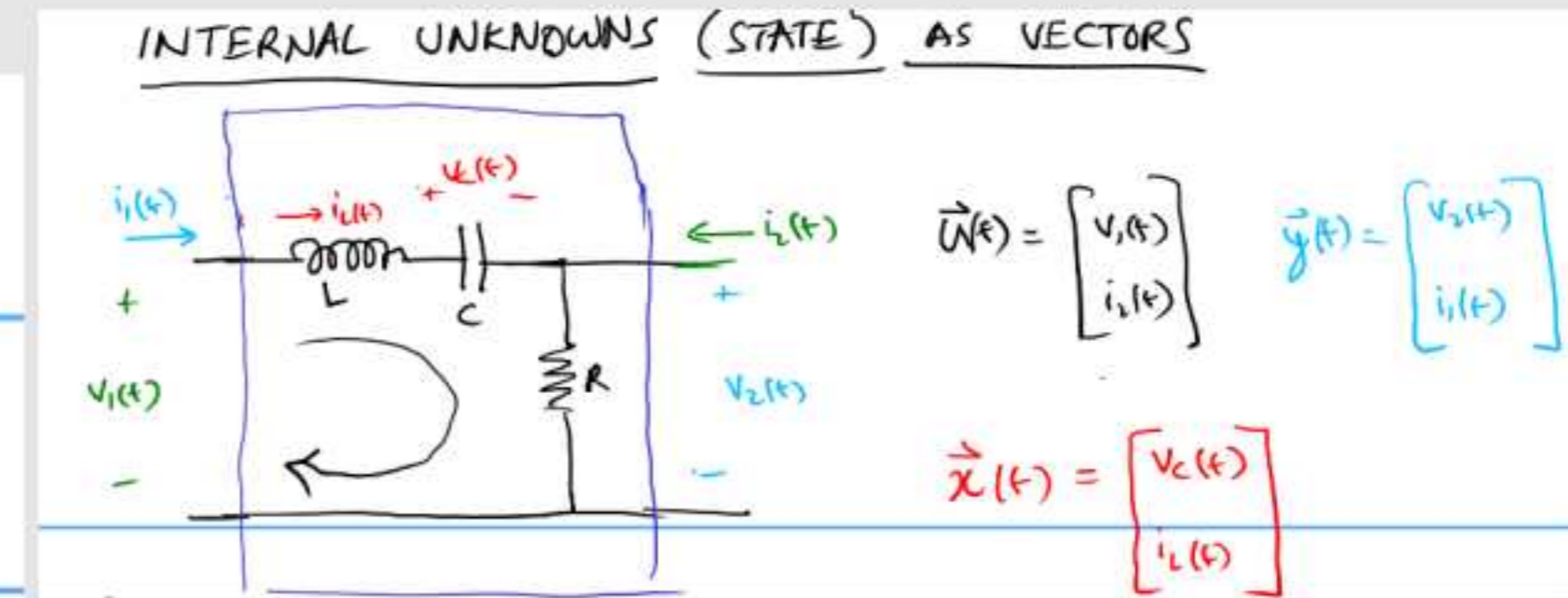




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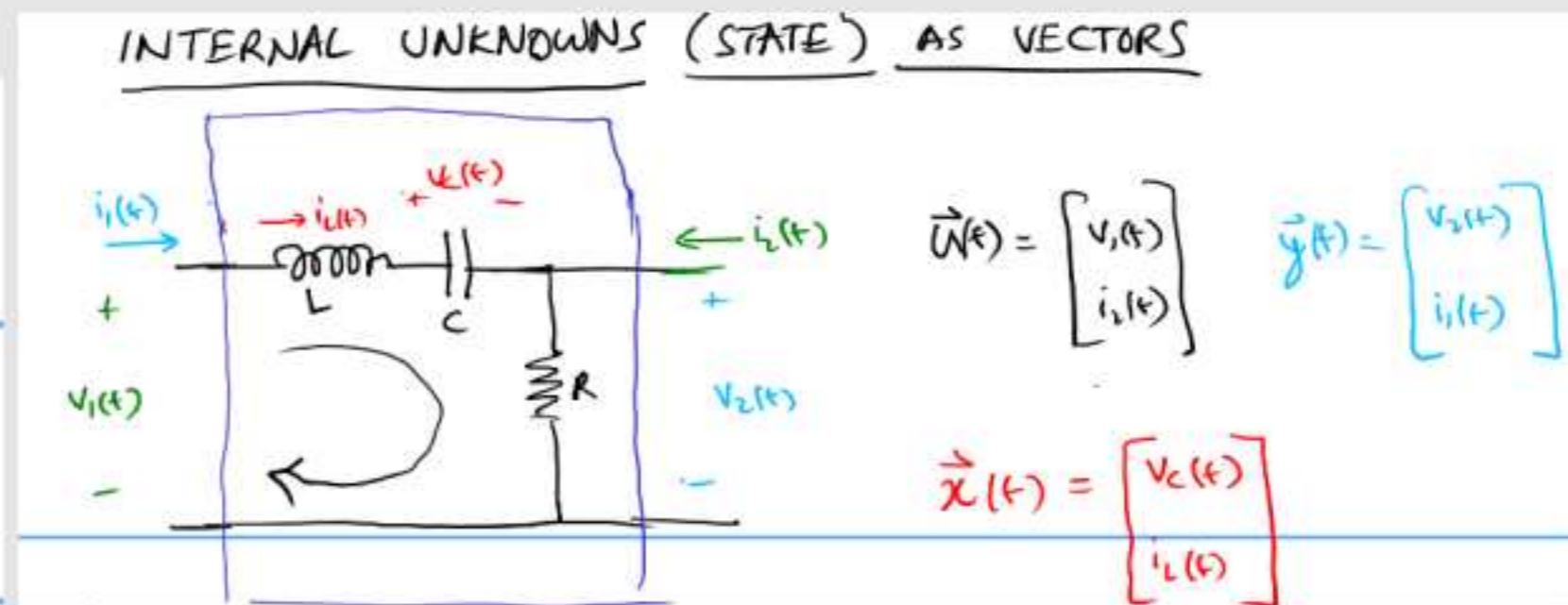


$$\vec{y}(t) = \underbrace{\begin{bmatrix} 0 & R \\ 0 & 1 \end{bmatrix}}_D \vec{x}(t) + \underbrace{\begin{bmatrix} 0 & R \\ 0 & 0 \end{bmatrix}}_F \vec{u}(t)$$

# The Outputs

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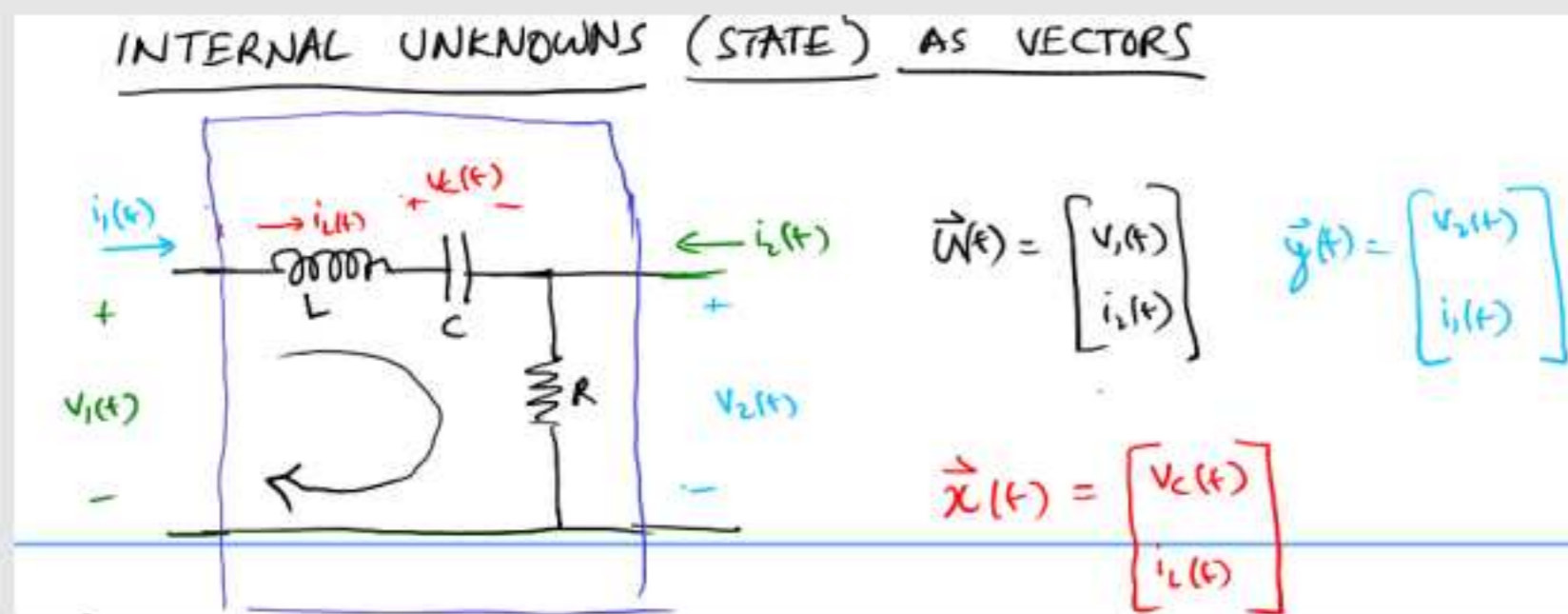


$$\vec{y}(t) = \underbrace{\begin{bmatrix} 0 & R \\ 0 & 1 \end{bmatrix}}_D \vec{x}(t) + \underbrace{\begin{bmatrix} 0 & R \\ 0 & 0 \end{bmatrix}}_E \vec{w}(t)$$

- also expressed using the **input** and **state vectors**

# State+Output Eqns Together

$$\frac{d}{dt} \begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix} = \begin{bmatrix} 0 & 1/L \\ -1/L & -R/L \end{bmatrix} \begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix} + \begin{bmatrix} 1/L \\ -R/L \end{bmatrix} \begin{bmatrix} v_1(t) \\ i_2(t) \end{bmatrix}$$

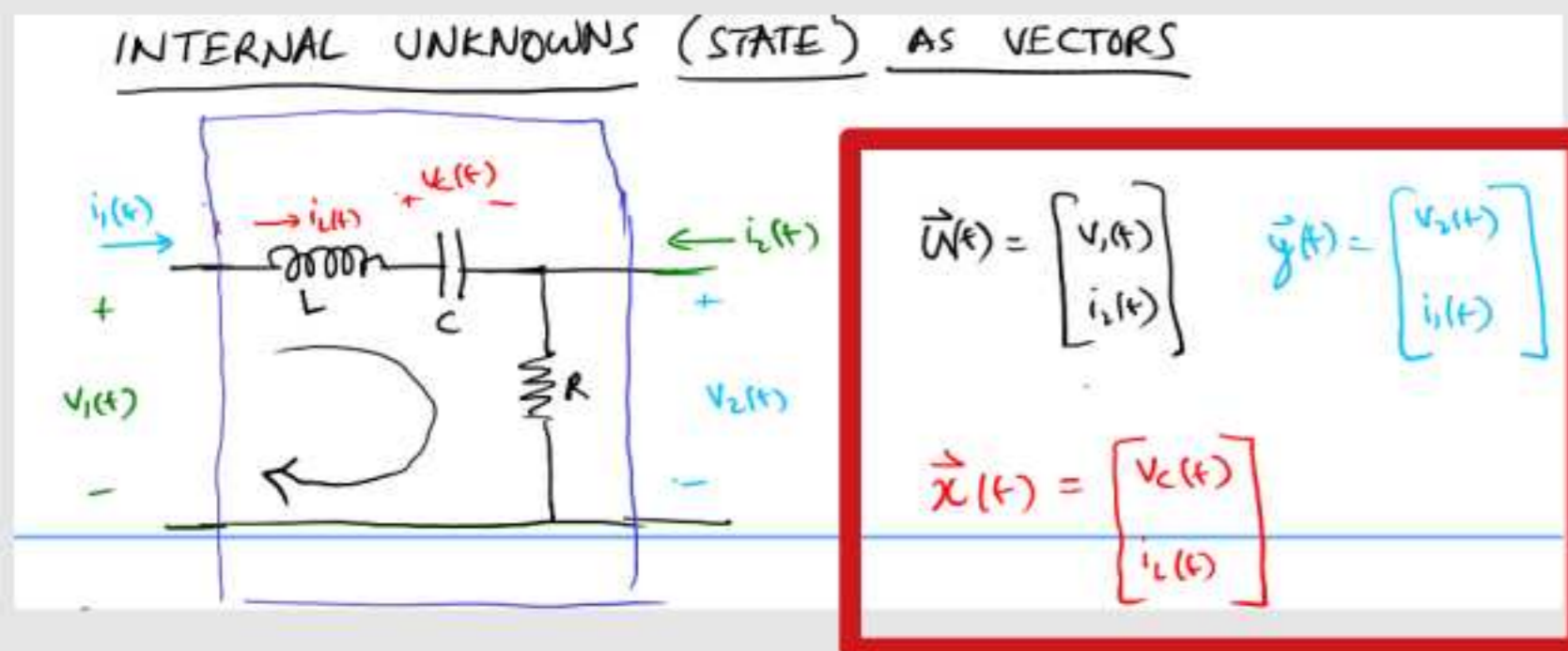


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- **general form:**  $\frac{d}{dt} \vec{x}(t) = \vec{f}(\vec{x}(t), \vec{u}(t))$ ,  $\vec{y}(t) = \vec{g}(\vec{x}(t), \vec{u}(t))$

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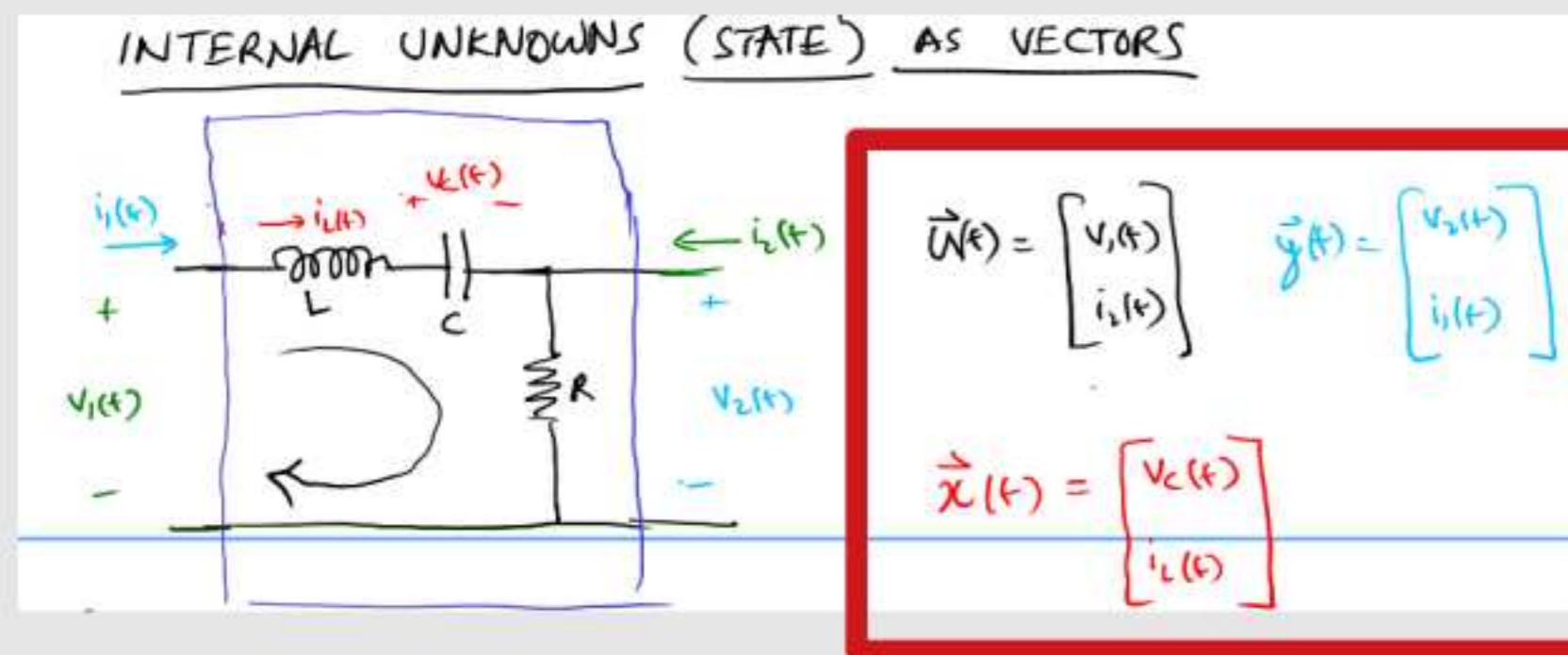


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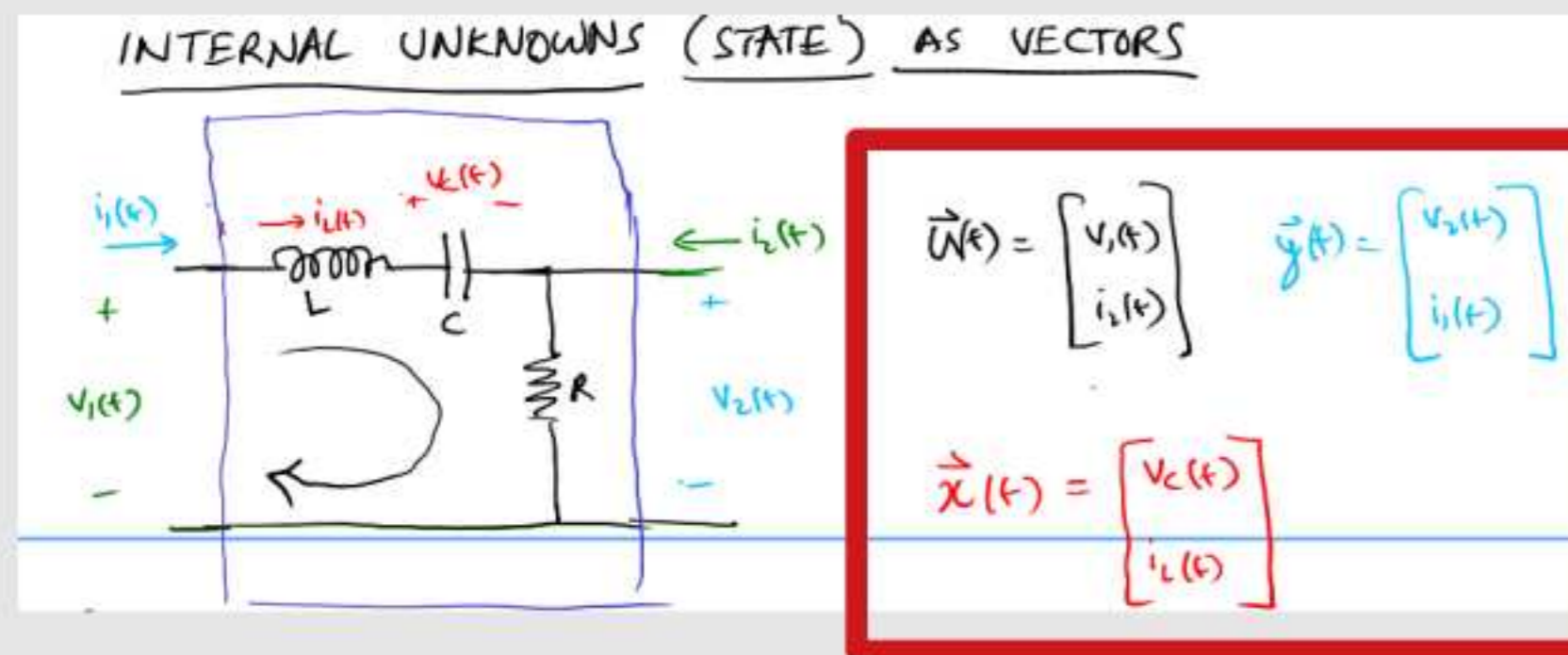


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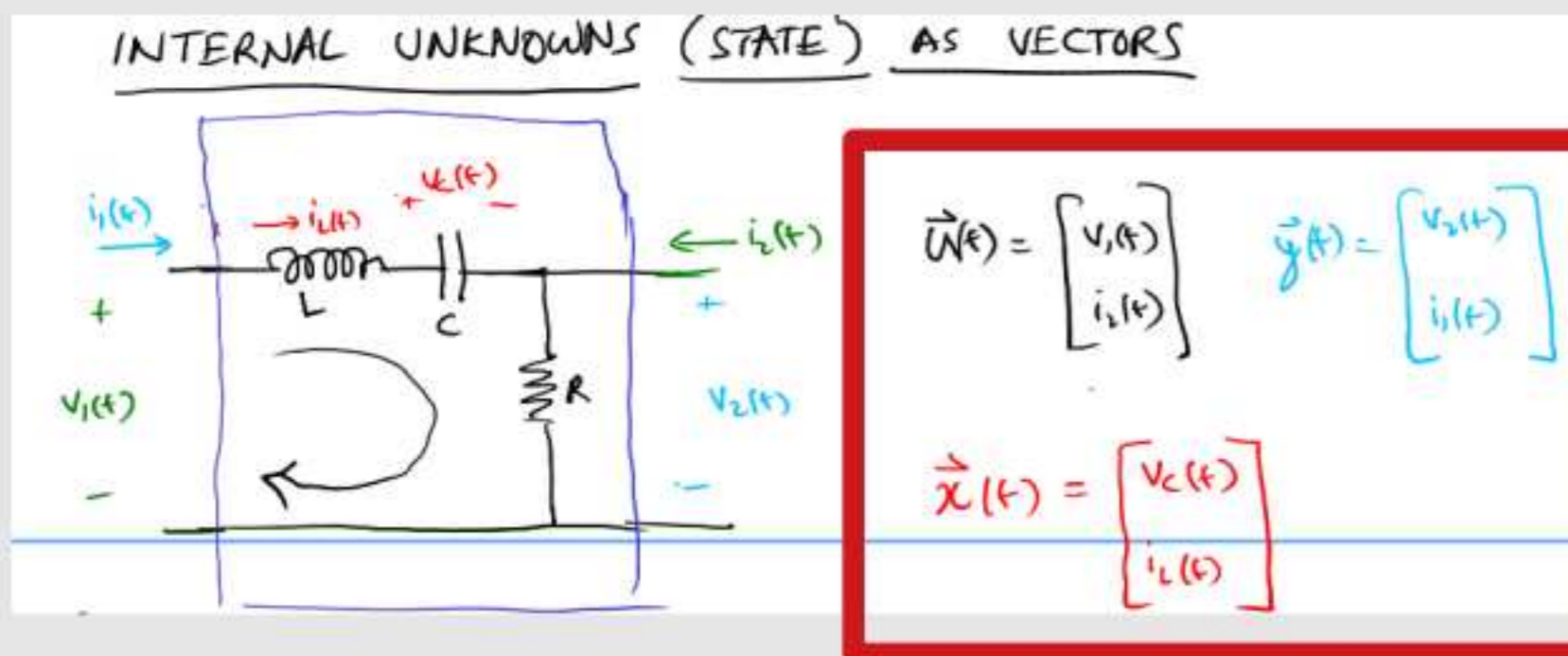
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 + initial condition (IC)

# State+Output Eqns Together

$$\frac{d}{dt} \begin{bmatrix} v_L(t) \\ i_L(t) \end{bmatrix} = \begin{bmatrix} \vdots & 1/C \\ -1/L & -R/L \end{bmatrix} \begin{bmatrix} v_L(t) \\ i_L(t) \end{bmatrix} + \begin{bmatrix} \vdots \\ 1/L \end{bmatrix} \begin{bmatrix} v_1(t) \\ i_2(t) \end{bmatrix}$$

$\xleftarrow{\vec{f}(\vec{x}, \vec{u})}$        $\vec{g}(\vec{x}, \vec{u})$



$$\vec{y}(t) = \underbrace{\begin{bmatrix} 0 & R \\ 0 & 1 \end{bmatrix}}_D \underbrace{\begin{bmatrix} v_L(t) \\ i_L(t) \end{bmatrix}}_{\vec{x}(t)} + \underbrace{\begin{bmatrix} 0 & R \\ 0 & 0 \end{bmatrix}}_E \underbrace{\begin{bmatrix} v_1(t) \\ i_2(t) \end{bmatrix}}_{\vec{u}(t)}$$

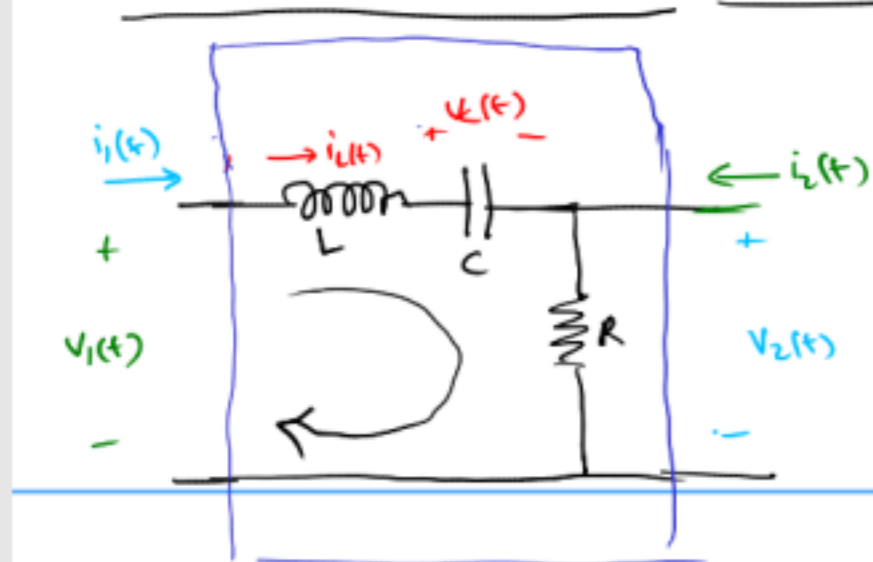
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 + initial condition (IC)

**STATE SPACE FORMULATION**

# State+Output Eqns Together

$$\frac{d}{dt} \begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix} = \underbrace{\begin{bmatrix} 0 & 1/C \\ -1/L & -R/L \end{bmatrix}}_{\vec{f}(\vec{x}, \vec{u})} \begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix} + \underbrace{\begin{bmatrix} 1/L \\ -R/L \end{bmatrix}}_{\vec{g}(\vec{x}, \vec{u})} \begin{bmatrix} v_1(t) \\ i_2(t) \end{bmatrix}$$

INTERNAL UNKNOWN(S) (STATE) AS VECTORS

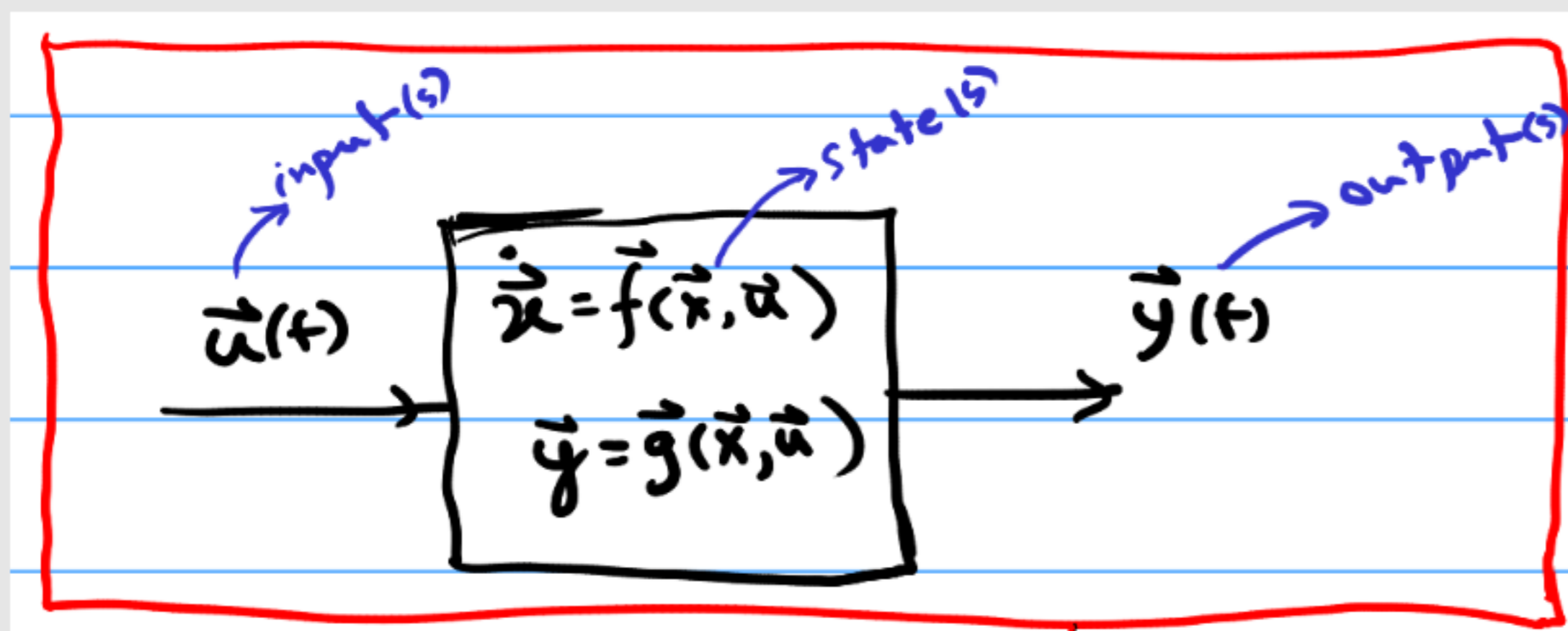


$$\vec{u}(t) = \begin{bmatrix} v_1(t) \\ i_2(t) \end{bmatrix} \quad \vec{y}(t) = \begin{bmatrix} v_2(t) \\ i_1(t) \end{bmatrix}$$

$$\vec{x}(t) = \begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix}$$

$$\vec{y}(t) = \underbrace{\begin{bmatrix} 0 & R \\ 0 & 1 \end{bmatrix}}_D \begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix} + \underbrace{\begin{bmatrix} 0 & R \\ 0 & 0 \end{bmatrix}}_E \begin{bmatrix} v_1(t) \\ i_2(t) \end{bmatrix}$$

- **general form:**  $\frac{d}{dt} \vec{x}(t) = \vec{f}(\vec{x}(t), \vec{u}(t)), \quad \vec{y}(t) = \vec{g}(\vec{x}(t), \vec{u}(t))$   
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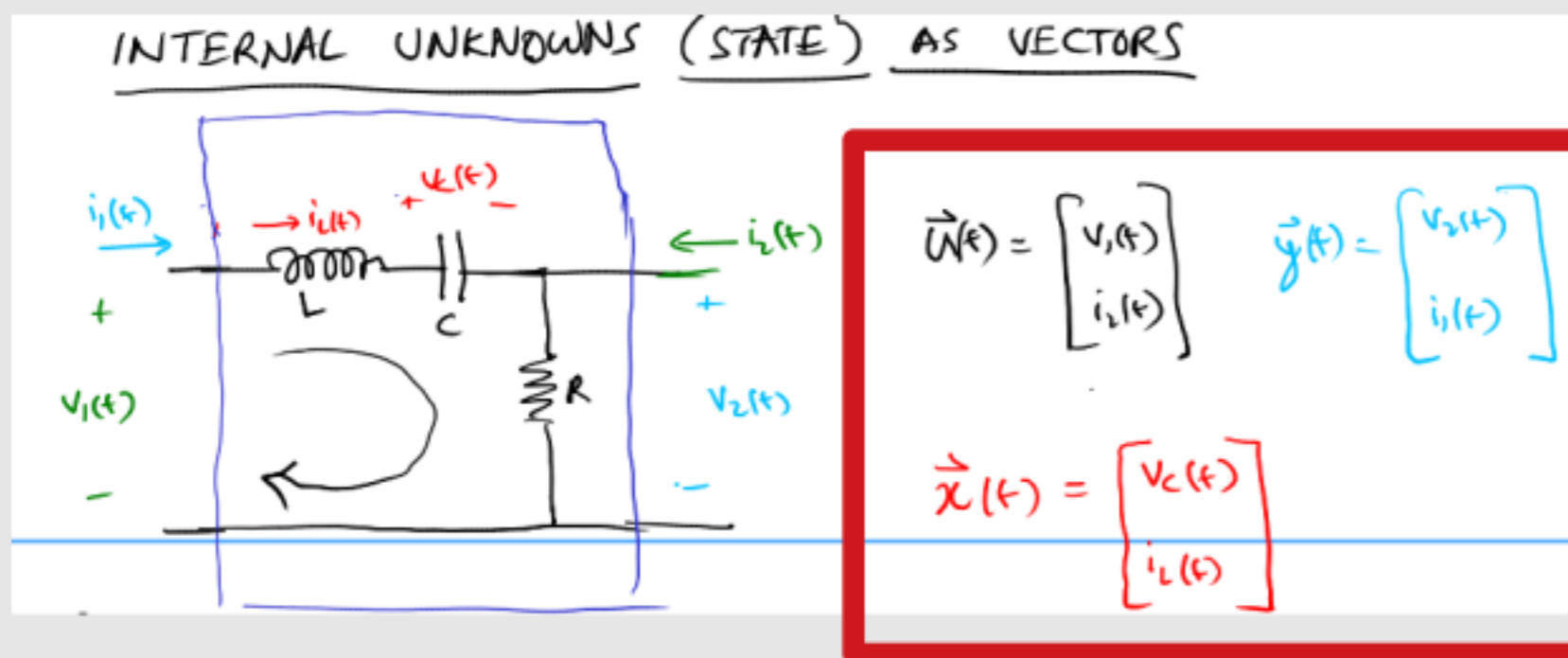


**STATE SPACE FORMULATION**



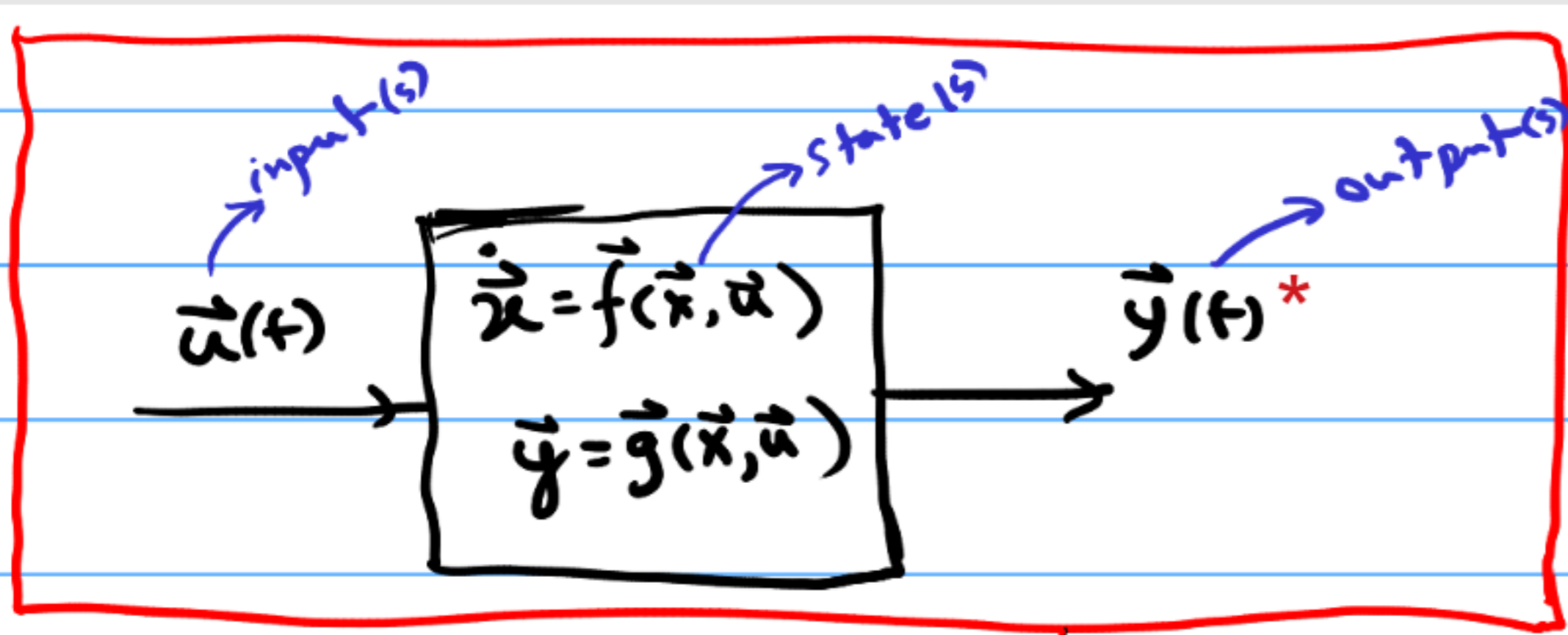
# State+Output Eqns Together

$$\frac{d}{dt} \begin{bmatrix} v_c(t) \\ i_L(t) \end{bmatrix} = \underbrace{\begin{bmatrix} 0 & 1/C \\ -1/L & -R/L \end{bmatrix}}_{\vec{f}(\vec{x}, \vec{u})} \begin{bmatrix} v_c(t) \\ i_L(t) \end{bmatrix} + \underbrace{\begin{bmatrix} 1/L \\ -R/L \end{bmatrix}}_{\vec{g}(\vec{x}, \vec{u})} \begin{bmatrix} v_1(t) \\ i_2(t) \end{bmatrix}$$



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## STATE SPACE FORMULATION

\* if not explicitly given, the entire state will be the output.

# State Space Formulation: Benefits

- why is it useful?

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  - any circuit can be written like this (not just this one)\*
    - however big or complicated

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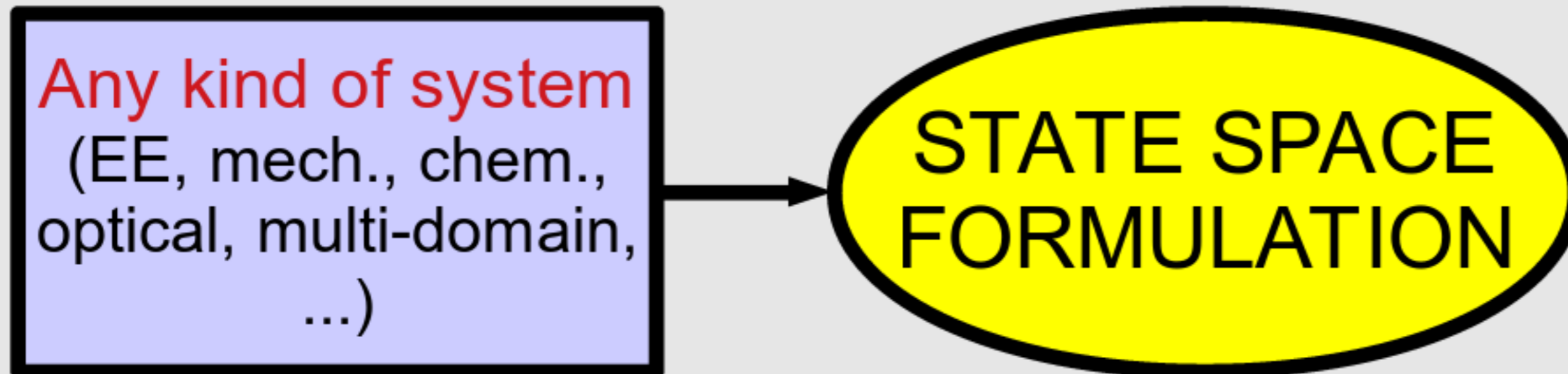
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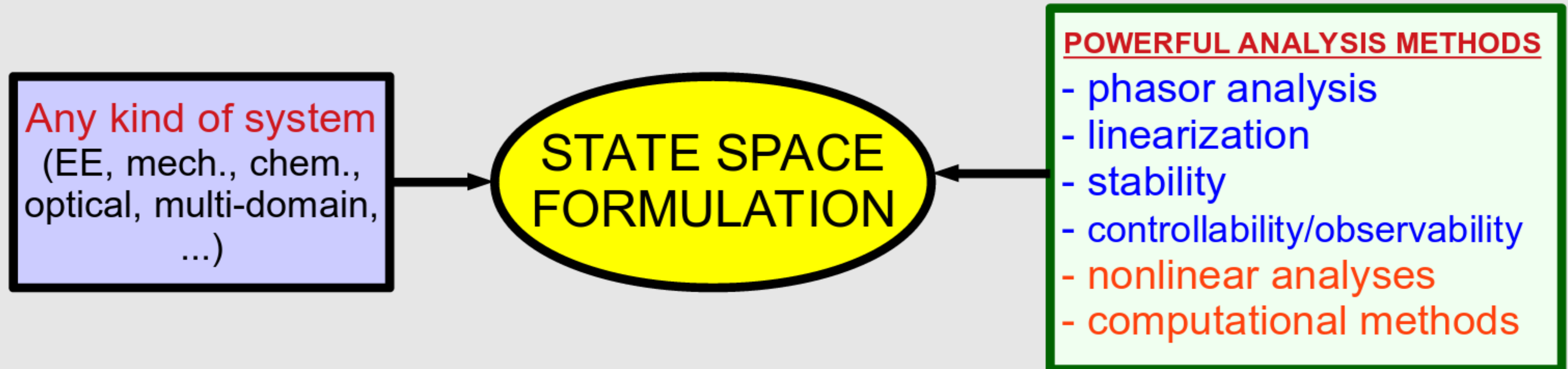


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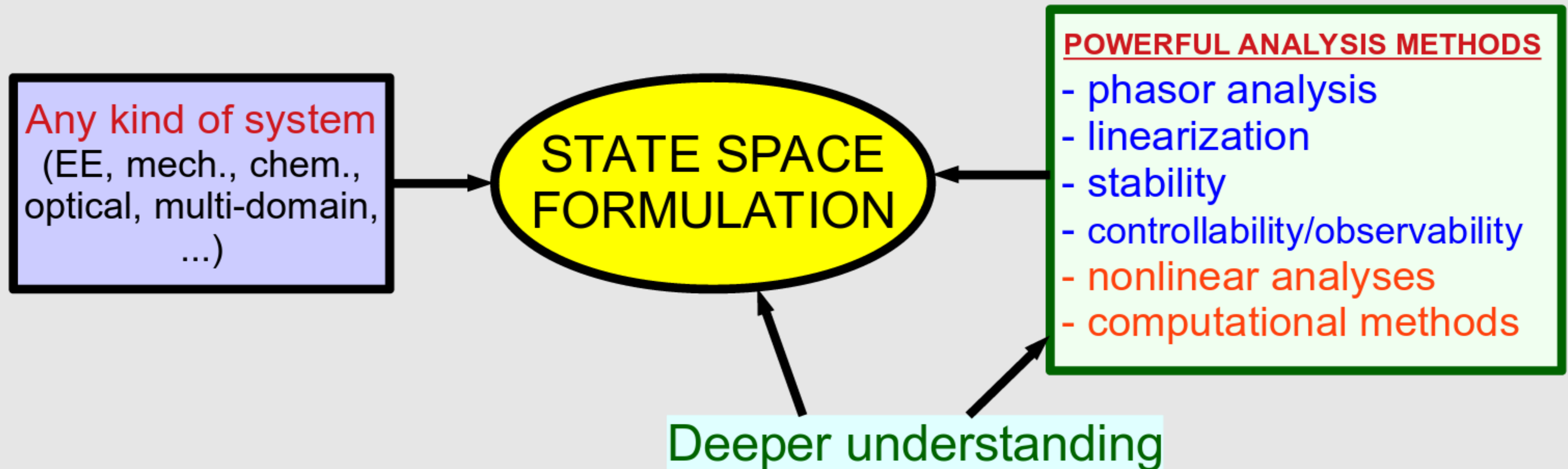


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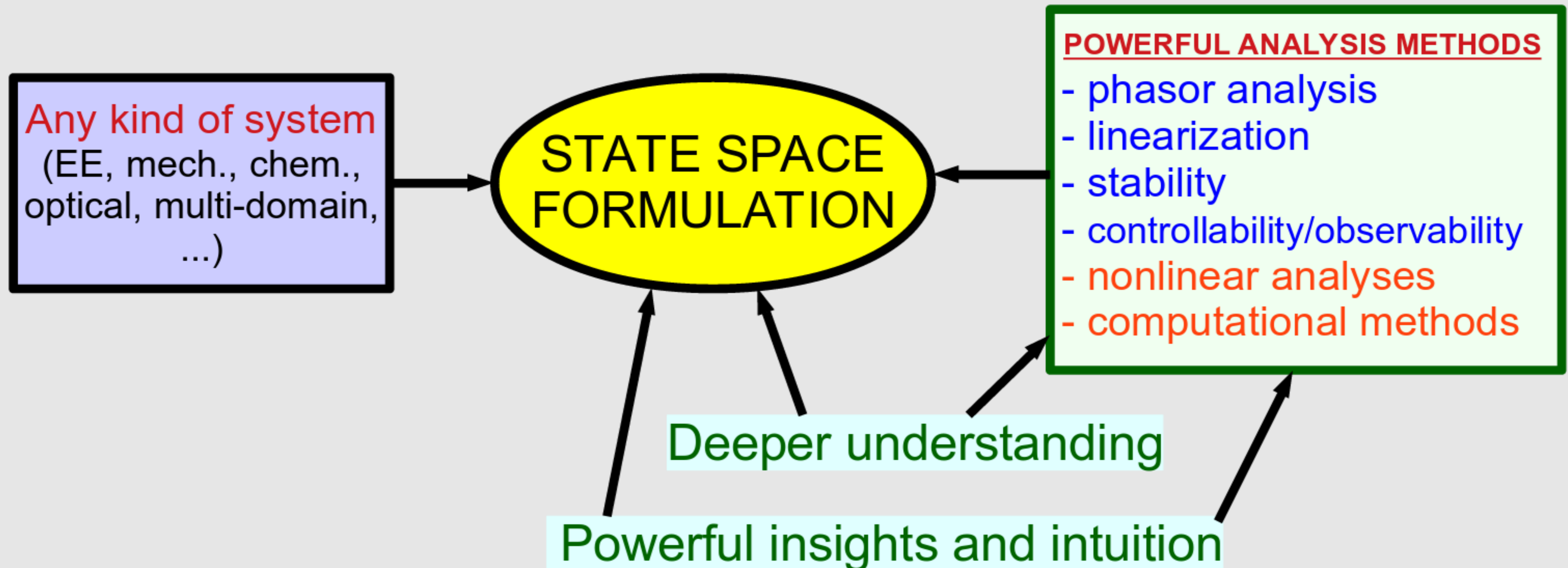


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# Previous Lecture

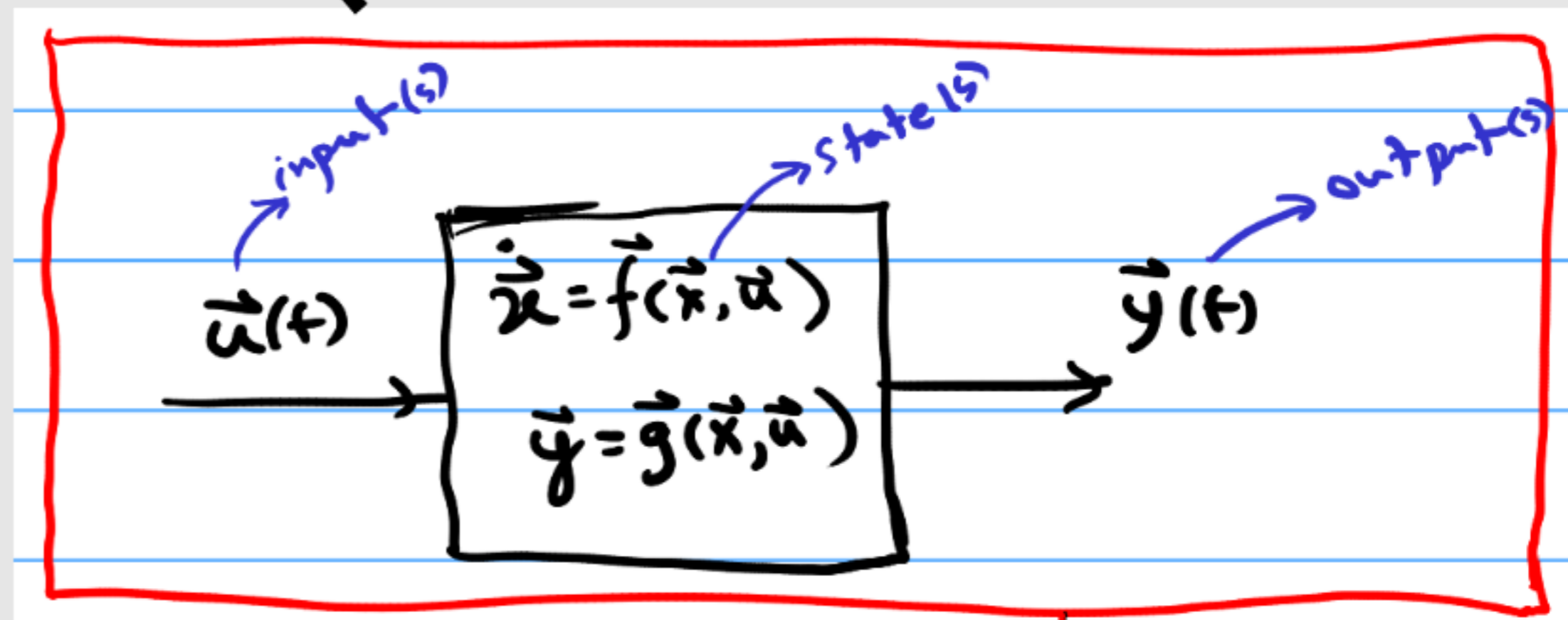
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+ initial condition (IC)

Any kind of system  
(EE, mech., chem.,  
optical, multi-domain,  
...)

STATE SPACE  
FORMULATION



# Previous Lecture

- examples

- RLC circuit
- pendulum

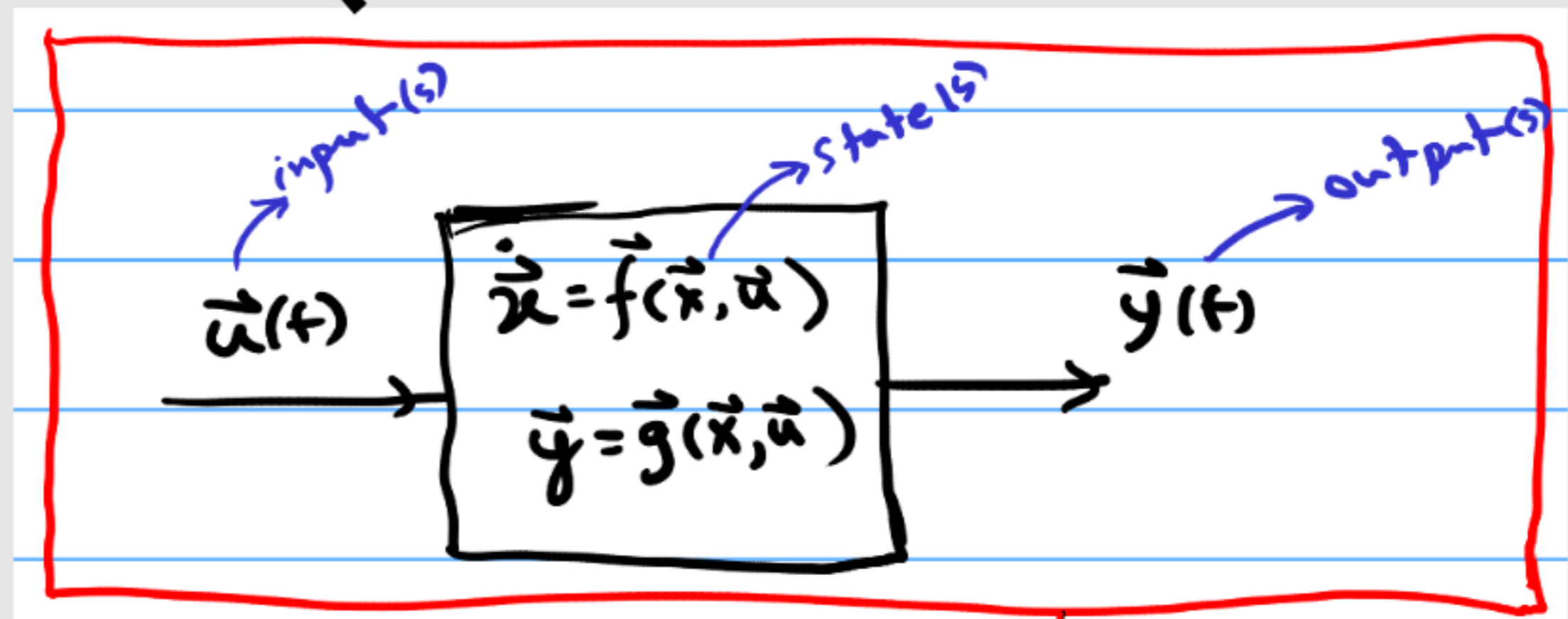
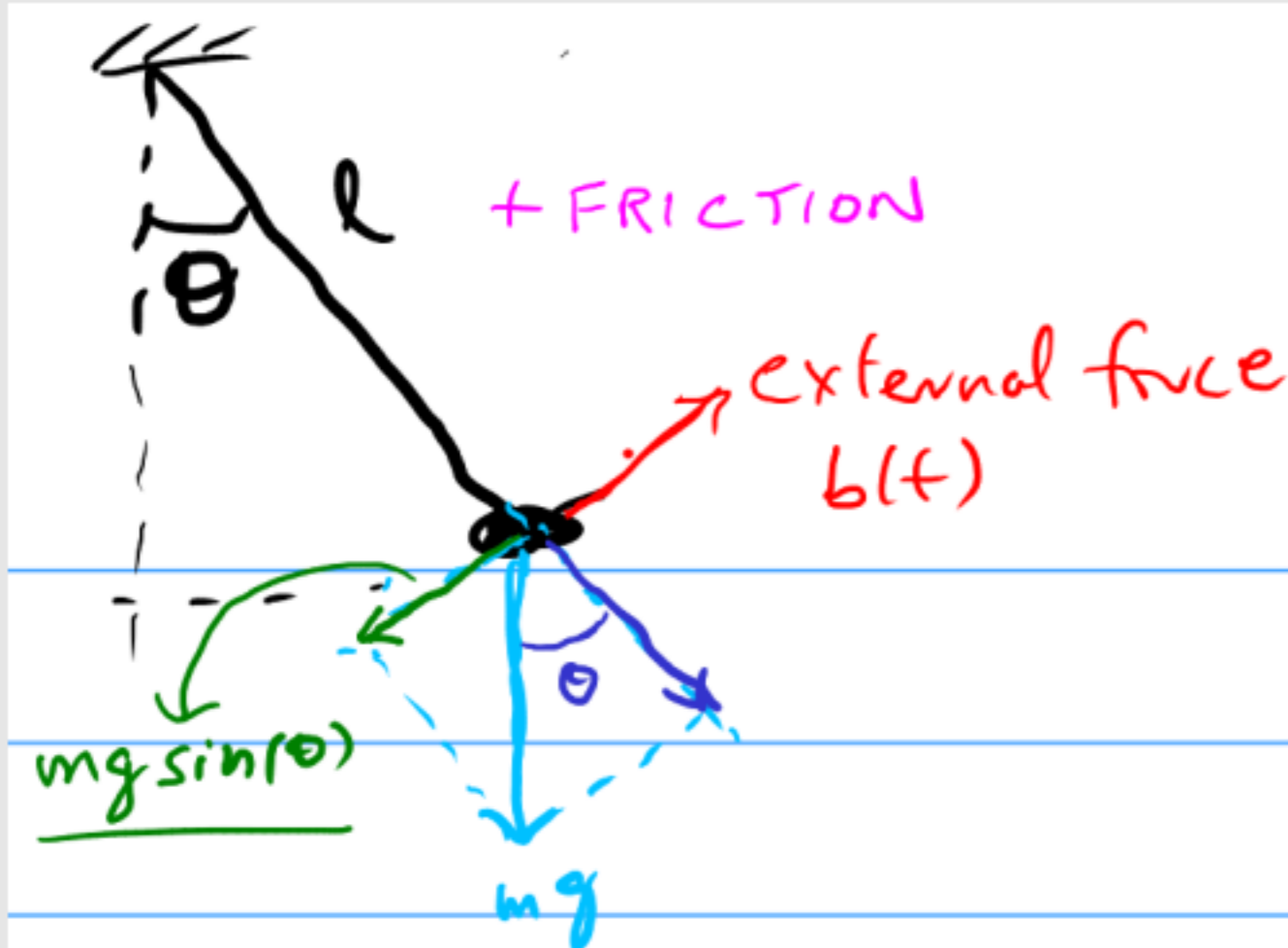
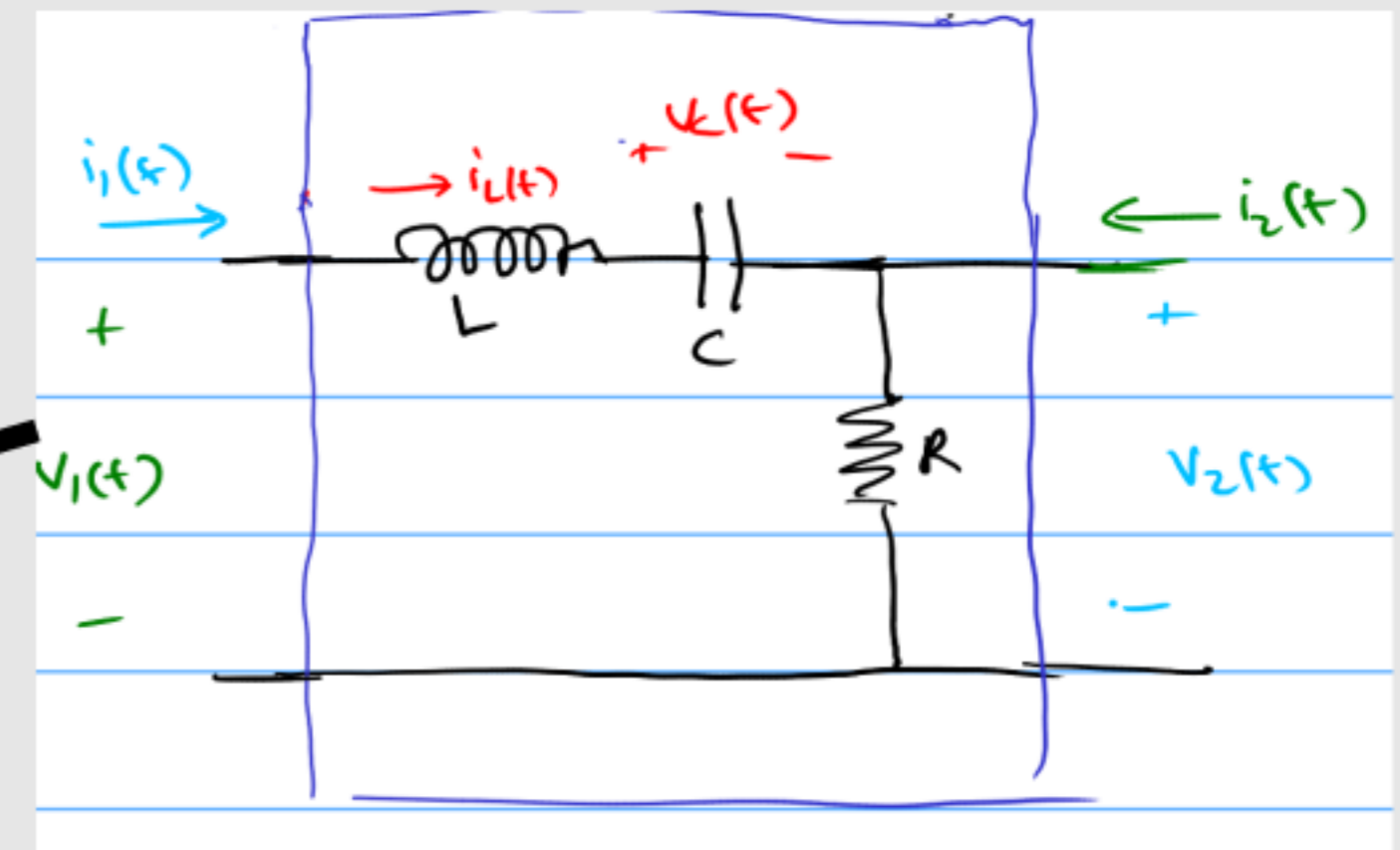
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STATE SPACE FORMULATION



# Mechanical Example: Pendulum

- (move to xournal)

→ Newton's equ. of motion:  $F = ma$  or  $a = \frac{F}{m}$

→ total tangential force =

force due to gravity:  $-mg \sin(\theta)$

+ force " " friction:  $-k \cdot \text{velocity}$

+ externally applied force:  $b(t)$

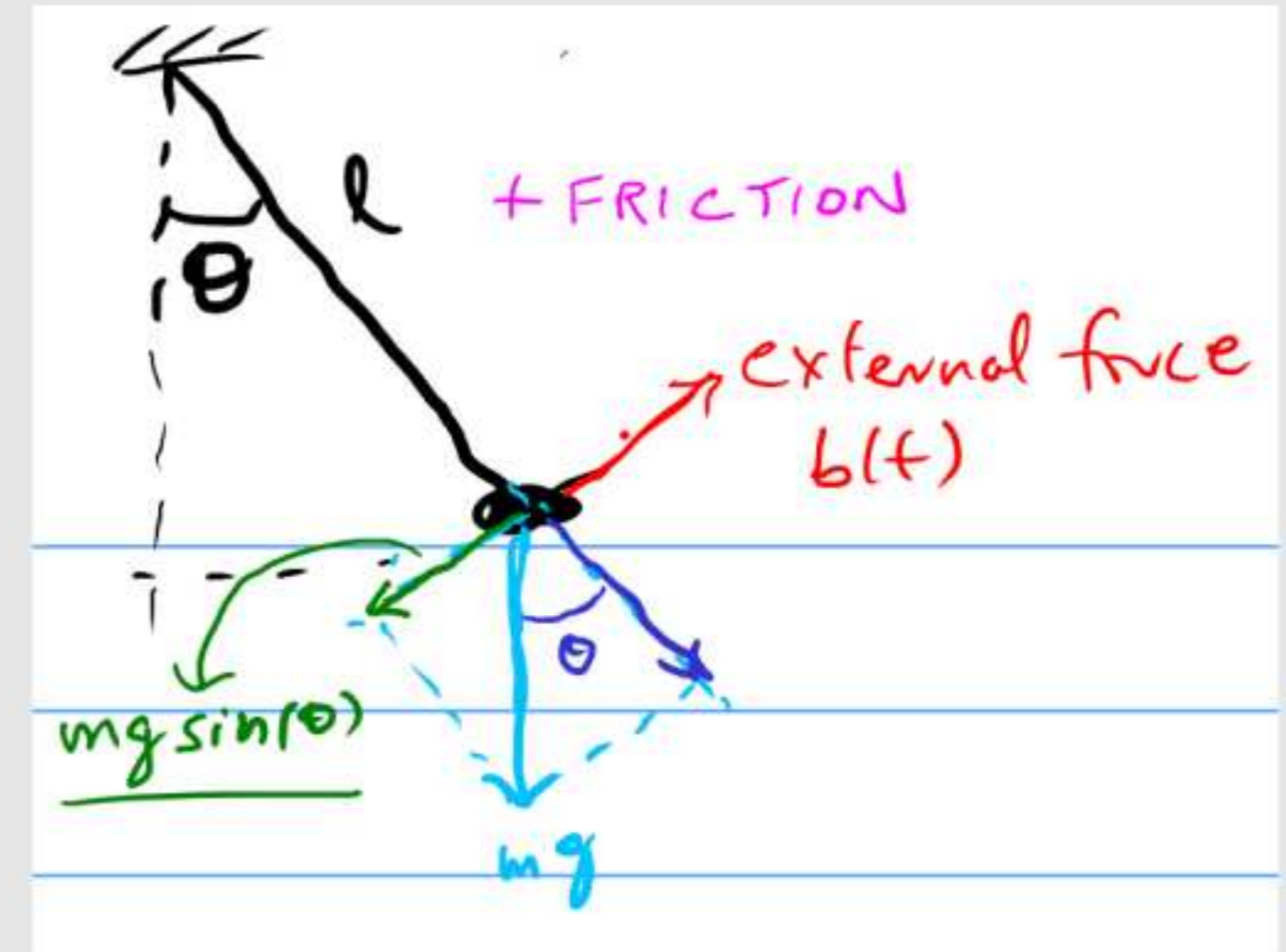
→ arc-length (from bottom)  $\equiv y = l\theta$  ←  $\theta$  in radians

→ velocity =  $\frac{dy}{dt} = l \frac{d\theta}{dt}$   
 $\underbrace{\hspace{1.5cm}}_{v_\theta}$

→ acceleration =  $\frac{d^2y}{dt^2} = l \frac{d^2\theta}{dt^2} = l \frac{dv_\theta}{dt}$

→ total force:  $-mg \sin(\theta) - kl \frac{d\theta}{dt} + b(t)$

→  $a = F/m \Rightarrow l \frac{d^2\theta}{dt^2} = -g \sin(\theta) - \frac{kl}{m} \frac{d\theta}{dt} + \frac{b(t)}{m}$



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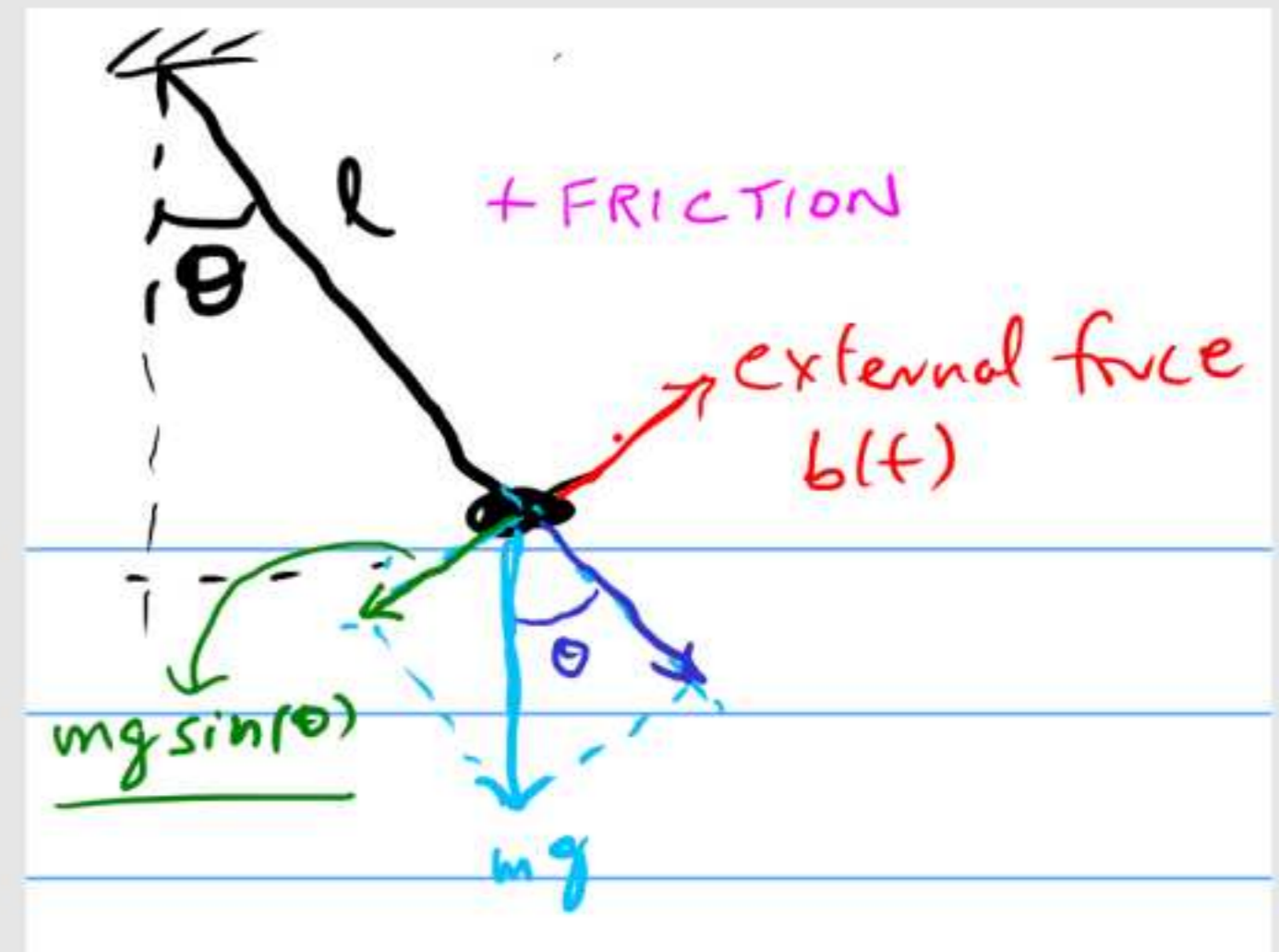
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$$\frac{d^2\theta}{dt^2} = -\frac{g}{l} \sin(\theta) - \frac{k}{m} \frac{d\theta}{dt} + \frac{b(t)}{m l}$$

$$\vec{x} = \begin{bmatrix} \theta \\ v_\theta \end{bmatrix}, \quad \vec{a} = \begin{bmatrix} b(t) \end{bmatrix}$$

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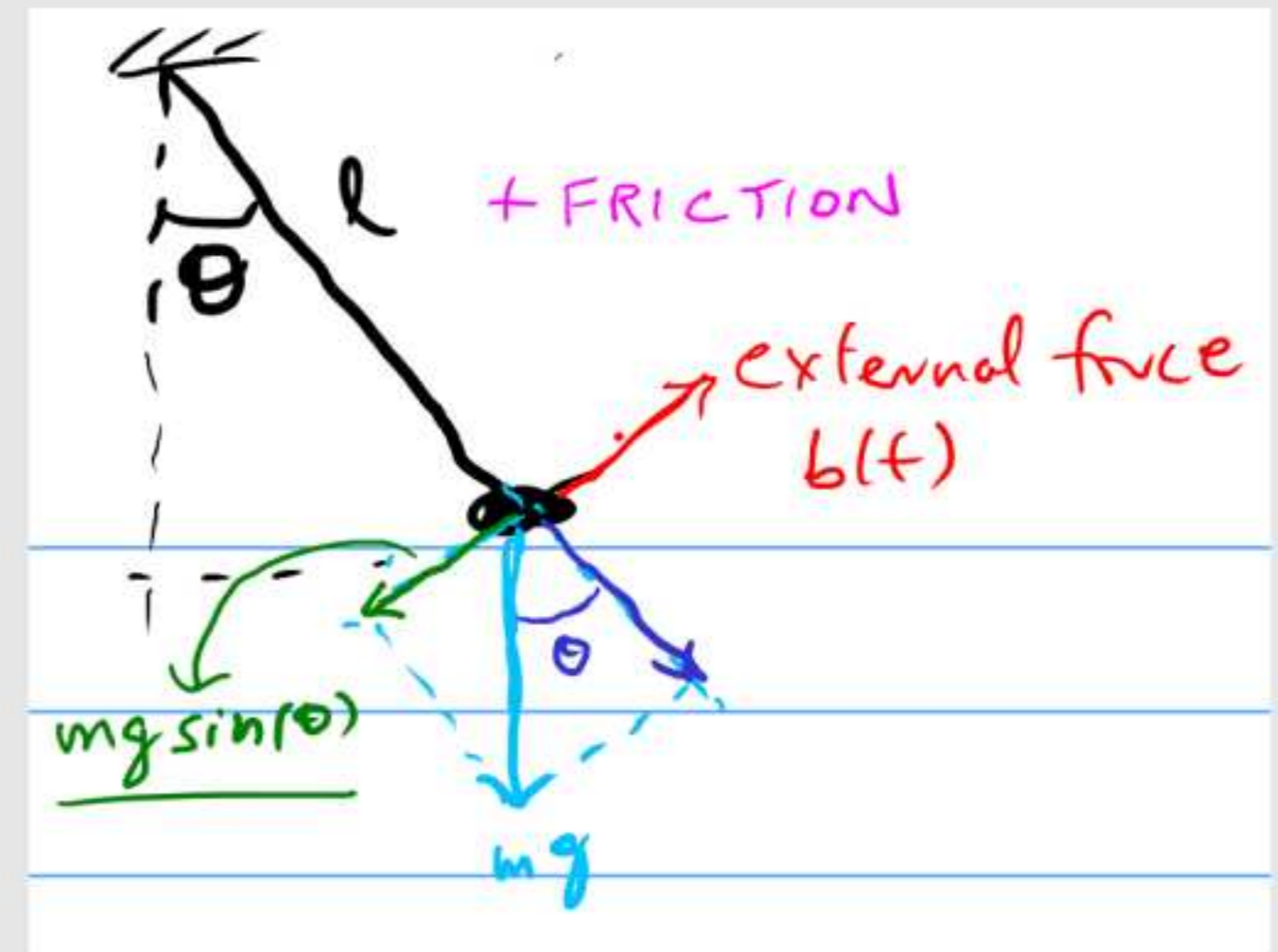
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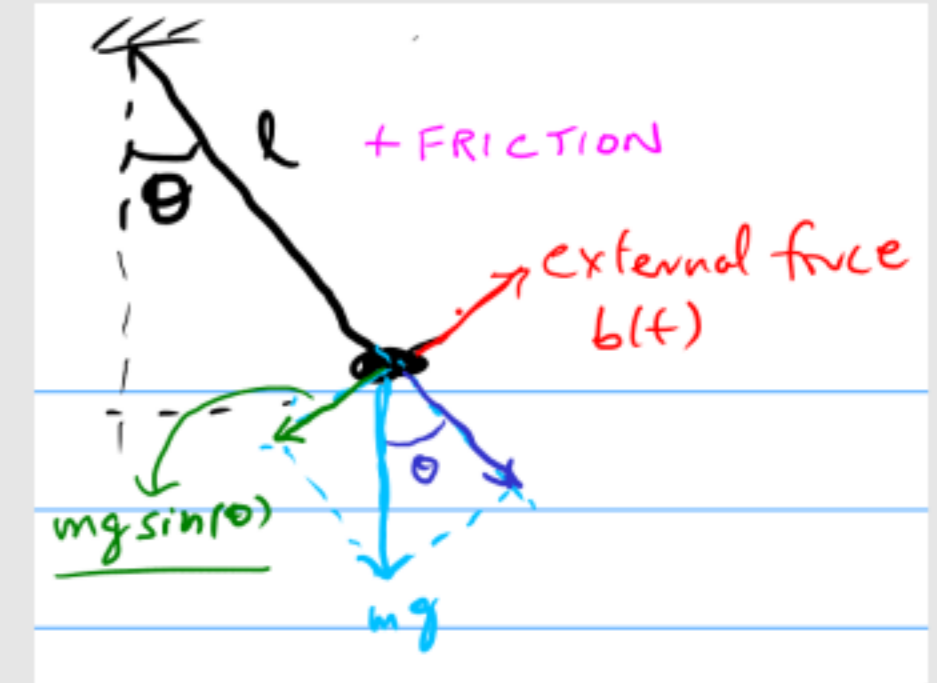
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- The system is nonlinear (because of  $\sin(\dots)$ )

# Pendulum: simplification for small $\theta$

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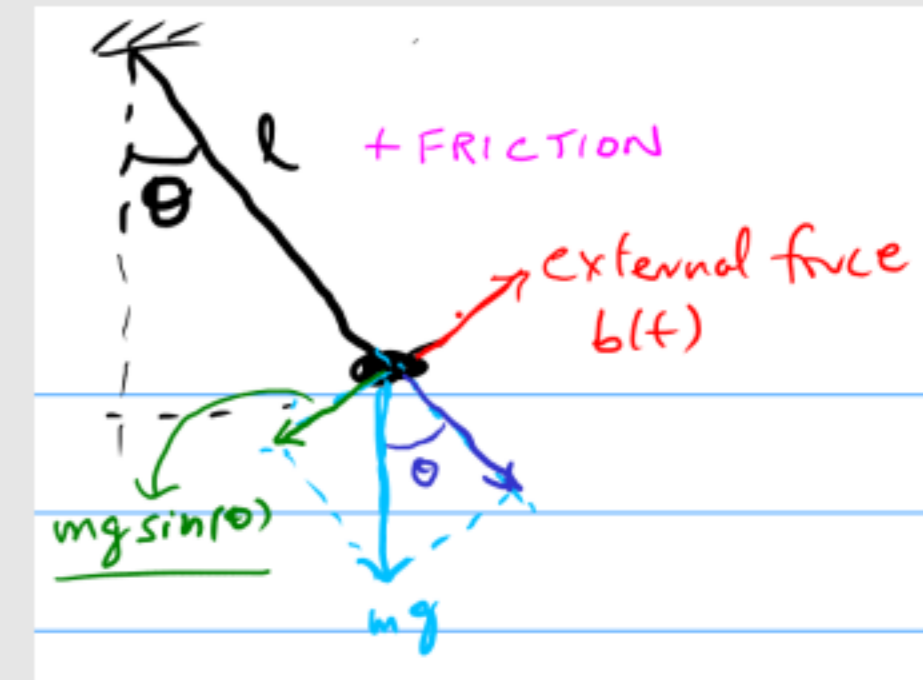
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$$\rightarrow \sin(\theta) \approx \theta \quad (\text{in radians})$$

→ example of linearization



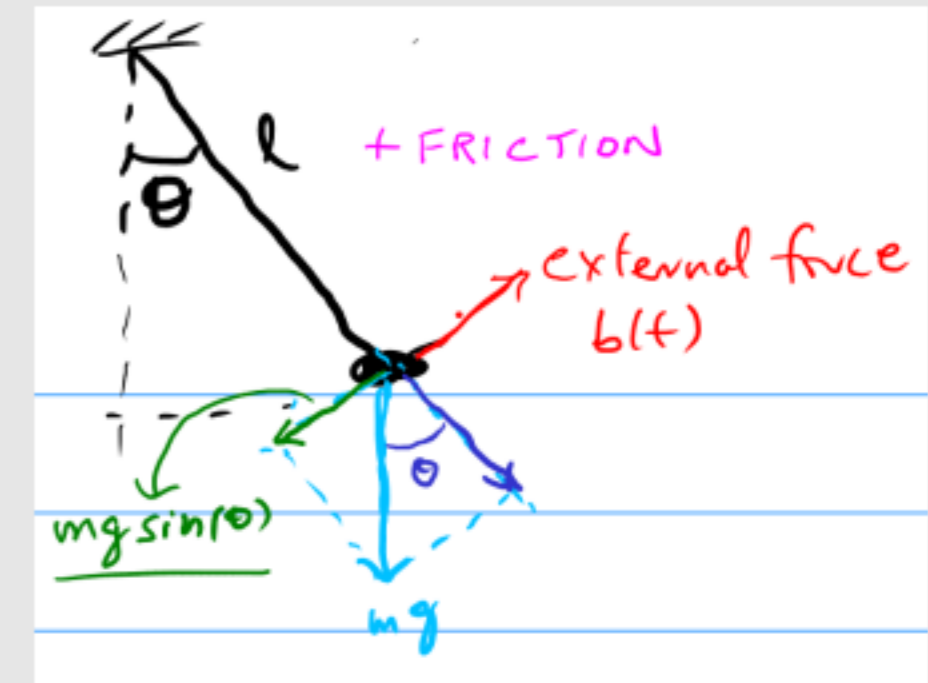
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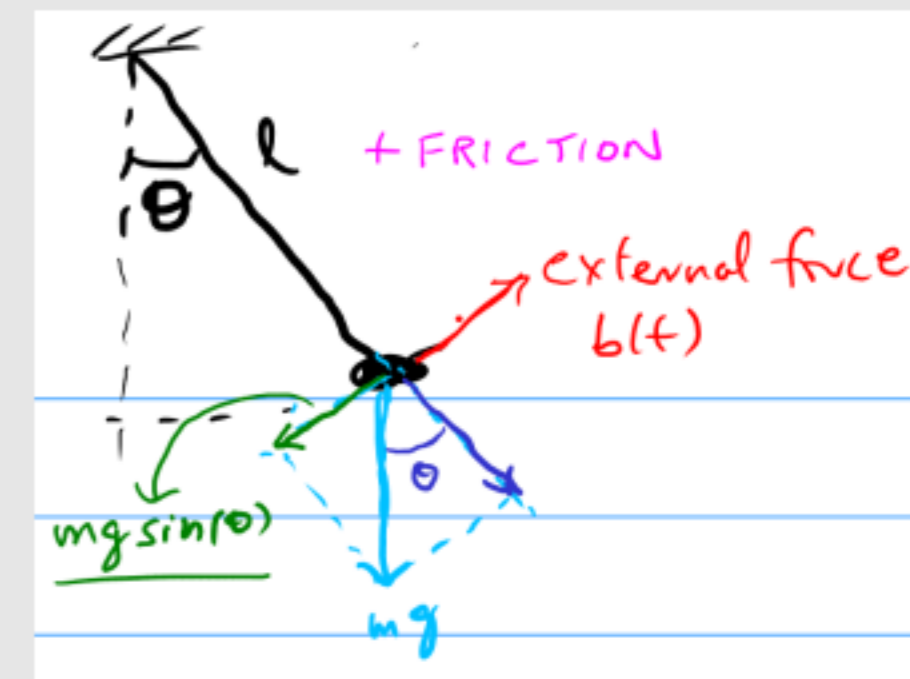
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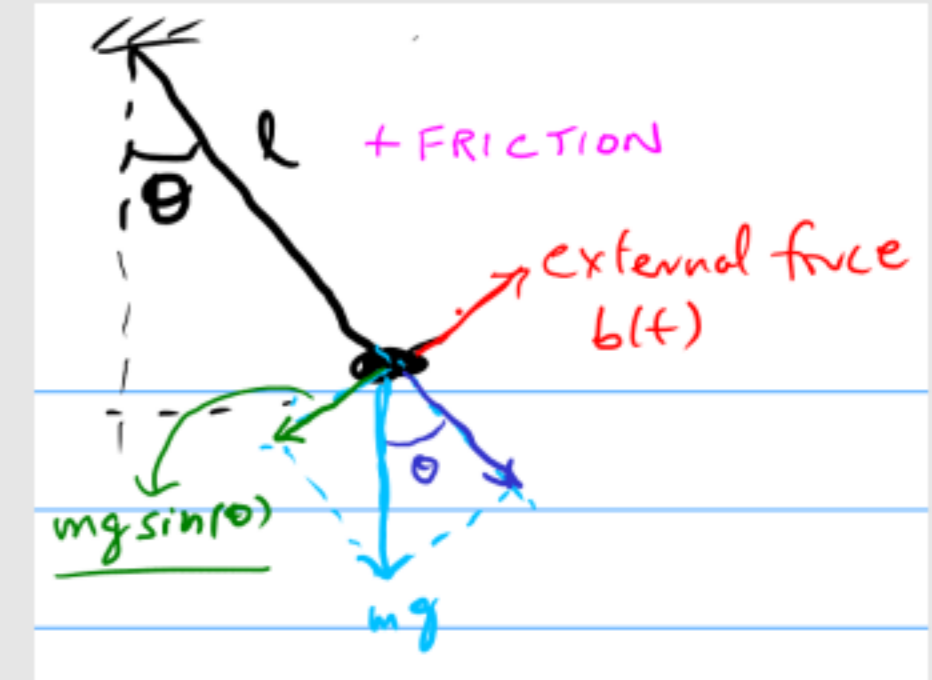
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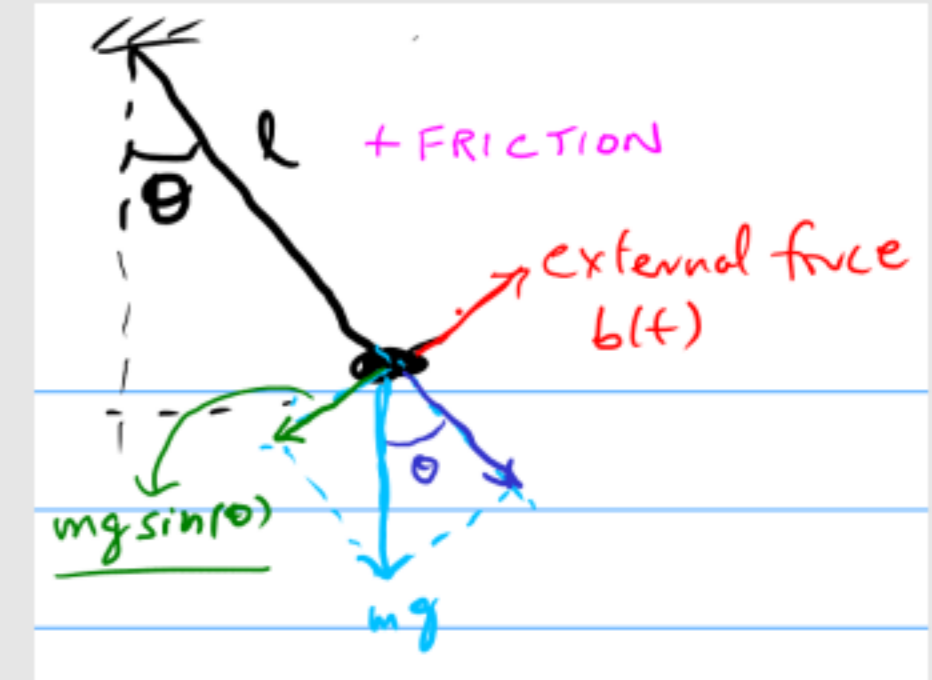
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- INSIGHT:** RLC ckt and damped pendulum are "the same"!

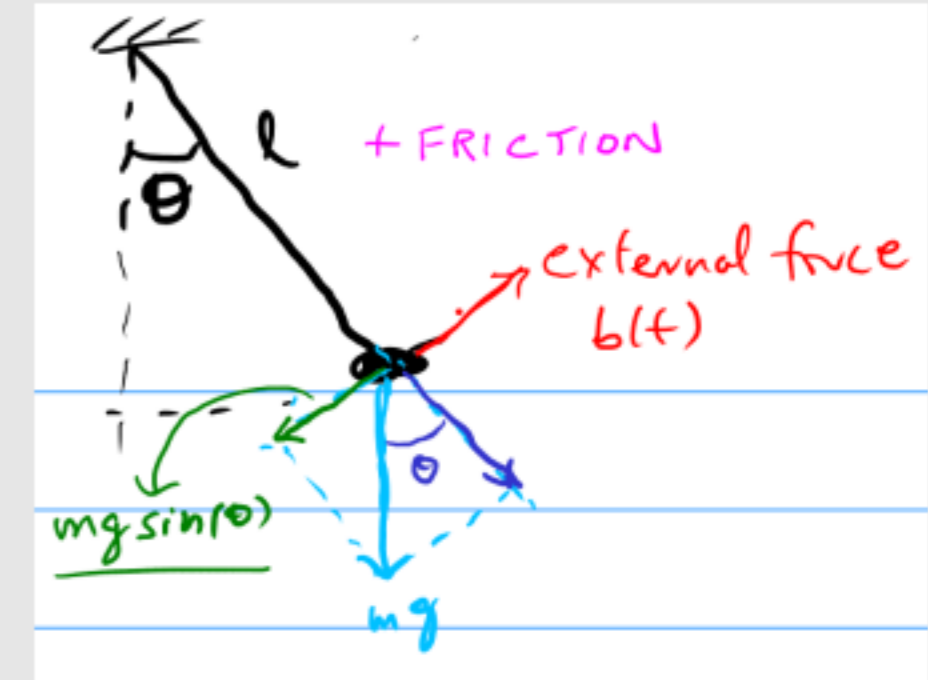
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↑  
Filters

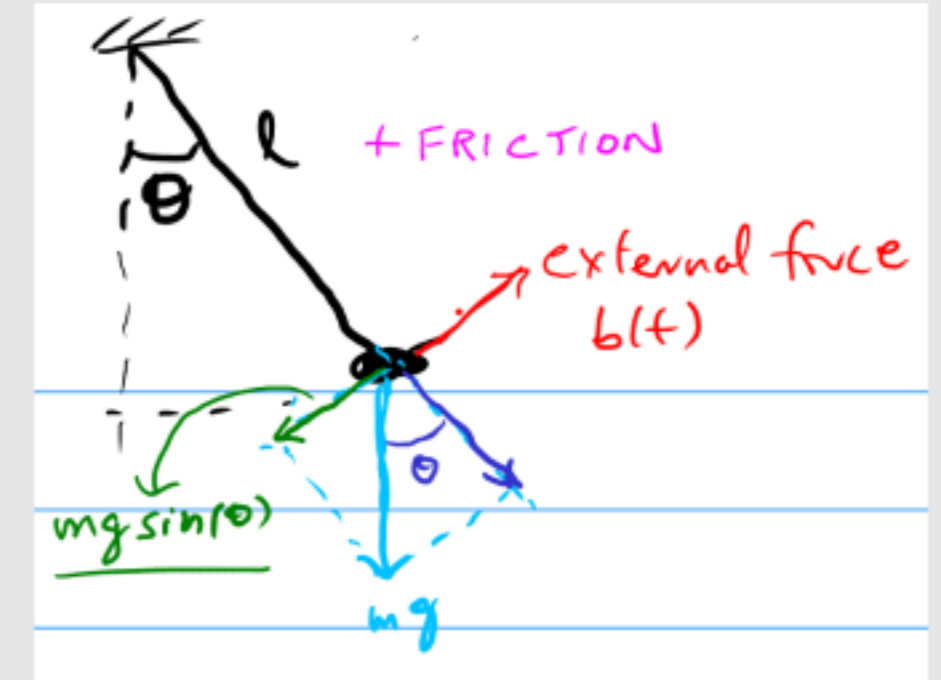
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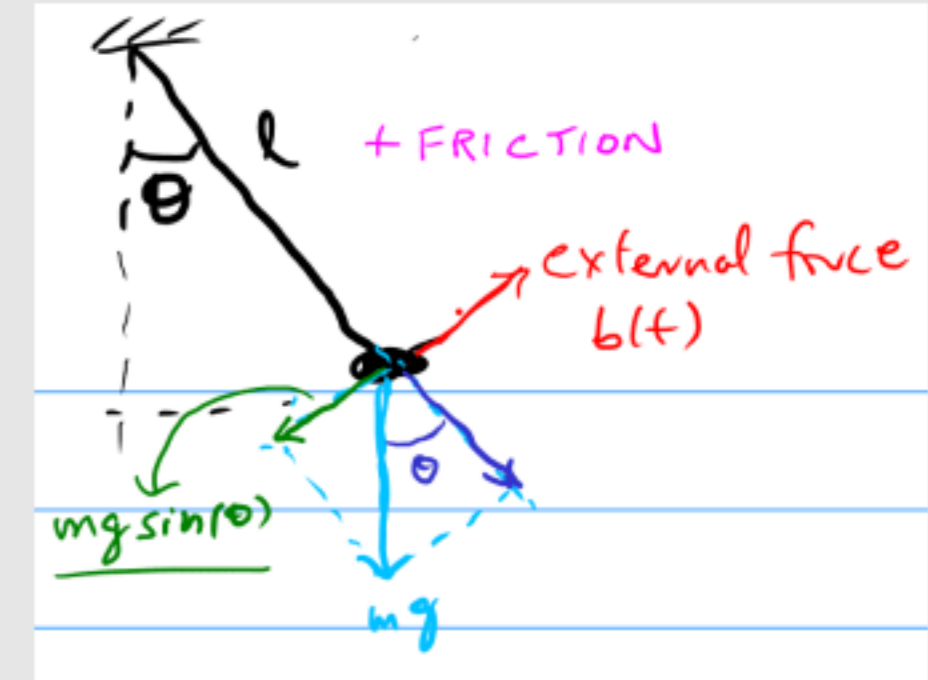
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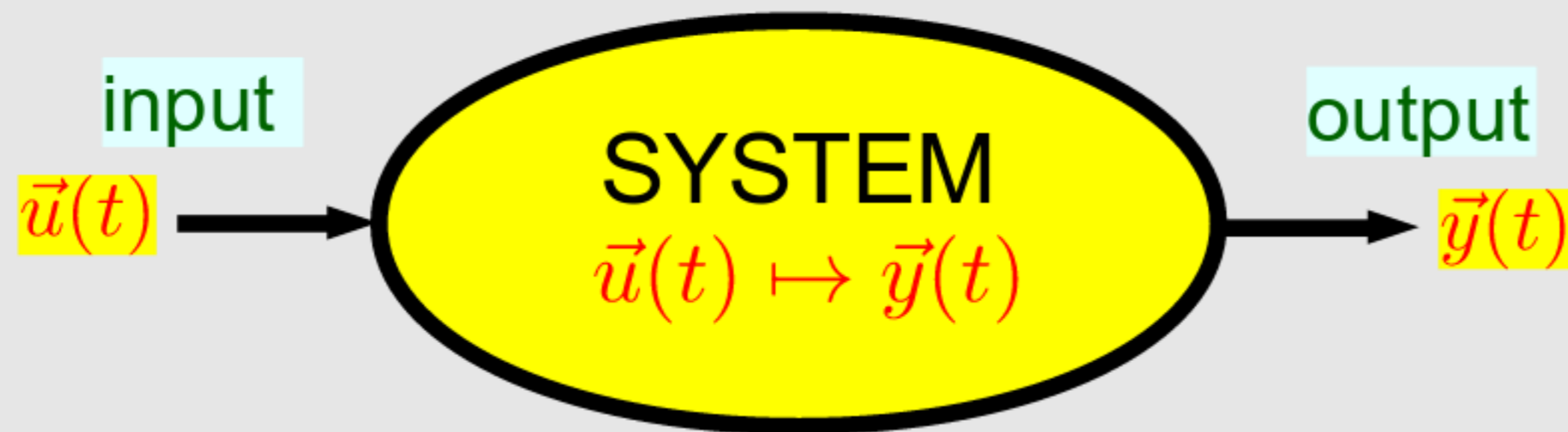
Filters

Filters??

**MEMS filters!**  
(smaller, better, cheaper)

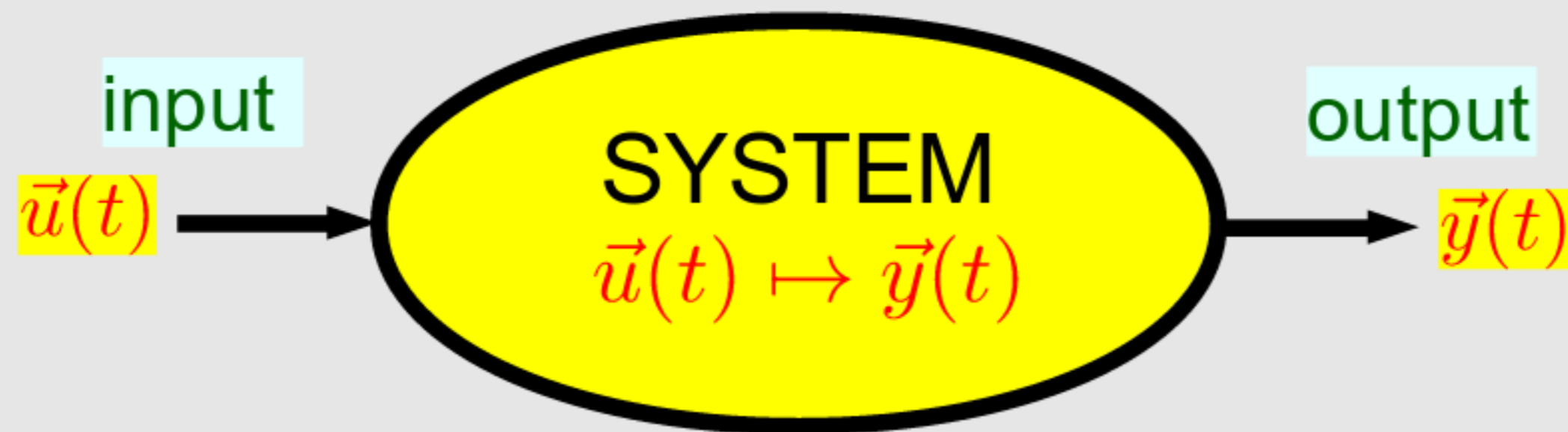
# Recap of Linearity

- The concept of **LINEARITY** is extremely important
- **it is fundamentally a systems concept**



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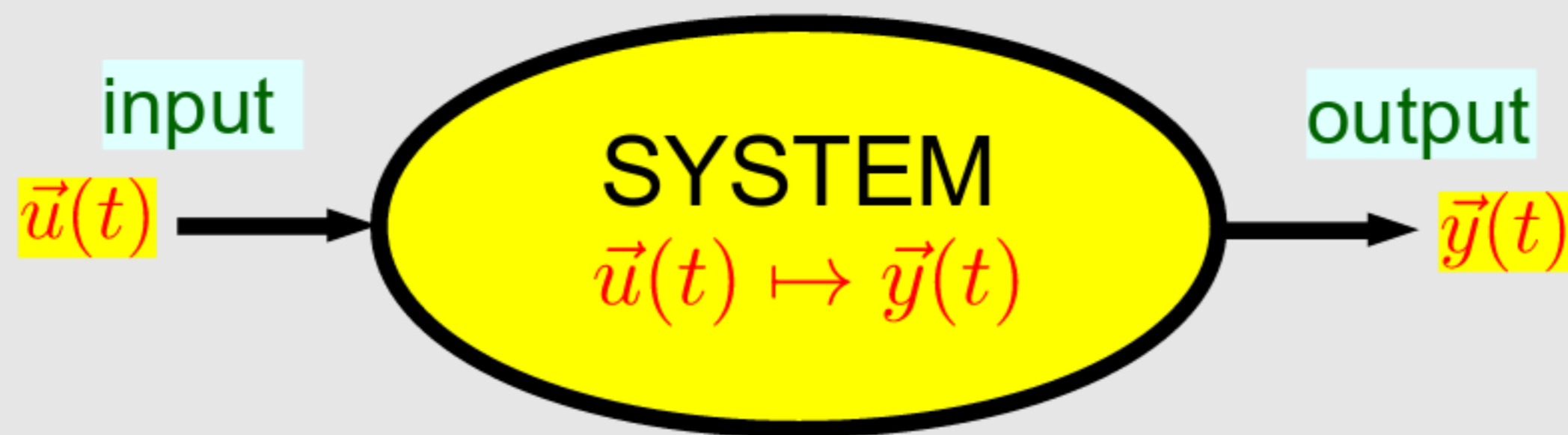


- 3 steps to check linearity
- **clearly identify your inputs and outputs (this affects linearity)**



# Recap of Linearity

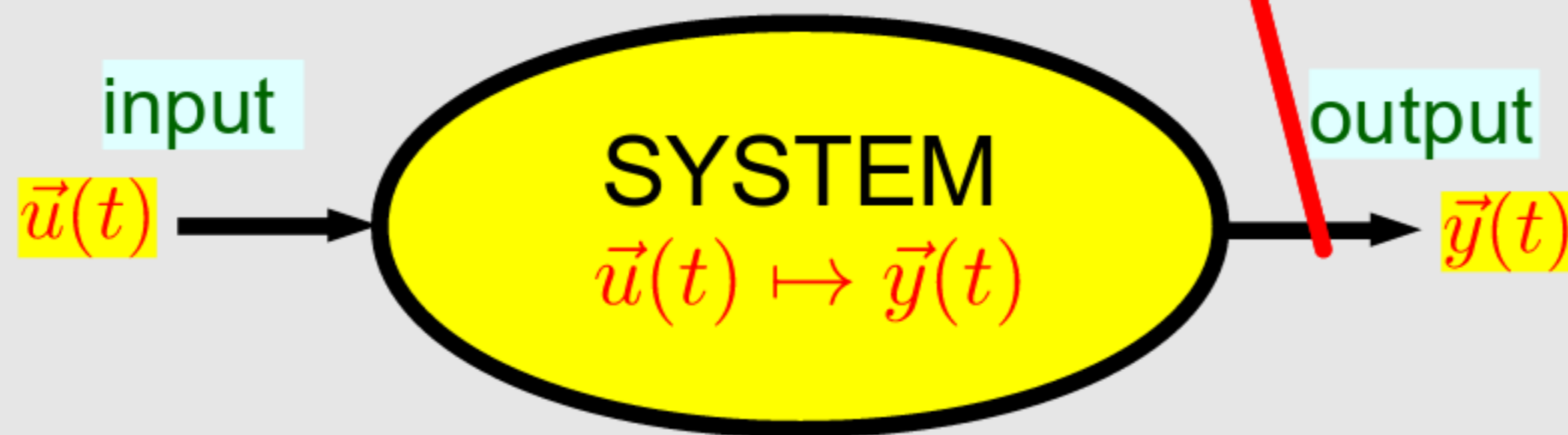
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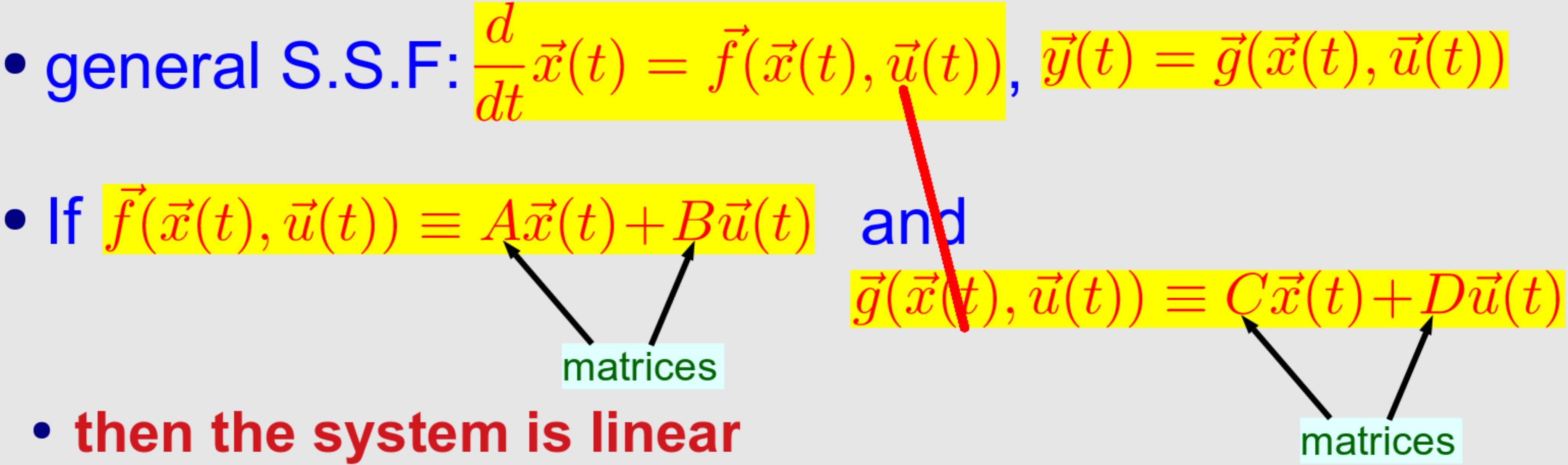
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  - **check scaling**
    - if  $\vec{u}(t) \mapsto \vec{y}(t)$ , then  $(\alpha \vec{u}(t)) \mapsto (\alpha \vec{y}(t))$ ,  $\forall \vec{u}(t)$  and  $\forall \alpha \in \mathbb{R}$

# Linearity of State Space Formulations

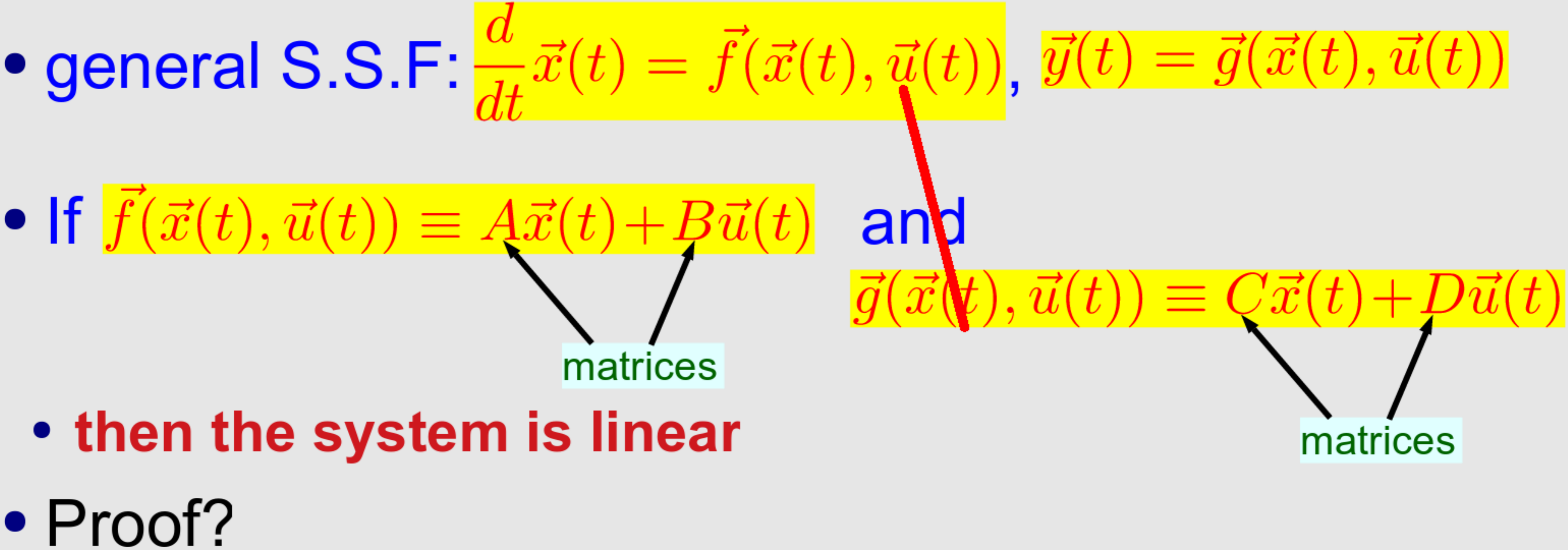
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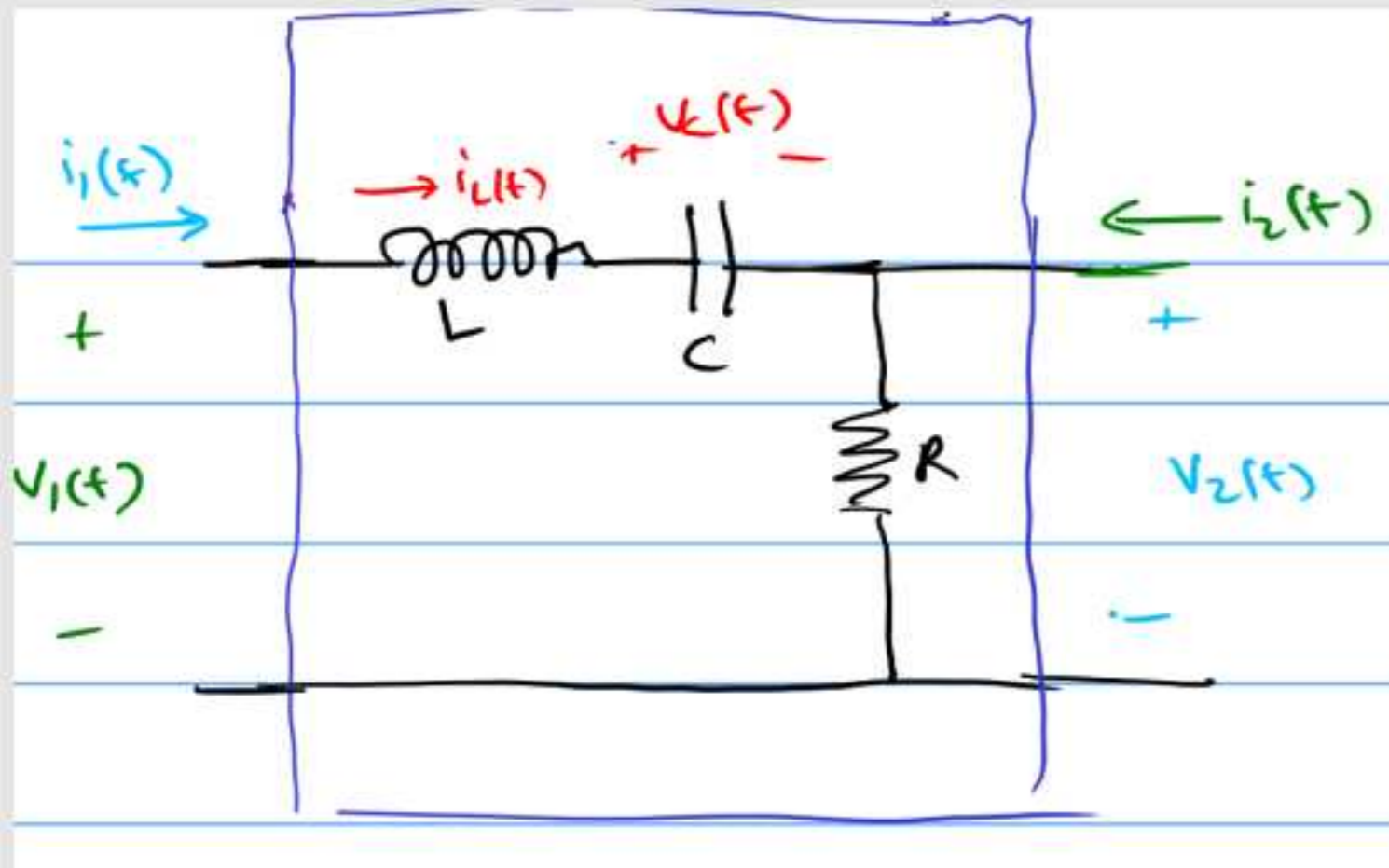
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  - If  $\vec{f}(\vec{x}(t), \vec{u}(t)) \equiv A\vec{x}(t) + B\vec{u}(t)$  and  $\vec{g}(\vec{x}(t), \vec{u}(t)) \equiv C\vec{x}(t) + D\vec{u}(t)$ 
    - then the system is linear
- 

# Linearity of State Space Formulations

- general S.S.F:  $\frac{d}{dt}\vec{x}(t) = \vec{f}(\vec{x}(t), \vec{u}(t)), \vec{y}(t) = \vec{g}(\vec{x}(t), \vec{u}(t))$
  - If  $\vec{f}(\vec{x}(t), \vec{u}(t)) \equiv A\vec{x}(t) + B\vec{u}(t)$  and  $\vec{g}(\vec{x}(t), \vec{u}(t)) \equiv C\vec{x}(t) + D\vec{u}(t)$ 
    - then the system is linear
    - Proof?
- 

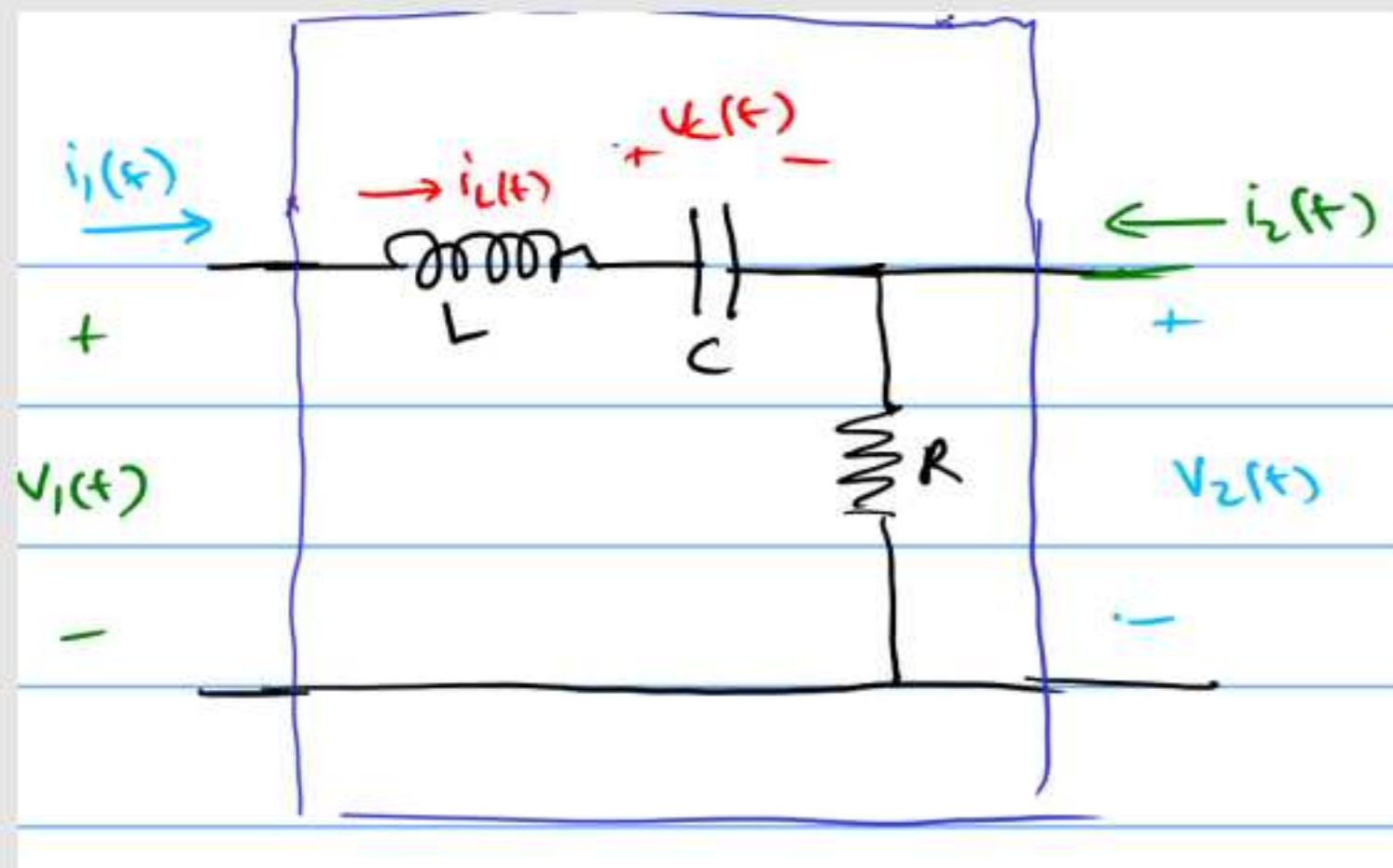
# Are these Systems Linear?



$$\frac{d}{dt} \begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix} = \begin{bmatrix} 0 & 1/C \\ -1/L & -R/L \end{bmatrix} \begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix} + \begin{bmatrix} 1/L & 0 \\ 0 & -R/L \end{bmatrix} \begin{bmatrix} v_1(t) \\ i_2(t) \end{bmatrix}$$

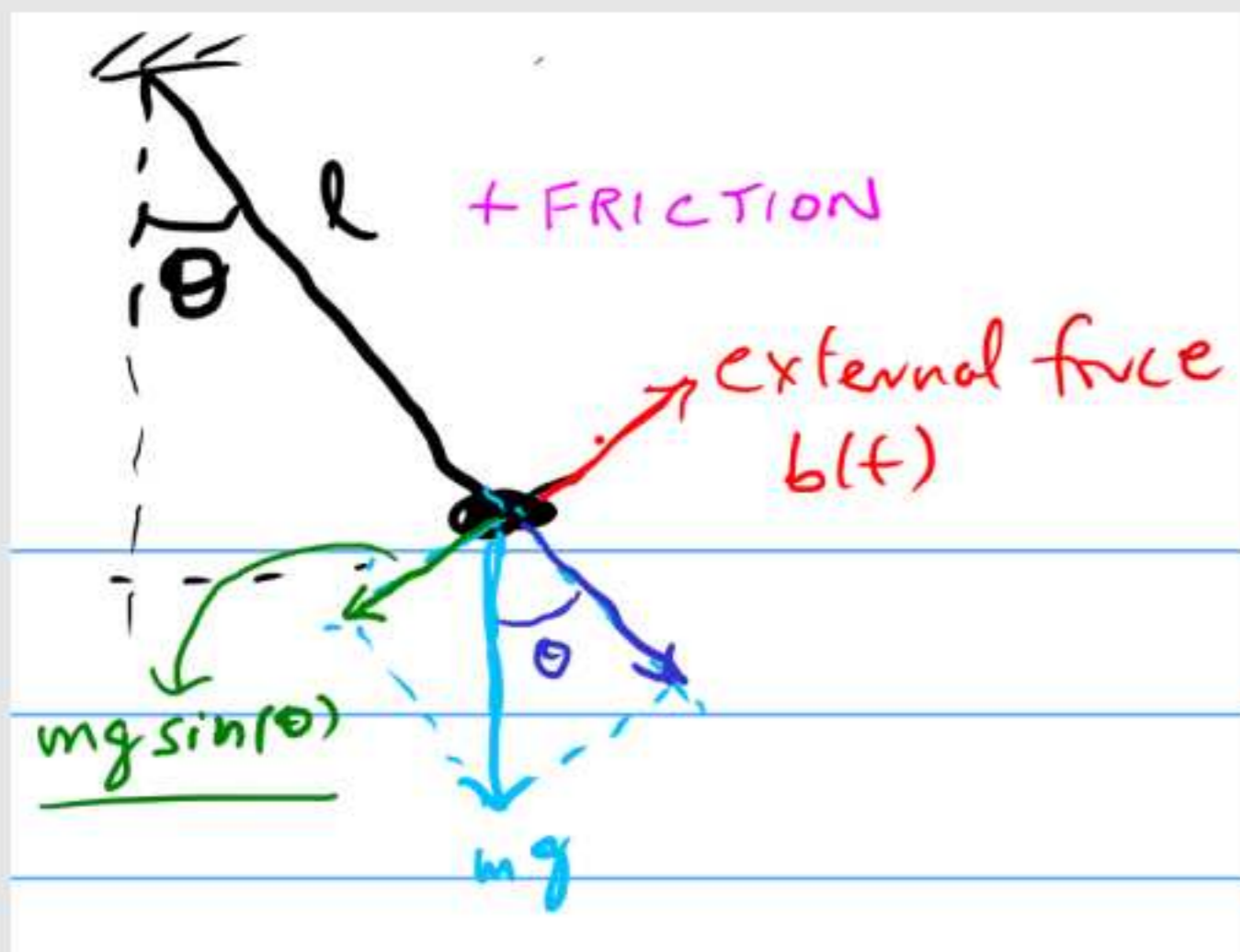
$$\begin{bmatrix} v_2(t) \\ i_1(t) \end{bmatrix} = \underbrace{\begin{bmatrix} 0 & R \\ 0 & 1 \end{bmatrix}}_D \begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix} + \underbrace{\begin{bmatrix} 0 & R \\ 0 & 0 \end{bmatrix}}_E \begin{bmatrix} v_1(t) \\ i_2(t) \end{bmatrix}$$

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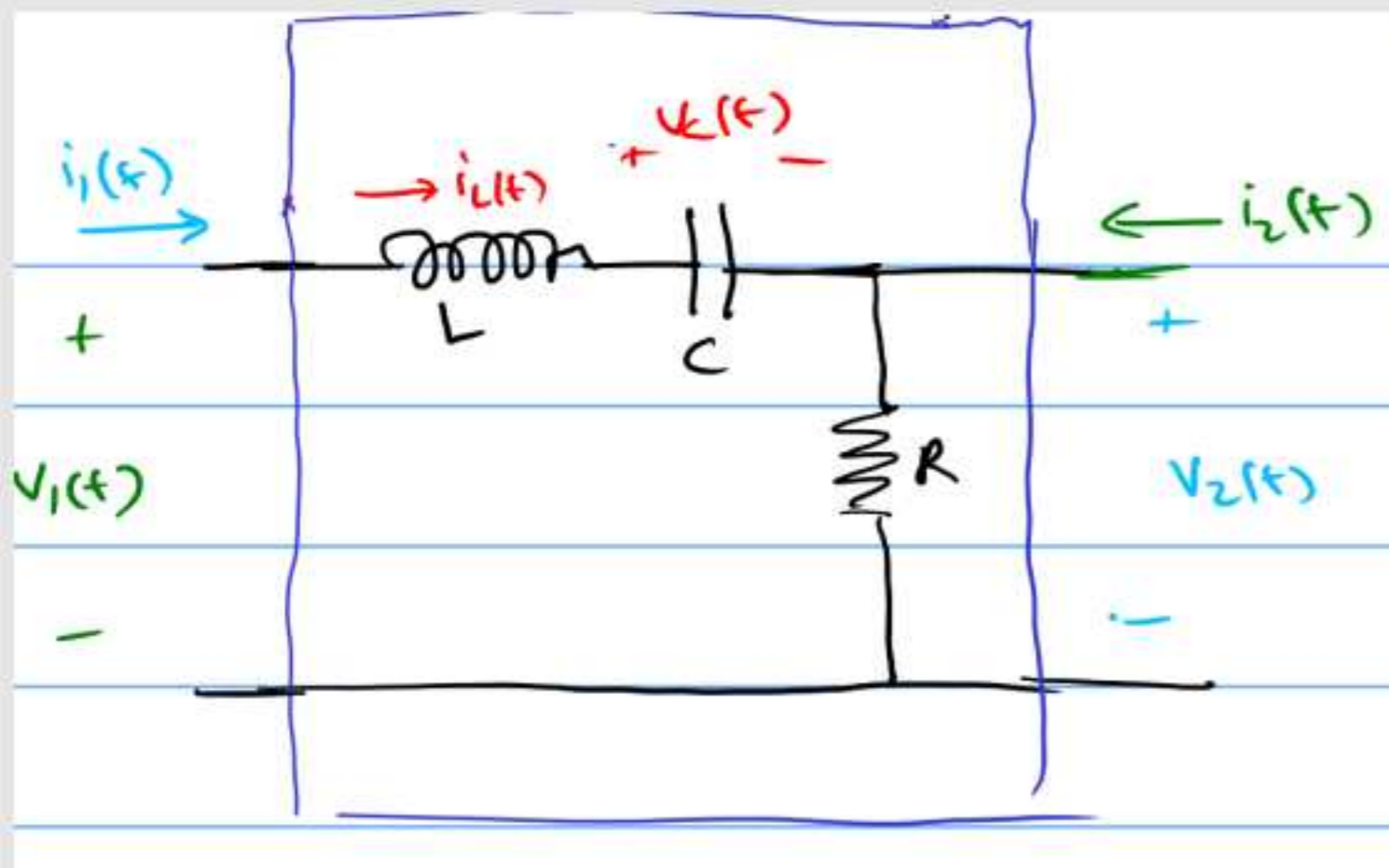
$$\begin{bmatrix} \vec{y}(t) \\ v_2(t) \\ i_1(t) \end{bmatrix} = \underbrace{\begin{bmatrix} 0 & 1 & R \\ 0 & 1 & 1 \end{bmatrix}}_D \begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix} + \underbrace{\begin{bmatrix} 0 & 1 & R \\ 0 & 1 & 0 \end{bmatrix}}_E \begin{bmatrix} v_1(t) \\ i_2(t) \end{bmatrix}$$



$$\vec{x} = \begin{bmatrix} \theta \\ v_\theta \end{bmatrix}, \quad \vec{a} = [b(t)]$$

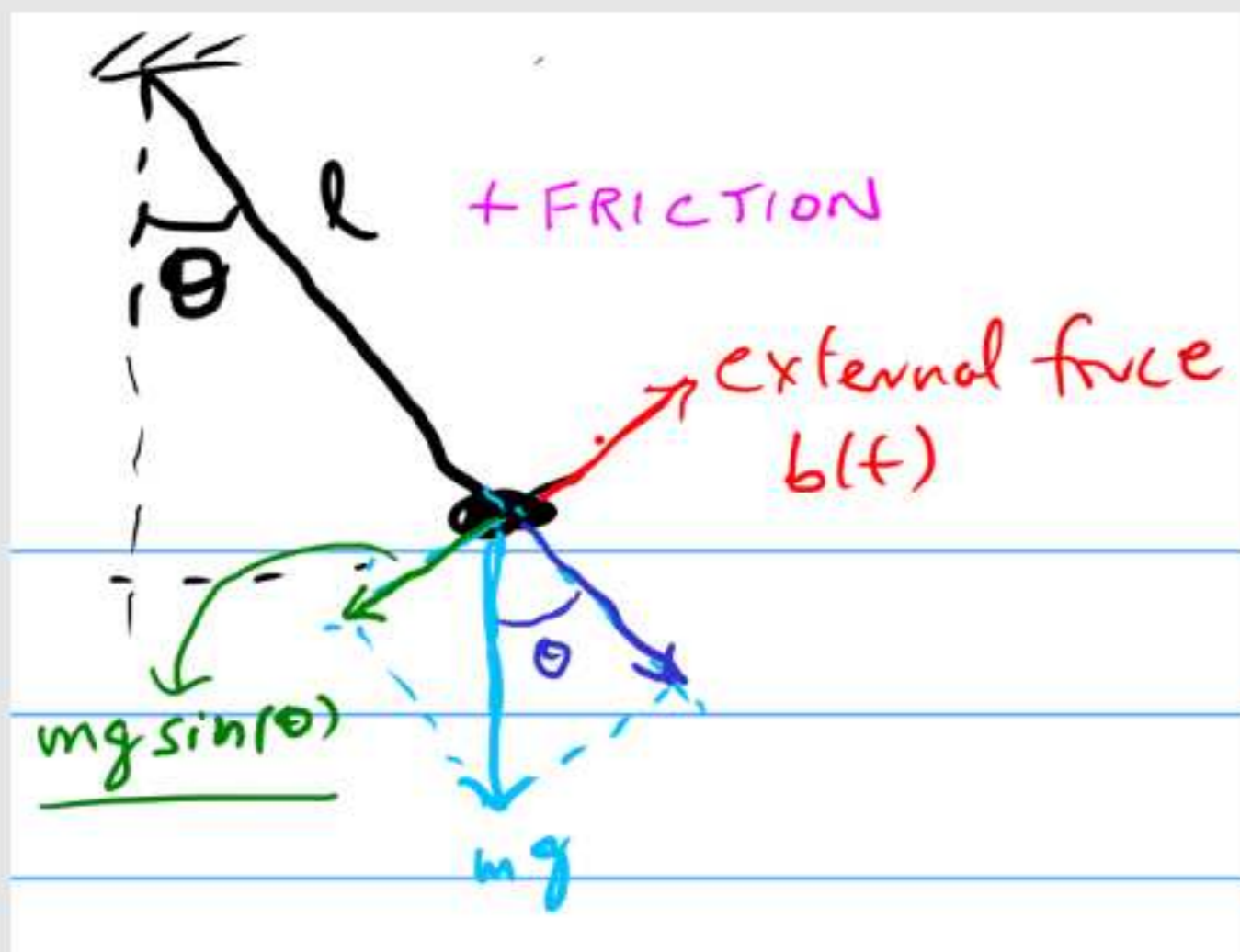
$$\frac{d\vec{x}}{dt} = \begin{bmatrix} v_\theta \\ -g/l \sin(\theta) - k/m v_\theta + \frac{b(t)}{ml} \end{bmatrix}$$

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# State Space F. for Discrete Time Systems

- What is a discrete-time system?
- example: compound interest
  - (move to xournal)

— Example: compound interest

— Principal  $P$

— Annual rate of interest  $r$ , compounded monthly. DISCRETE  
(integer, not  
real number)

— Savings  $S[t] = S[t-1] + \frac{r}{12} S[t-1]$   
with  $S[0] = P$  ← INITIAL CONDITION

— Additions/withdrawals each month:  $u[t]$

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- general form:  $\vec{x}[t+1] = \vec{f}(\vec{x}[t], \vec{u}[t])$ ,  $\vec{y}[t] = \vec{g}(\vec{x}[t], \vec{u}[t])$   
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**STATE SPACE FORMULATION**

- Discrete time sometimes more natural (eg, for finance, social dynamics, ...)

# Another D.T. Example: Profs. and PhDs.

- (move to xournal)

- $p[t]$ : no. of profs. in the US, year  $t$  ( $t=1,2,3,\dots$ )
- $r[t]$ : no. of PhDs in year  $t$
- $\gamma$ : fraction of PhDs who become professors
- $\delta$ : fraction in each profession retiring
- $u[t]$ : average number of PhD students graduated per prof. per year  
↑ can be manipulated by the professor (controlled by, eg, funding)
- Q: how do  $p(t)$  and  $r(t)$  evolve with time?

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$$- r[t+1] = r[t] - \delta r[t] - \gamma r[t] + p[t] u[t]$$

- State space repr.?

$$\vec{x}(t) \triangleq \begin{bmatrix} p[t] \\ r[t] \end{bmatrix}; \quad \vec{f}(\vec{x}) = \begin{bmatrix} p(1-\delta) + \gamma r \\ r(1-\delta-\gamma) + pu \end{bmatrix}$$

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**VECTOR D.T. STATE-SPACE FORMULATION**

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• Linear?

**VECTOR D.T. STATE-SPACE FORMULATION**