

Lecture 10

+ Design example - bandpass filter

V_{in} components :

	freq	amplitude	
signal	600 Hz	1 mV	{ desired
(alternate current)	AC	60 Hz	10 mV } interference
fluorescent light	60 kHz	20 mV	X

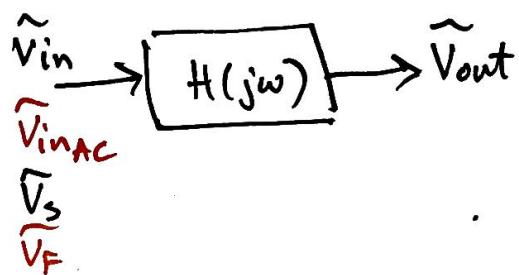
Design goal: Want to attenuate the interference (AC and fluorescent) components by 100 ×, but keep the signal.

$$V_{in}(+) = V_{AC} \cos(\omega_{AC}t + \phi_{AC}) + V_s \cos(\omega_s t + \phi_s) + V_F \cos(\omega_F t + \phi_F)$$

$$\omega_{AC} = 2\pi \cdot 60 \text{ Hz} = 377 \frac{\text{rad}}{\text{s}}$$

$$\omega_s = 2\pi \cdot 600 \text{ Hz}$$

$$\omega_F = 2\pi 60 \text{ kHz}$$

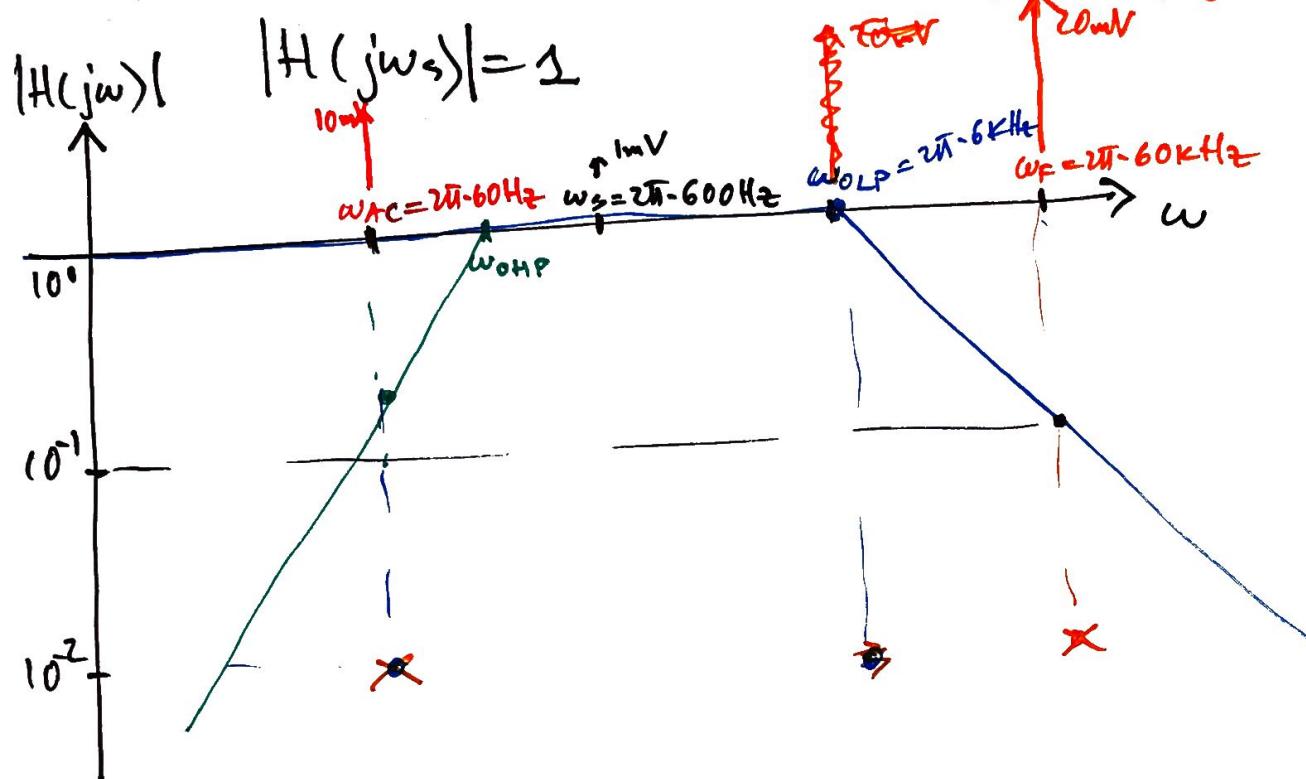
strategy:

$$\begin{aligned}
 V_{out}(+) = & |H(j\omega_{AC})| \cdot V_{AC} \cdot \cos(\omega_{AC}t + \phi_{AC} + \angle H(j\omega_{AC})) \\
 & + |H(j\omega_s)| \cdot V_s \cdot \cos(\omega_s t + \phi_s + \angle H(j\omega_s)) \\
 & + |H(j\omega_F)| \cdot V_F \cdot \cos(\omega_F t + \phi_F + \angle H(j\omega_F))
 \end{aligned}$$

Design goal:

$$|H(j\omega_{AC})| = \frac{1}{100} \quad |H(j\omega_F)| = \frac{1}{100}$$

(2)



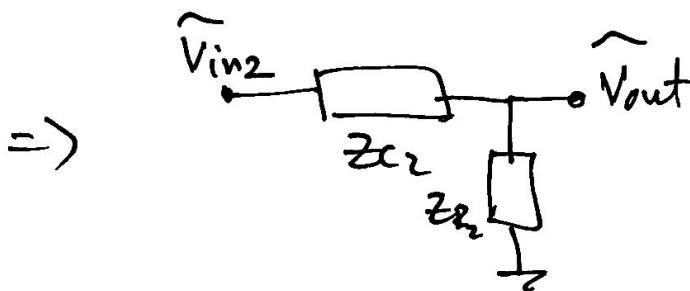
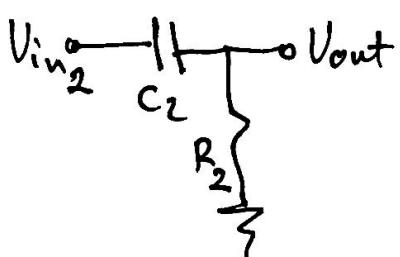
$H_{LP}(j\omega)$ - a "low-pass" filter



$$H_{LP}(j\omega) = \frac{\tilde{V}_{out_1}}{\tilde{V}_{in}} = \frac{1}{1 + j \frac{\omega}{\omega_{OLP}}} , \quad \omega_{OLP} = \frac{1}{R_1 C_1}$$

(13)

$H_{HP}(j\omega)$ - a "high-pass" filter



$$H_{HP}(j\omega) = \frac{\hat{V}_{out}}{\hat{V}_{in2}} = \frac{j \frac{\omega}{\omega_{0HP}}}{1 + j \frac{\omega}{\omega_{0HP}}} = \frac{1}{1 - j \frac{\omega_{0HP}}{\omega}}, \quad \omega_{0HP} = \frac{1}{R_2 C_2}$$

$$H(j\omega) = \frac{\hat{V}_{out}}{\hat{V}_{in}} = \frac{\hat{V}_{out}}{\hat{V}_{in2}} \cdot \underbrace{\frac{\hat{V}_{in2}}{\hat{V}_{out1}}}_{H_{HP}(j\omega)} \cdot \underbrace{\frac{\hat{V}_{out1}}{\hat{V}_{in}}}_{H_{LP}(j\omega)} = H_{HP}(j\omega) H_{AG}(j\omega) H_{LP}(j\omega)$$

$$= \frac{1}{1 + j \frac{\omega}{\omega_{0LP}}} \cdot \frac{1}{1 - j \frac{\omega_{0HP}}{\omega}}$$

Need to choose ω_{0LP} & ω_{0HP} .

Compromise - want to attenuate the interference w/o attenuating the signal.

$$\omega_{0HP} = \sqrt{\omega_{AC} \cdot \omega_S}$$

$$\log \omega_{0HP} = \frac{1}{2} \log \omega_{AC} + \frac{1}{2} \log \omega_S$$

$$\omega_{0LP} = \sqrt{\omega_S \cdot \omega_F}$$

$$\omega_{0HP} = \frac{1}{R_2 C_2}, \quad \omega_{0LP} = \frac{1}{R_1 C_1}$$

$$\omega_{0HP} = \sqrt{2\pi \cdot 60\text{Hz} \cdot 2\pi \cdot 600\text{Hz}} = 2\pi \cdot 190\text{Hz}$$

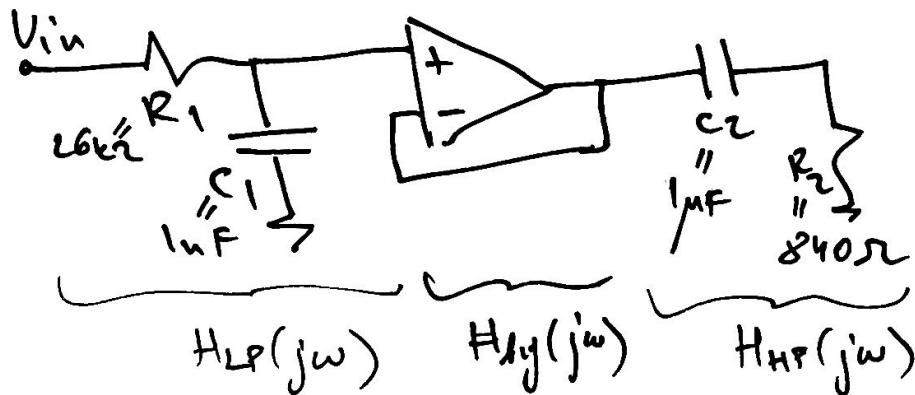
$$\omega_{0LP} = \sqrt{2\pi \cdot 600\text{Hz} \cdot 2\pi \cdot 60\text{kHz}} = 2\pi \cdot 6\text{kHz}$$

(24)

Pick a reasonable C :

$$C_1 = 1\text{nF} \Rightarrow R_1 = \frac{1}{\omega_{0LP} \cdot C_1} = 26\text{k}\Omega$$

$$C_2 = 1\mu\text{F} \Rightarrow R_2 = \frac{1}{\omega_{0HP} \cdot C_2} = 840\Omega$$



Check: Evaluate the TF $H(j\omega)$ @ $\omega_{AC}, \omega_S, \omega_F$

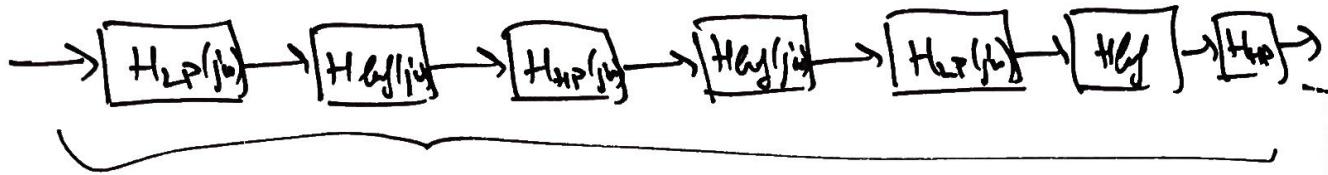
ω	$ H_{LP}(j\omega) $	$ H_{HP}(j\omega) $	$ H(j\omega) $	$V_{in} \cdot H(j\omega) = V_{out}$
$2\pi \cdot 60\text{Hz}$	$\frac{1}{\sqrt{1 + \left(\frac{2\pi \cdot 60\text{Hz}}{26\text{k}\Omega}\right)^2}} \approx 1$	$\frac{1}{\sqrt{1 + \left(\frac{2\pi \cdot 190\text{Hz}}{840\Omega}\right)^2}} \approx 0.3$	$1 \cdot 0.3 \approx 0.3$	$10\text{mV} \cdot 0.3 = 3\text{mV}$
$2\pi \cdot 600\text{Hz}$	$\frac{1}{\sqrt{1 + \left(\frac{2\pi \cdot 600\text{Hz}}{26\text{k}\Omega}\right)^2}} \approx 1$	≈ 0.95	$1 \cdot 0.95 \approx 0.95$	$1\text{mV} \cdot 0.95 = 0.95\text{mV}$
$2\pi \cdot 60\text{kHz}$	$\frac{1}{\sqrt{1 + \left(\frac{2\pi \cdot 60\text{kHz}}{26\text{k}\Omega}\right)^2}} = 0.1$	≈ 1	$1 \cdot 0.1 = 0.1$	$20\text{mV} \cdot 0.1 = 2\text{mV}$

Wanted $\frac{1}{100}$ for $|H_{HP}(j\omega_{AC})|$ & $|H(j\omega_F)|$

but only got $0.3 < 0.1$ - not quite enough.



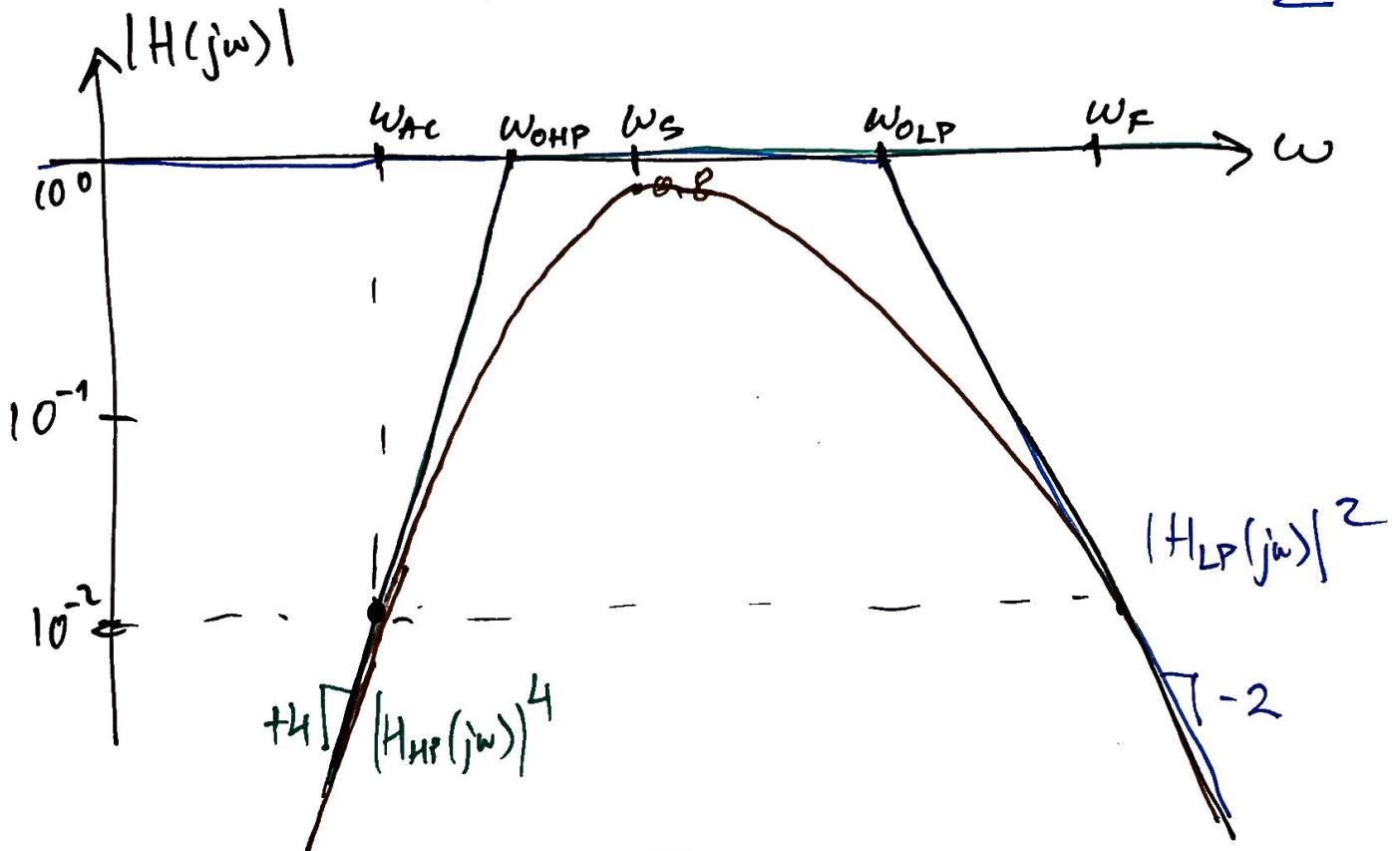
Can keep going ...



$$H_{\text{tot}}(j\omega) = H_{\text{LP}}^m(j\omega) H_{\text{HP}}^m(j\omega)$$

$$|H_{\text{tot}}(j\omega_{\text{ac}})| = \frac{1}{100} = 1^m \cdot 0.3^m \Rightarrow m=4$$

$$|H_{\text{tot}}(j\omega_F)| = \frac{1}{100} = 0.1^n \cdot 1^m \Rightarrow \cancel{n=2}$$



$$|H_{\text{tot}}(j\omega_s)| = 1^m \cdot 0.95^m = 0.8 \quad (\text{o.k. but not great})$$

$$H_{\text{tot}}(j\omega) = \frac{\left(j \frac{\omega}{\omega_{0\text{HP}}}\right)^4}{\left(1 + j \frac{\omega}{\omega_{0\text{HP}}}\right)^4 \cdot \left(1 + j \frac{\omega}{\omega_{0\text{LP}}}\right)^2}$$

In general:

$$H(j\omega) = K \frac{(j\omega)^{N_{z_0}} (1+j\frac{\omega}{\omega_{z_1}}) \dots (1+j\frac{\omega}{\omega_{z_n}})}{(j\omega)^{N_{po}} (1+j\frac{\omega}{\omega_{p_1}}) \dots (1+j\frac{\omega}{\omega_{p_m}})}$$

↑ origin poles
↓ origin zeros

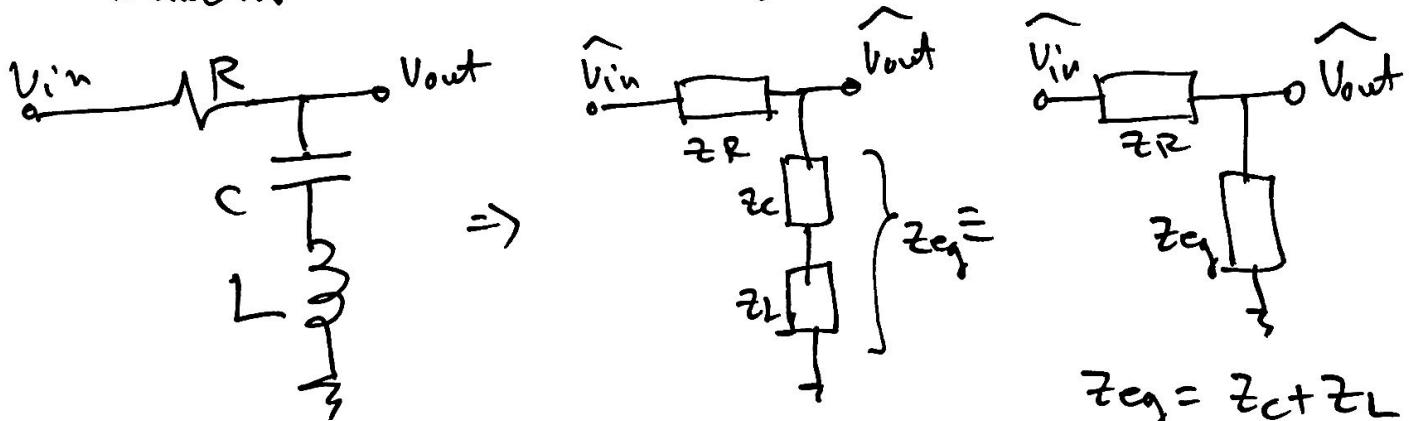
ω_{z_n} - zeroes } control system terminology
 ω_{p_m} - poles } $(105, 120, \dots)$

What if our desired signal is at 100 Hz?

- Our previous design won't work 😞

Need a different filter!

Inductor to the rescue!



$$Z_{eg} = Z_C + Z_L = \frac{1}{j\omega C} + j\omega L = j(\omega L - \frac{1}{\omega C})$$

Fantastic!

$$H(j\omega) = \frac{\hat{V}_{out}}{\hat{V}_{in}} = \frac{Z_{eg}}{Z_{eg} + Z_R} =$$

$$\text{say } Z_{eg}(j\omega_0) = 0 = j(\underbrace{\omega_0 L - \frac{1}{\omega_0 C}}_0)$$

(67)

$$\omega_0 = \frac{1}{\sqrt{LC}}$$

$$|H(j\omega_0)| = \left| \frac{\cancel{z_{eg}(j\omega_0)}^0}{\cancel{z_{eg}(j\omega_0) + z_R}^0} \right| = \left| \frac{0}{\cancel{z_R}^R} \right| = 0$$

$$H(j\omega) = \frac{j(\omega L - \frac{1}{\omega C})}{R + j(\omega L - \frac{1}{\omega C})}$$

$$\omega_0 = \omega_{AC} = 2\pi \cdot 60 \text{ Hz}$$

$$C = 100 \mu\text{F} \Rightarrow L = 70 \text{ mH}$$

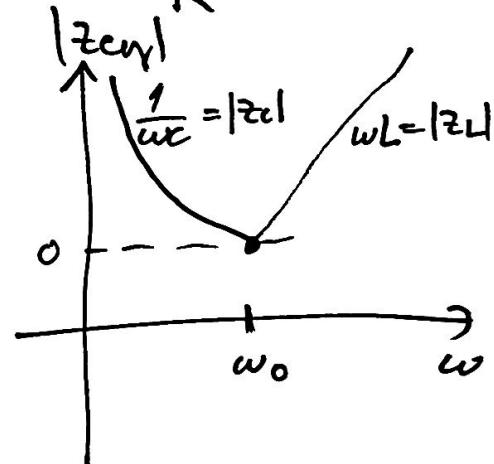
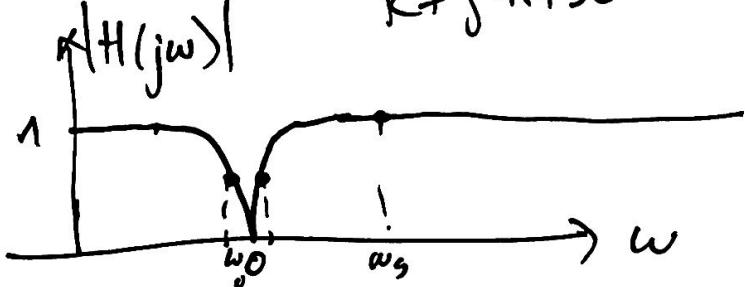
$$H(j\omega_0) = 0$$

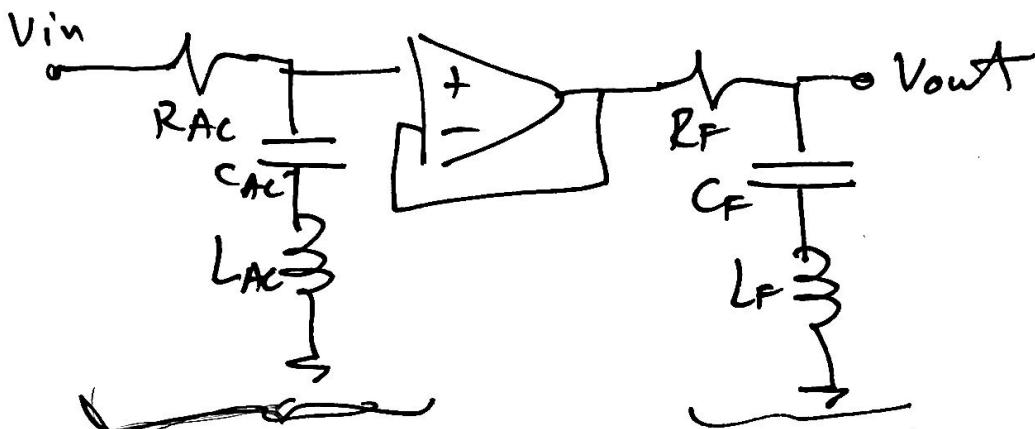
" $2\pi \cdot 60 \text{ Hz}$ "

$$H(j2\pi \cdot 55 \text{ Hz}) = \frac{j \cdot 3.5 \Omega}{R + j3.5 \Omega} \quad \cancel{\text{Ansatz}} \quad \text{approx } R = 3 \Omega$$

$$H(j2\pi \cdot 65 \text{ Hz}) = \frac{j 4.7 \Omega}{R + j4.7 \Omega} \quad \cancel{\text{Ansatz}}$$

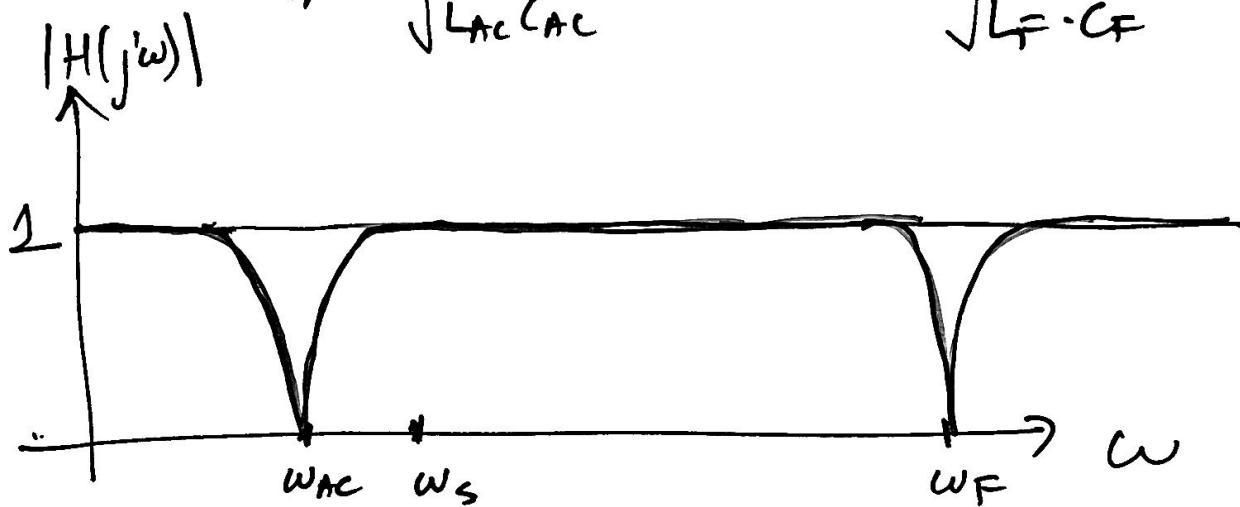
$$|H(j2\pi \cdot 55, 65)| \approx 0.5$$





$$\omega_{AC} = \frac{1}{\sqrt{L_{AC}C_{AC}}}$$

$$\omega_{AF} = \frac{1}{\sqrt{L_F \cdot C_F}}$$



Band-pass:

