



The background image shows a detailed microchip layout with various functional blocks highlighted by dashed yellow boxes. The labels include 'RX' (Receiver), 'LO Buffer' (Local Oscillator Buffer), 'Hybrid', 'Wilkinson' (referring to a Wilkinson power divider), 'LO Buffer' (another instance), and 'TX' (Transmitter). The layout features a dense grid of circuit traces and components.

EECS 16B

Designing Information Devices and Systems II

Prof. Ali Niknejad and Prof. Kannan Ramchandran
Department of Electrical Engineering and Computer Sciences, UC Berkeley,
niknejad@berkeley.edu

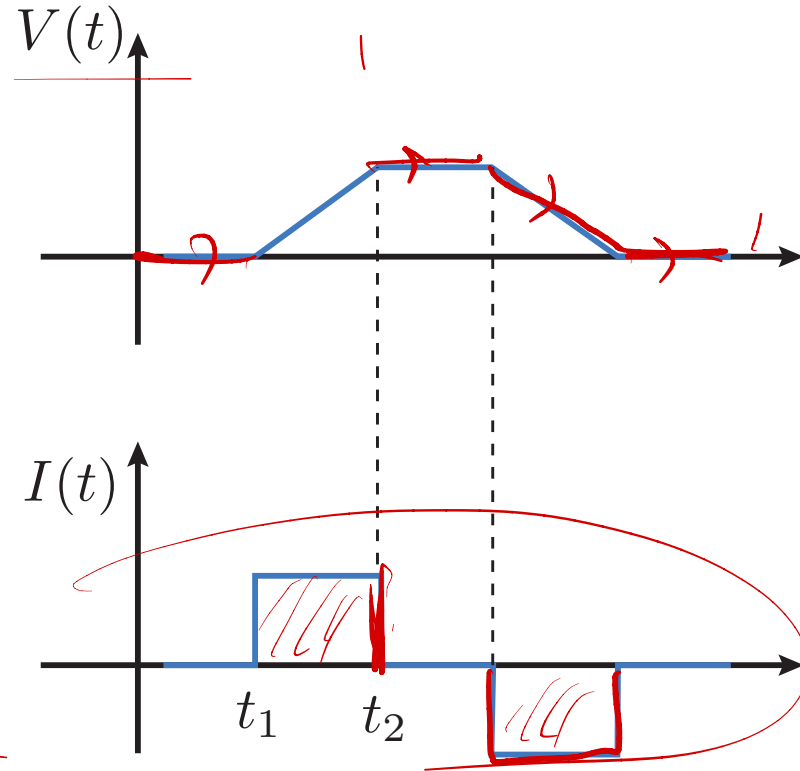
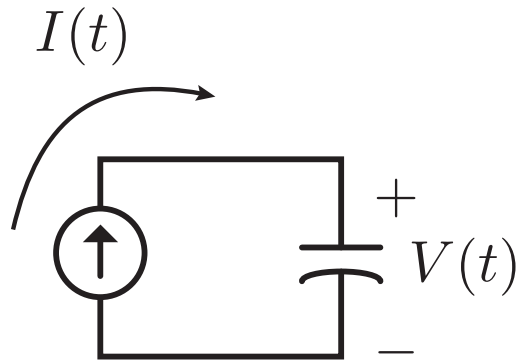
Module 2: RC Circuits, Digital Logic Gates, and Transfer Functions

EECS 16B

RC Circuits

- Solve RC with and without inputs
 - “Natural” response and “forced” response
 - “Moving Average” (Convolution Integral)
- Step Response
- Pulse Response
- Preview: Sinusoidal Steady-State Response
- Low Pass vs High Pass
- Introduction to Transistors

Capacitor Discharge: Linear



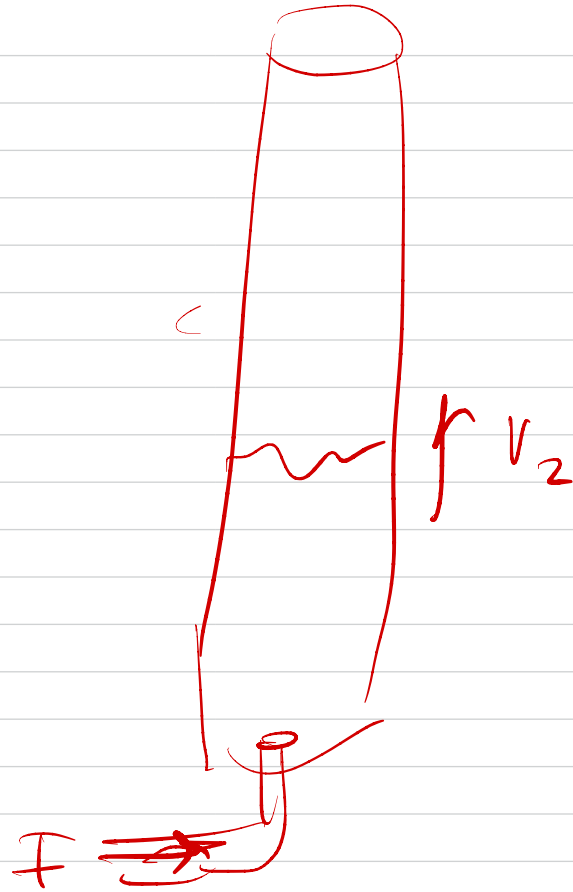
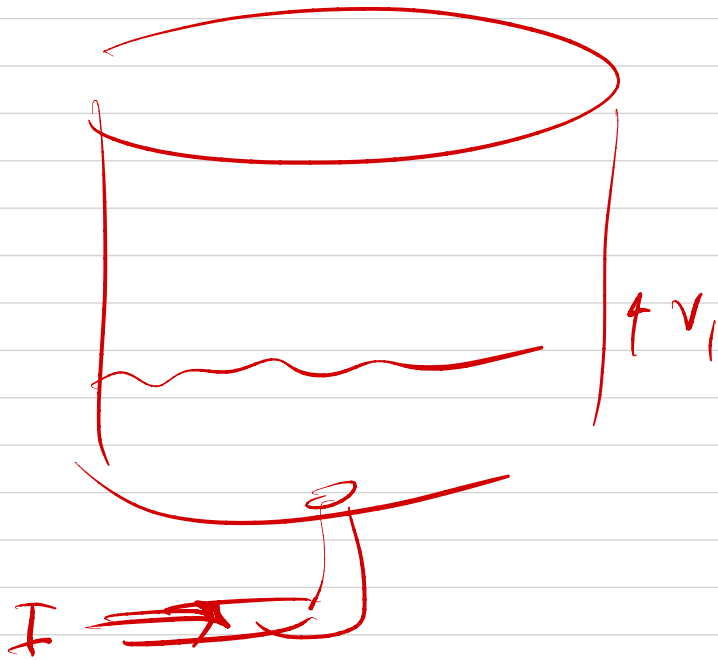
$k=0$
 $V(0)=0$

$$I(t) = C \frac{dV}{dt}$$

$$\int \frac{1}{C} I(t) dt = \int \frac{dV}{dt} dt$$

$$= V(t) + k$$

$$V(t) = k + \frac{1}{C} \int I(t) dt$$

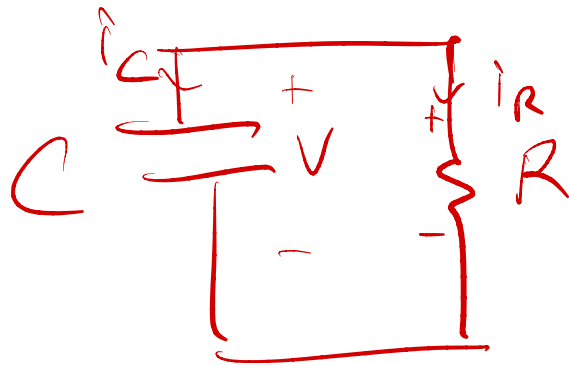


Capacitor Discharge

- Water analogy: Rate of outflow is not constant but depends on the height of the water in the tank (the pressure)

RC Circuit

- Can't solve by "inspection", need to solve differential equation



$$V(t) = ?$$

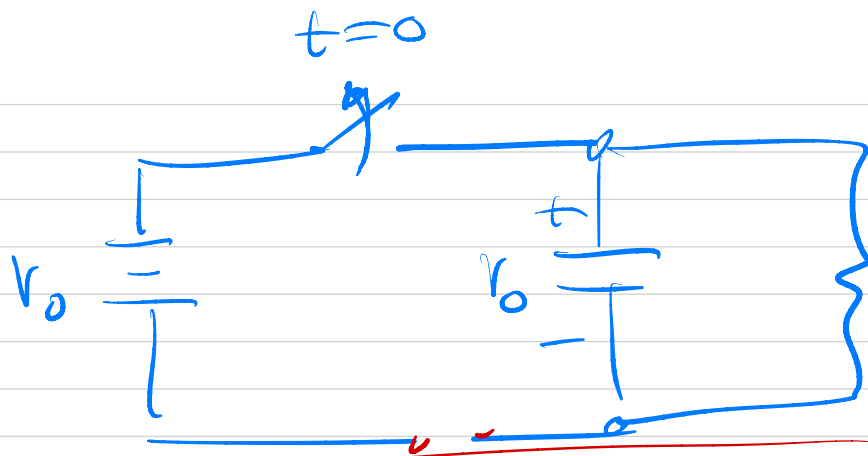
$$i = C \frac{dV}{dt} = - \left(\frac{V}{R} \right)$$

$$\frac{V}{R} + C \frac{dV}{dt} = 0$$

$$V + RC \frac{dV}{dt} = 0$$

Initial Condition

$$V(0) = V_0$$



$$v + RC \frac{dv}{dt} = 0$$

$$1 + RC \frac{1}{\tau} = 0$$

$$\tau = -RC$$

$$v(t) = K e^{t/\tau}$$

$$\cancel{K} e^{\cancel{t/\tau}} + RC \frac{1}{\tau} \cancel{K} e^{\cancel{t/\tau}} = 0$$

RC Solution

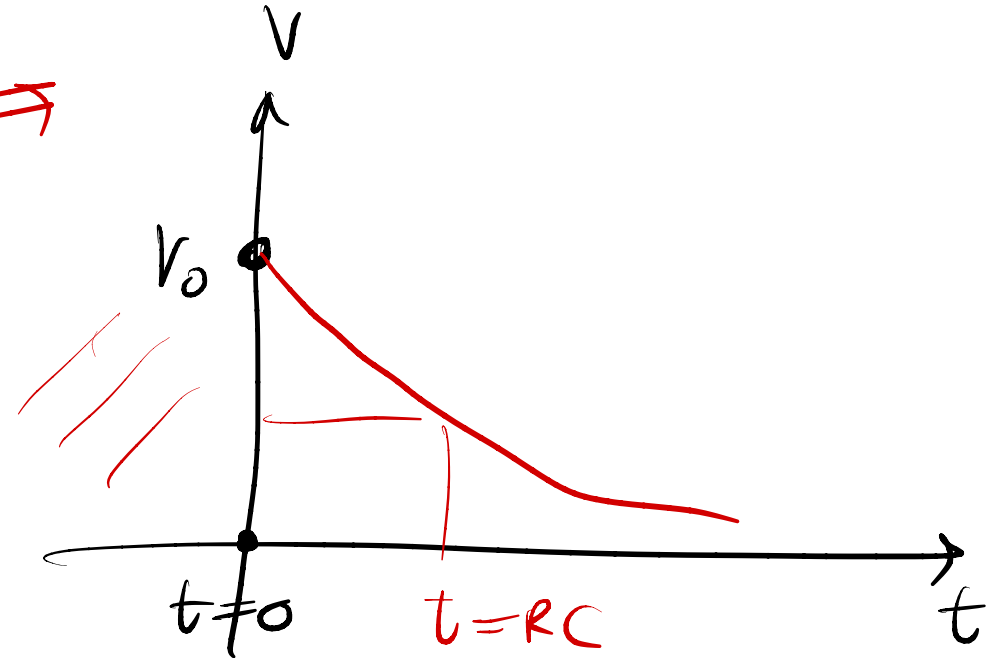
- Easy to guess for first-order equation

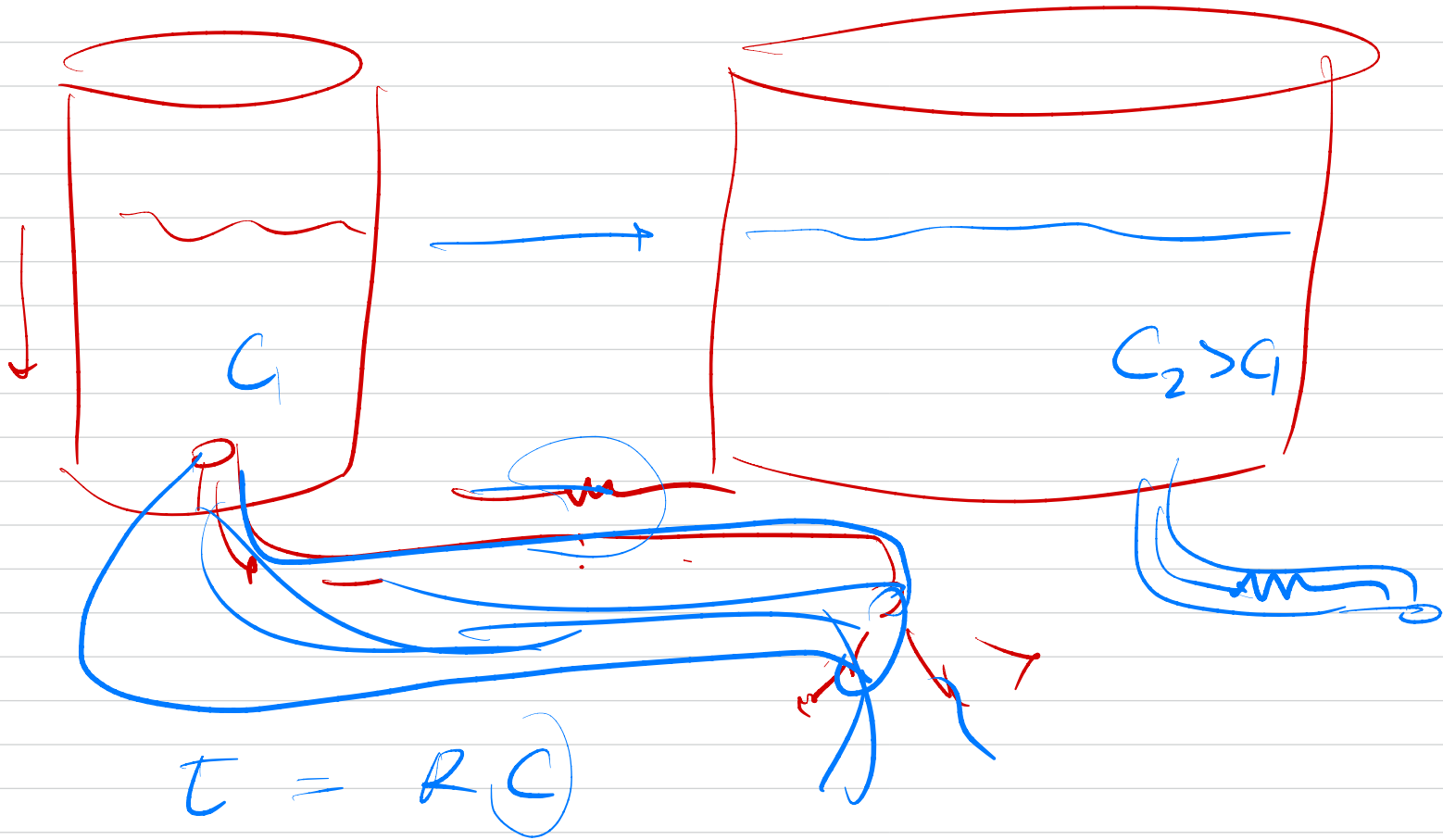
$$V(t) = K e^{-t/\tau'}$$

$$\tau' = RC$$

$$V(0) = V_0 = K \Rightarrow$$

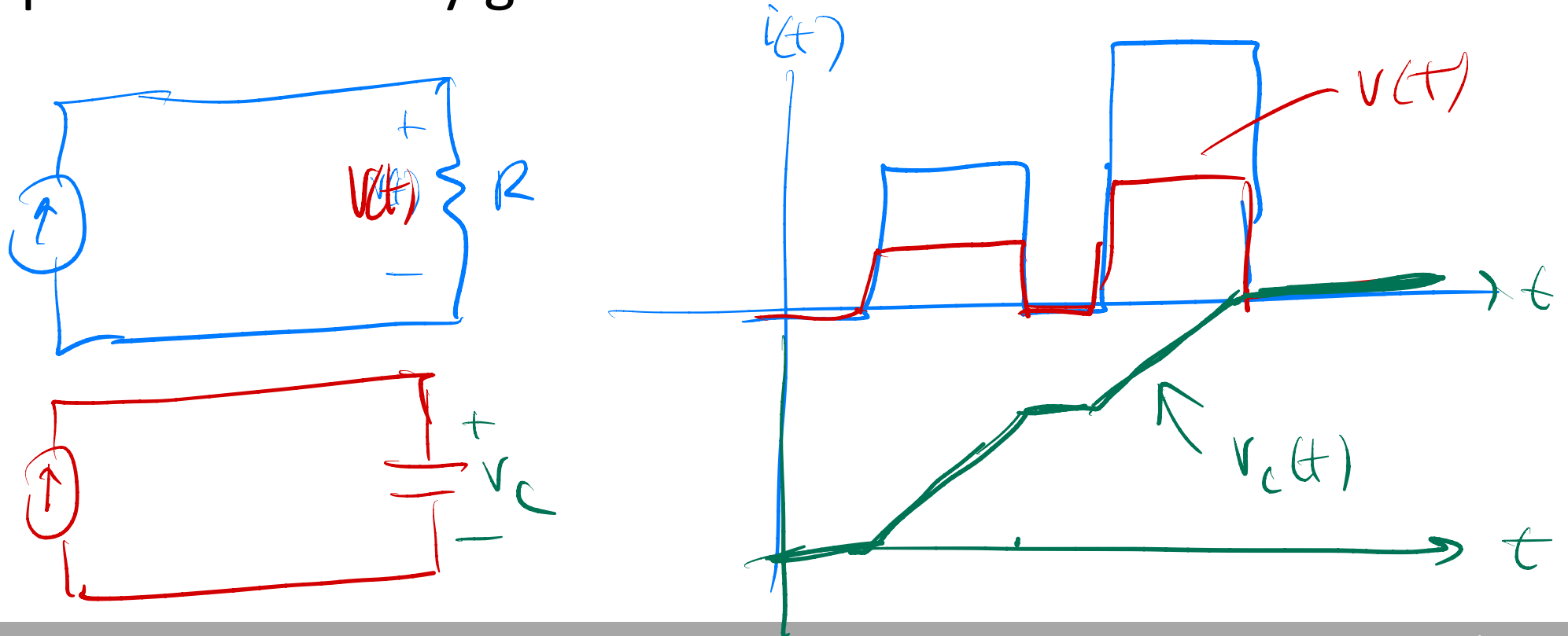
$$V(t) = V_0 e^{-t/\tau'}$$





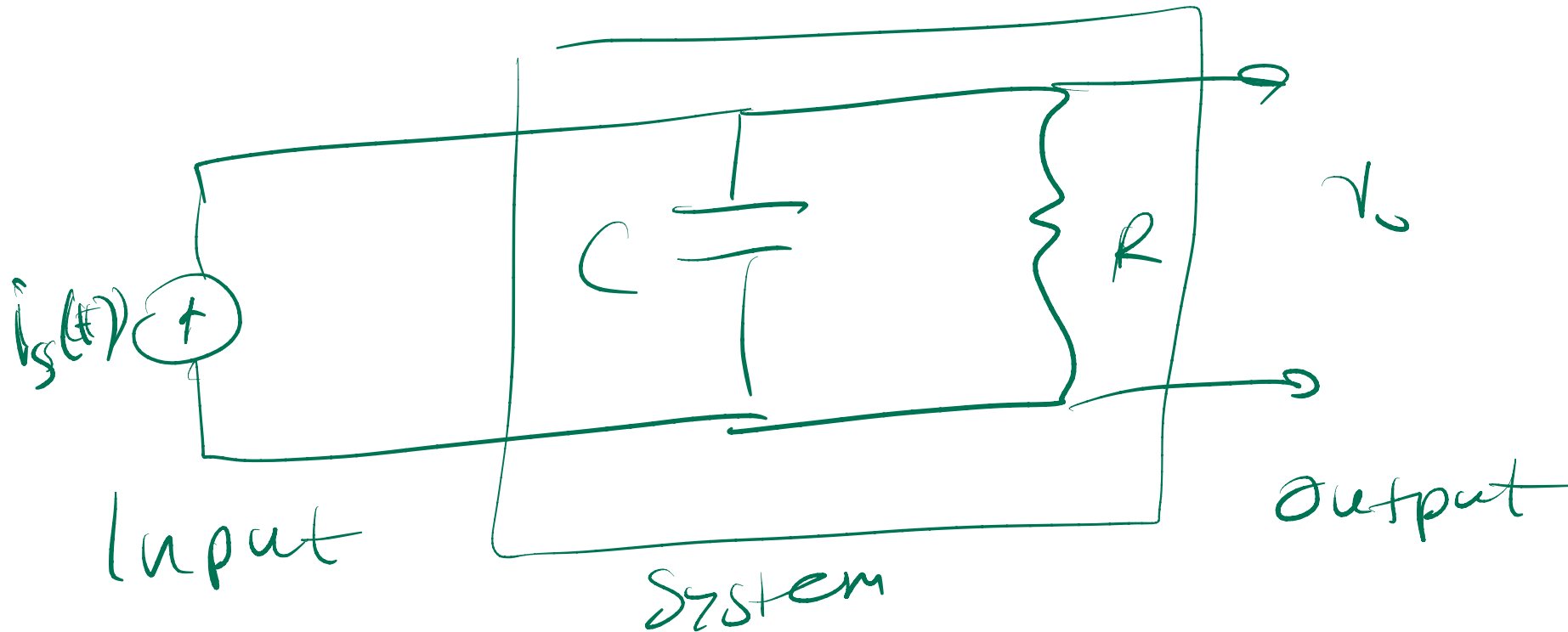
Capacitor Has “Memory”

- A resistive circuit without capacitors has no memory, the transfer function is instantaneous and if the input goes to zero, the output immediately goes to zero.



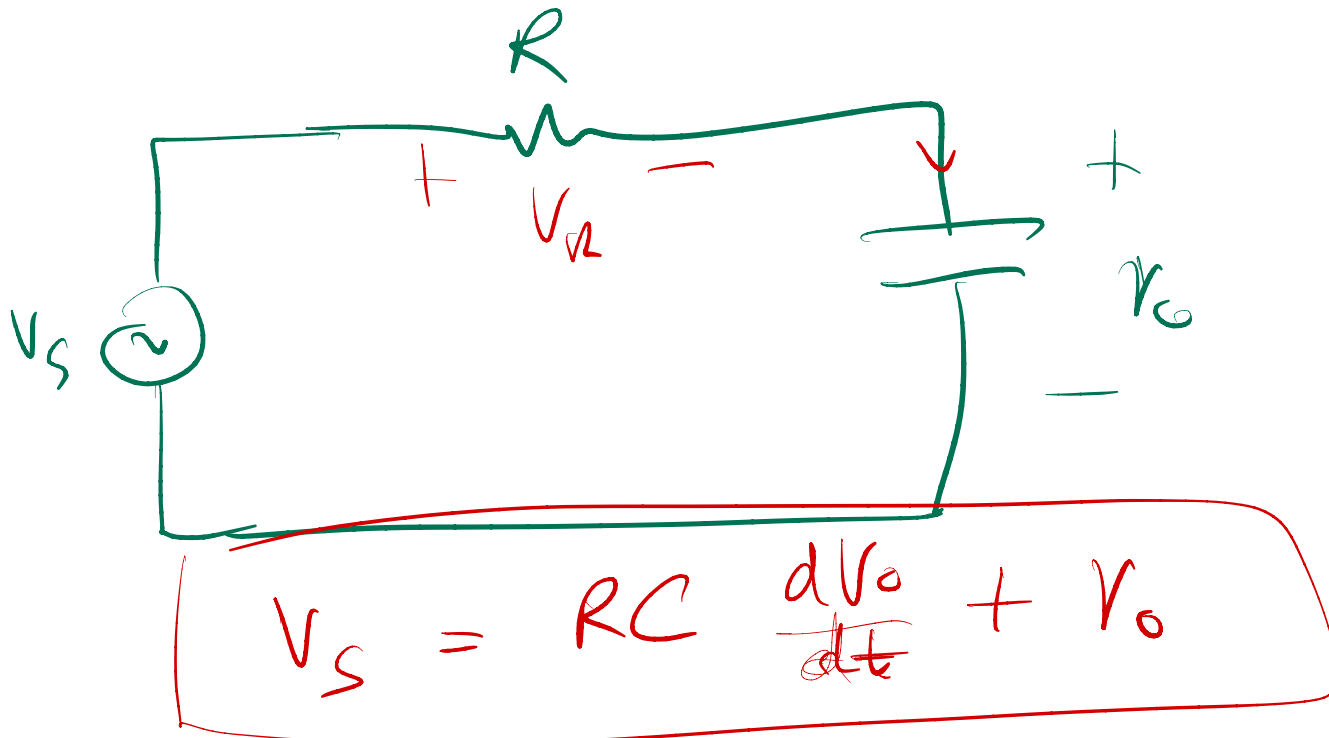
Circuit as a System

- Consider inputs (independent voltage/current sources) and outputs (voltages or currents at any node or in any branch of the circuit). Dependent sources are not inputs.



Linear Constant Coefficient Differential Eq.

- Homogenous solution: No inputs. Sometimes called the “natural” solution
- Forced response or a *particular* solution



$$\begin{aligned} V_S &= V_R + V_C \\ i_C &= C \frac{dV_C}{dt} \\ V_R &= RC \frac{dV_C}{dt} \end{aligned}$$

Superposition

- Equation is linear, so a superposition of solutions is also a solution.

$$0 = \tau \frac{dV_0}{dt} + V_0$$

$$0 = \tau \frac{d\psi_1}{dt} + \psi_1$$

$$\psi_1(0) = C_1$$

$$0 = \tau \frac{d\psi_2}{dt} + \psi_2$$

$$\psi_2(0) = C_2$$

$$\psi = C_1 \psi_1 + C_2 \psi_2$$

$$0 = \tau \frac{d(\alpha_1 \psi_1 + \alpha_2 \psi_2)}{dt} + \alpha_1 \dot{\psi}_1 + \alpha_2 \dot{\psi}_2$$

$$= \underbrace{\left(\tau \frac{d\psi_1}{dt} + \psi_1 \right)}_0 \alpha_1 + \underbrace{\left(\tau \frac{d\psi_2}{dt} + \psi_2 \right)}_0 \alpha_2$$

Uniqueness

- Note that for a first-order differential equation, there can be at most one unique solution for the homogenous case

$$\psi_{\text{diff}} = \psi_1 - \psi_2$$

$$\psi_1(0) = C$$

$$\psi_2(0) = C$$

$$\tau \frac{d\psi_{\text{diff}}}{dt} + \psi_{\text{diff}} = 0$$

$$\psi_{\text{diff}}(0) = 0$$

$$\psi_{\text{diff}} \equiv 0$$

$$\Rightarrow \psi_1 = \psi_2$$

General Solution

$$v = v_0 + v_p$$

homogeneous solution

particular solution

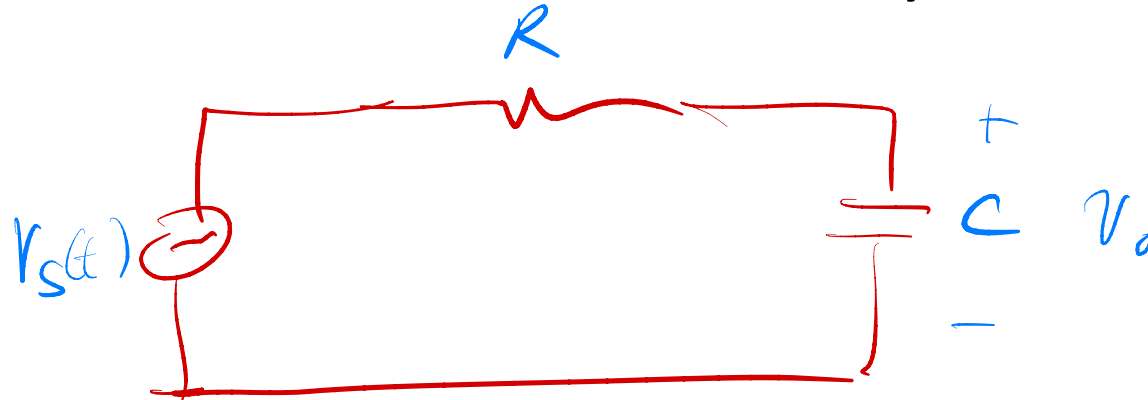
$$v_s = \tau \frac{dv}{dt} + v$$

$$= \tau \frac{d}{dt} (v_0 + v_p) + (v_0 + v_p)$$

$$= \left(\tau \frac{dv_0}{dt} + v_0 \right) + \left(\tau \frac{dv_p}{dt} + v_p \right)$$

RC Circuit with Inputs

- Now consider an arbitrary source connected to an RC circuit.



$$V_h = K e^{-t/\tau}$$

$$e^{st} v_s(t) = \left(\tau \frac{dv}{dt} + v \right) e^{st}$$

$$(v e^{st})' = v' e^{st} + s v e^{st}$$

$$= \tau e^{st} \frac{dv}{dt} + v e^{st}$$

$$= \tau \left(e^{st} v' + \frac{1}{\tau} v e^{st} \right) \quad s = \frac{1}{\tau} \quad \tau \left(e^{st} v \right)'$$

Solution with Inputs (Integrating Factor)

$$e^{st} v_s(t) = \tau (e^{st} v(t))'$$

$$\int e^{st} v_s(t) dt = \tau (e^{st} \underline{v(t)} + K)$$

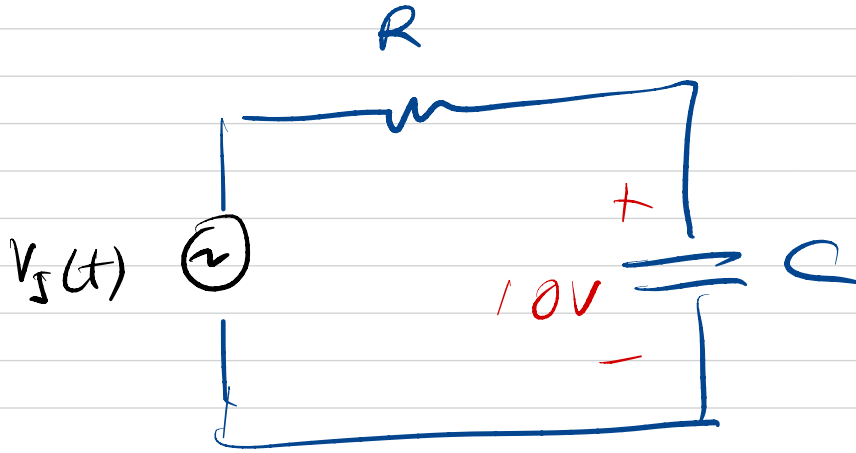
$$v(t) = \underbrace{\frac{1}{\tau} e^{-st}}_{s = 1/\tau} \int_{-\infty}^t e^{sx} v_s(x) dx + \underbrace{K e^{-st}}_{\text{homogeneous solution}}$$

Complete Solution

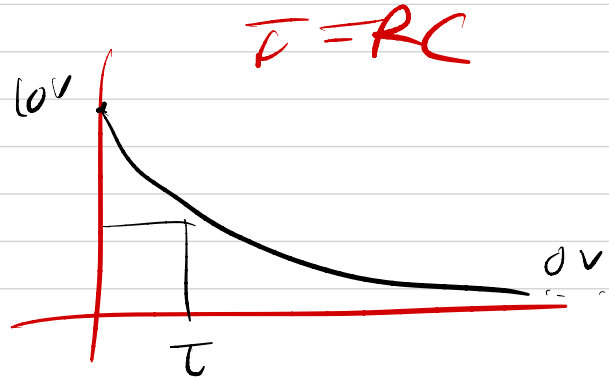
$$v(t) = \frac{1}{\tau} e^{-st} \int_{-\infty}^t e^{sx} v_s(x) dx + k e^{-st}$$

$$\begin{aligned} v_p &= \frac{1}{\tau} e^{-st} \int_0^t e^{sx} v_s dx \\ &= \frac{1}{\tau} e^{-st} v_s \int_0^t e^{sx} dx \\ &= \frac{1}{\tau} e^{-st} v_s \left[\frac{e^{sx}}{s} \right]_0^t = v_s \end{aligned}$$

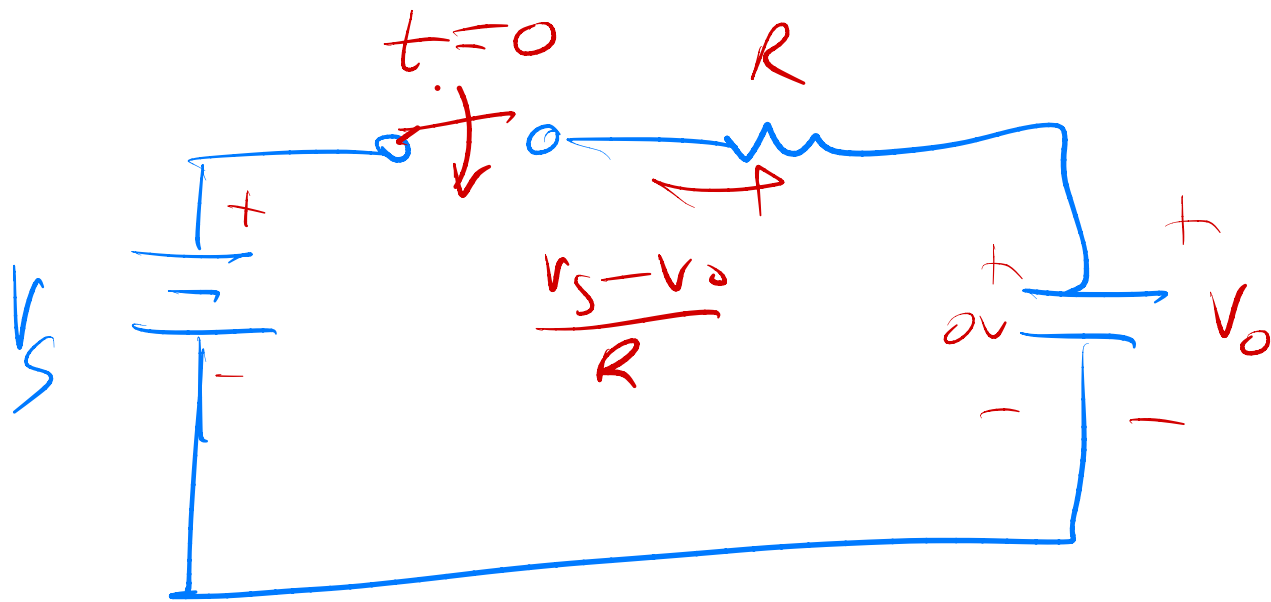
Homogeneous Solution



$$v_c(t) = v(0) e^{-t/\tau}$$



RC Circuits with DC Inputs



$$V_o(0) = 0 = V_S + K$$

$$K = -V_S$$

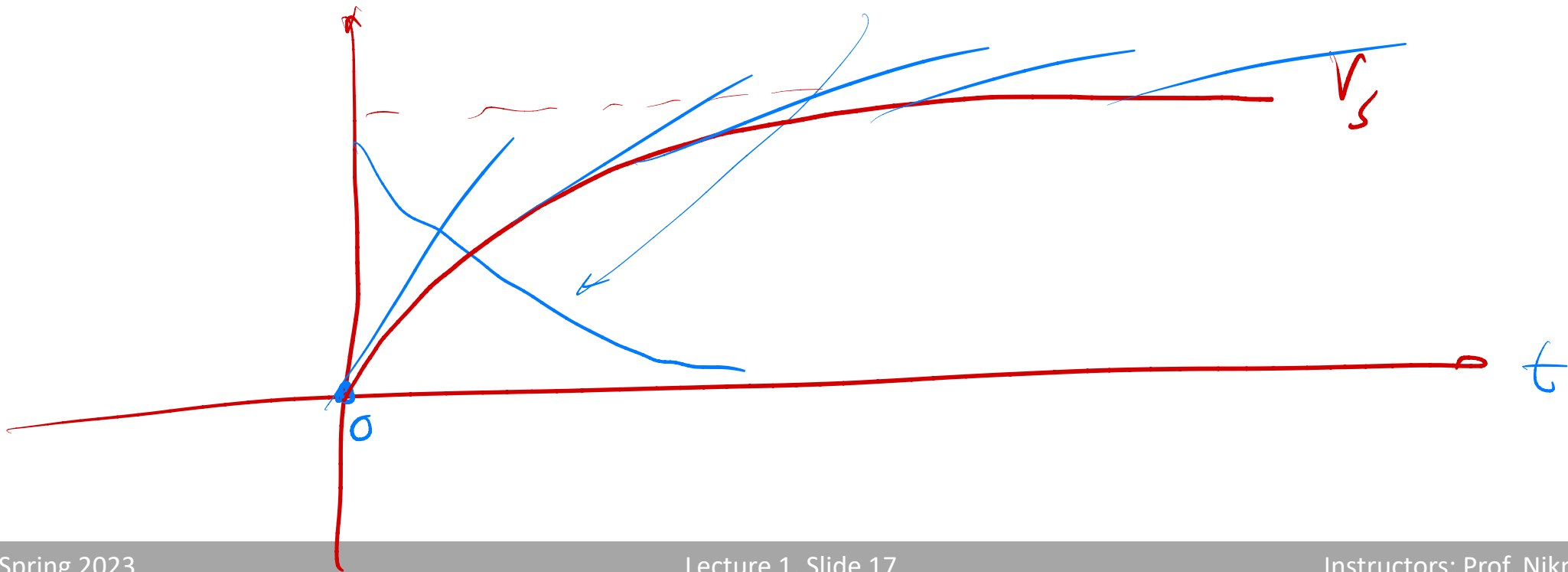
$$V_o(0) = 0V$$

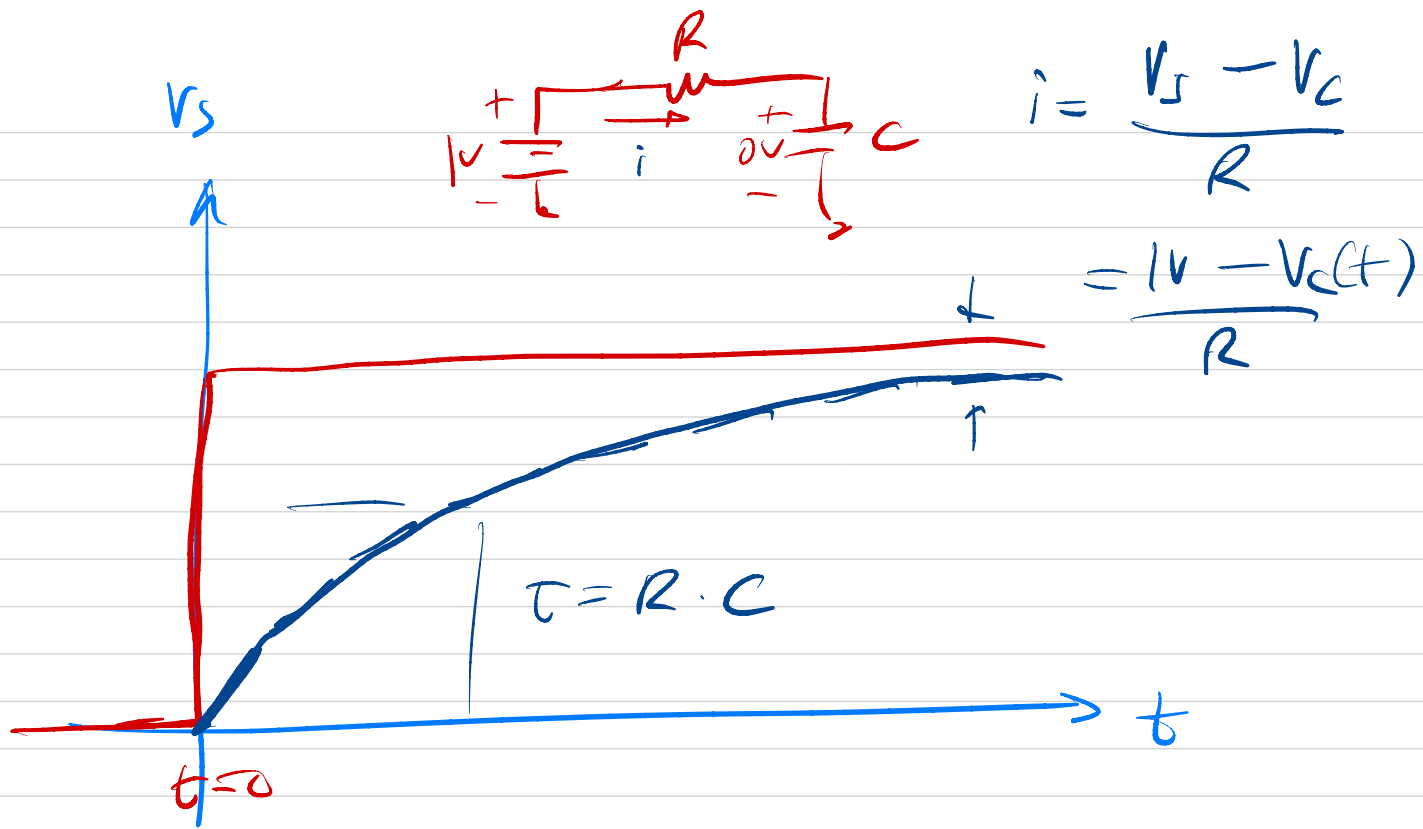
$$V_o(t) = V_S + K e^{-t/\tau} = 0$$

particular solution

Switching Circuits

$$V(t) = V_s + k e^{-t/\tau}$$
$$= V_s (1 - \underbrace{e^{-t/\tau}})$$





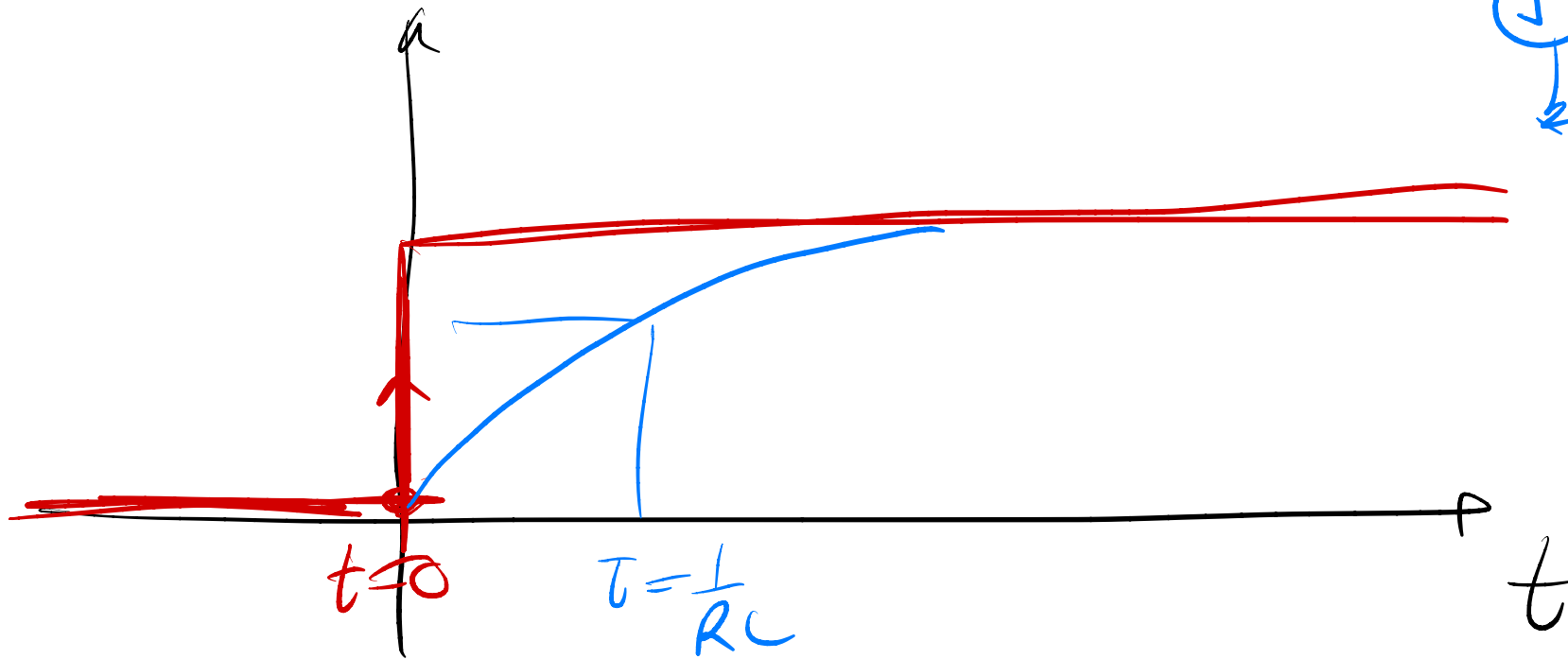
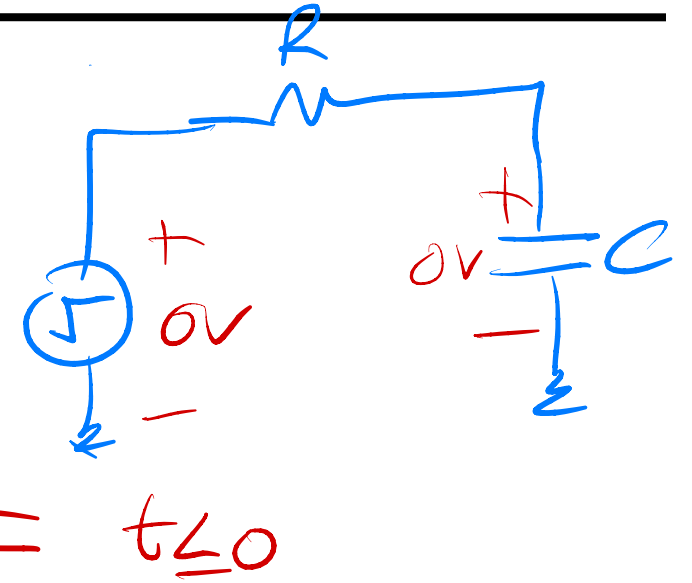
$$C i = C v$$

$$i = C \frac{dv}{dt}$$

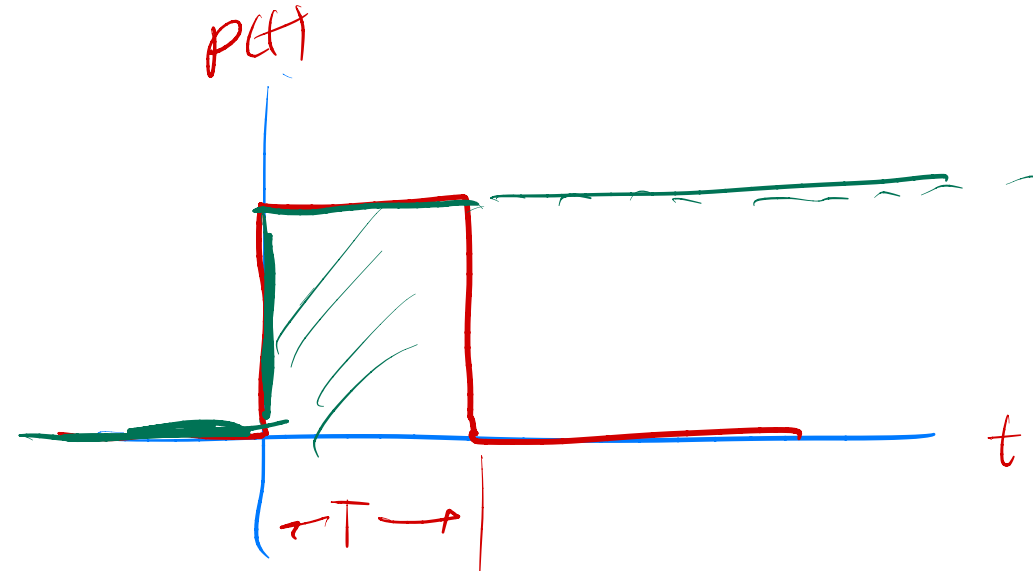
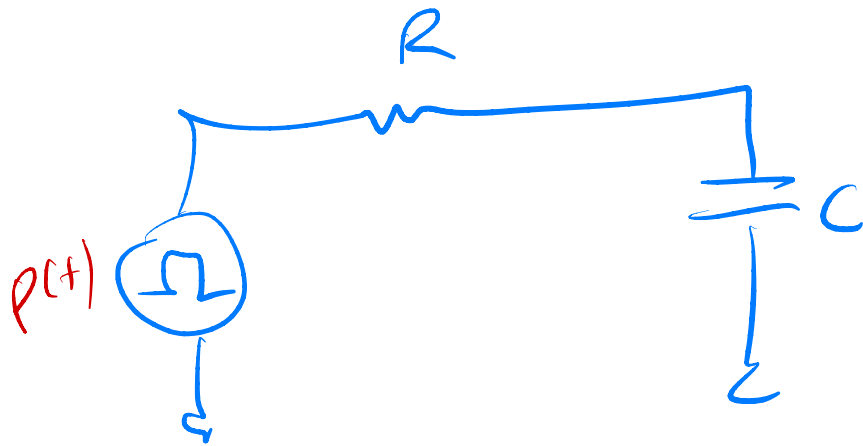
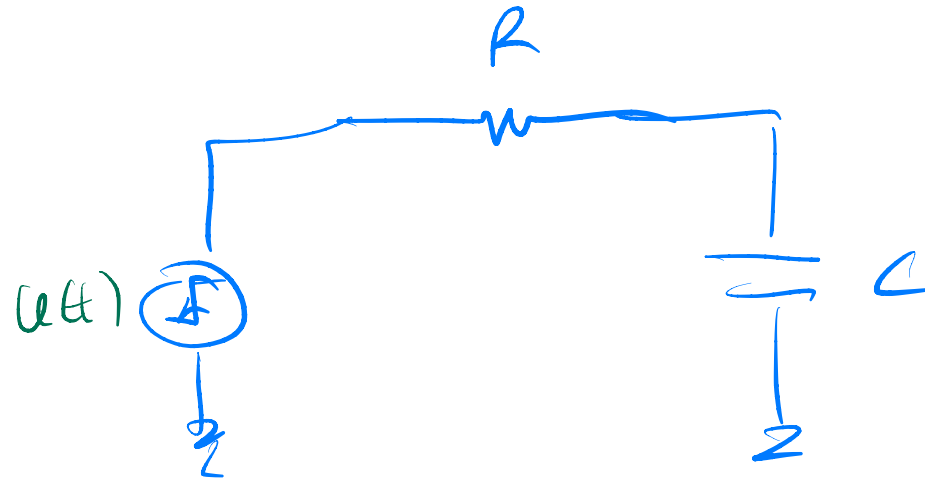
$$V(t) = \frac{1}{C} \int_0^t i(x) dx + V(0)$$

Step Response

$$V_S(t) = u(t) \quad \leftarrow \text{For Input}$$



Source Superposition



$$p(t) = u(t) - u(t - T)$$

delayed
step
func

Pulse Response

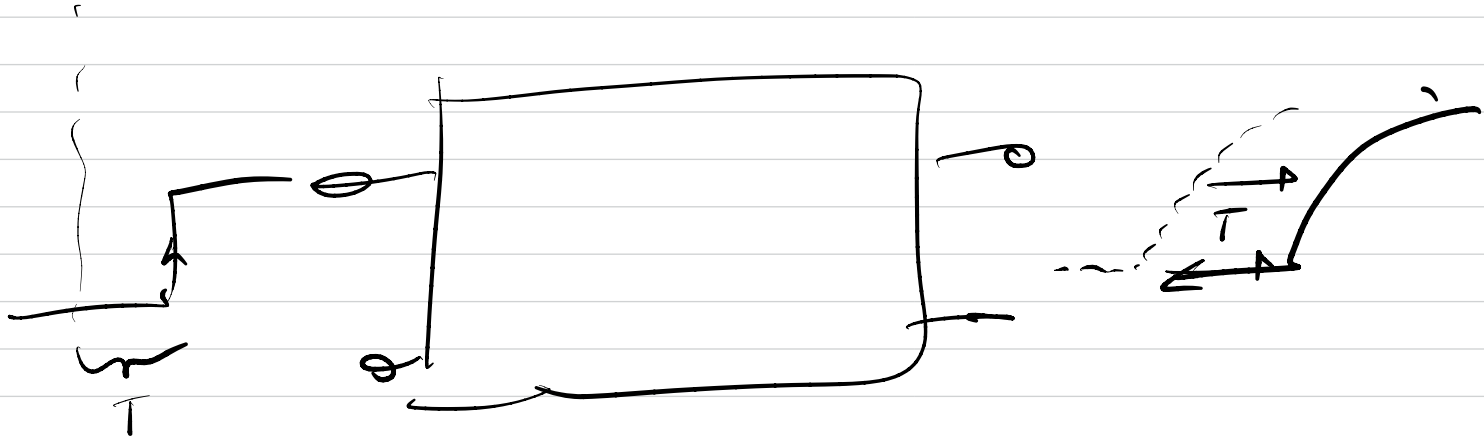
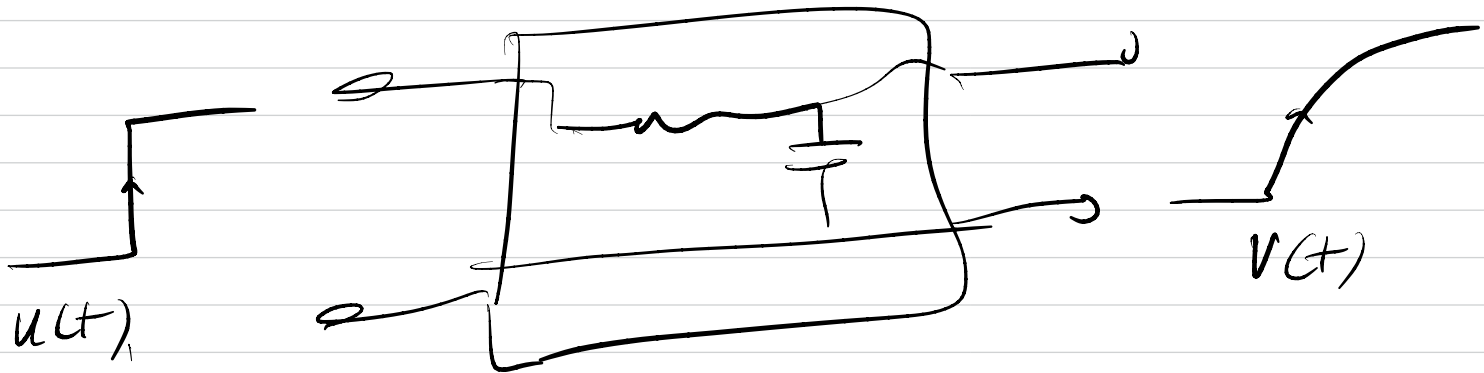
$$p(t) = \tau \frac{dv_c}{dt} + v_c \quad \tau = RC$$

$$\underline{u(t)} - u(t-\tau) = \tau \frac{dv_c}{dt} + v_c$$

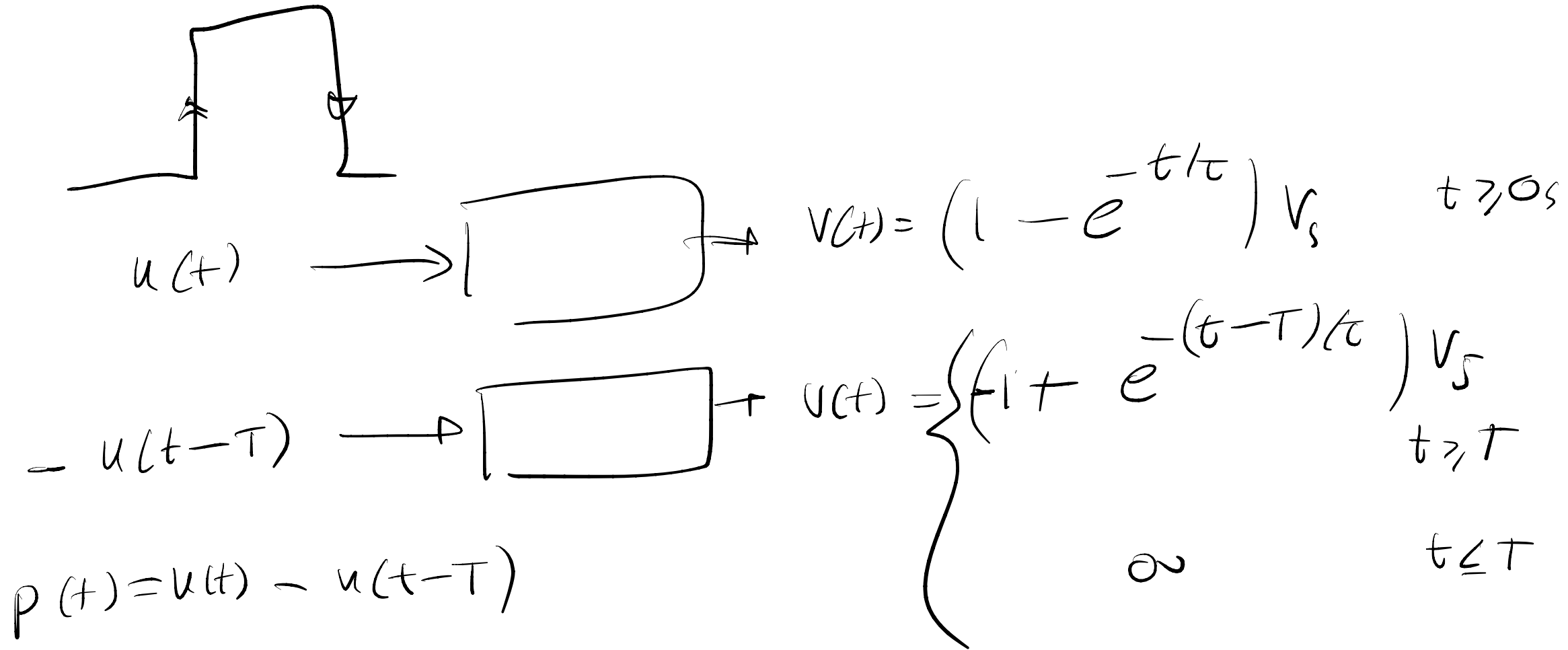
$$= \tau \frac{d(\tilde{v}_c + \tilde{\tilde{v}}_c)}{dt} + (\tilde{v}_c + \tilde{\tilde{v}}_c)$$

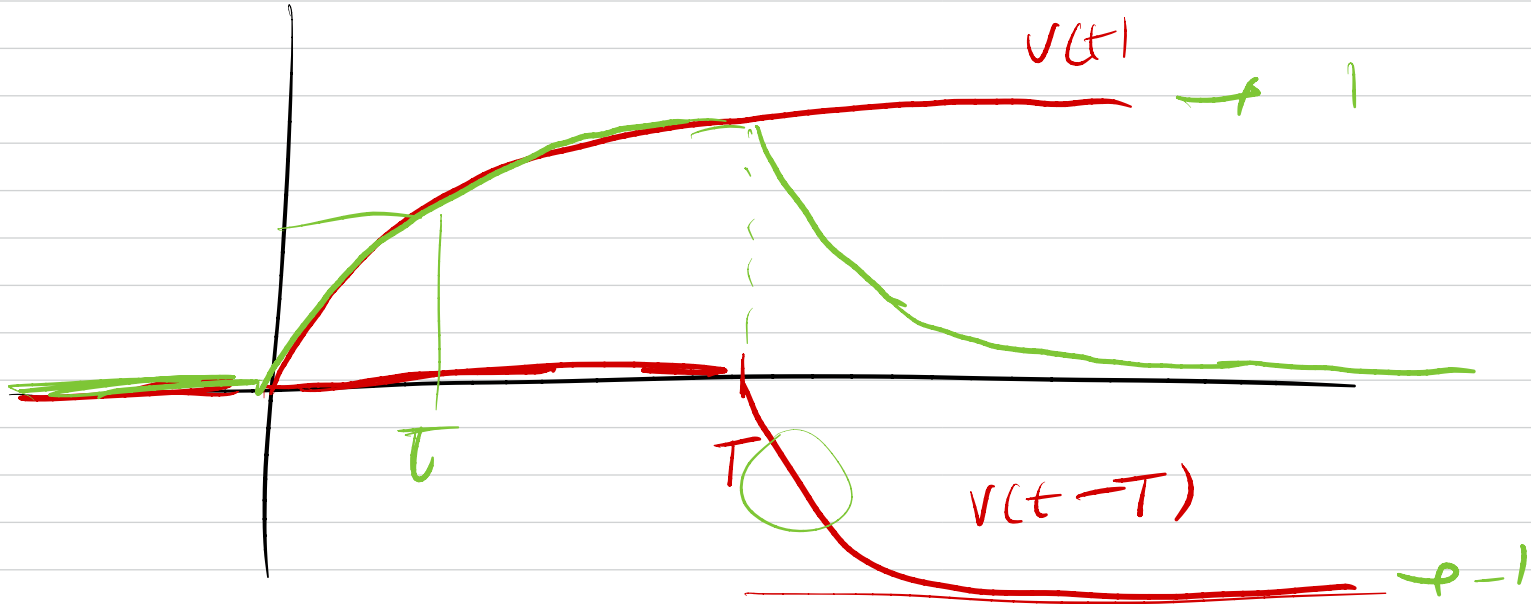
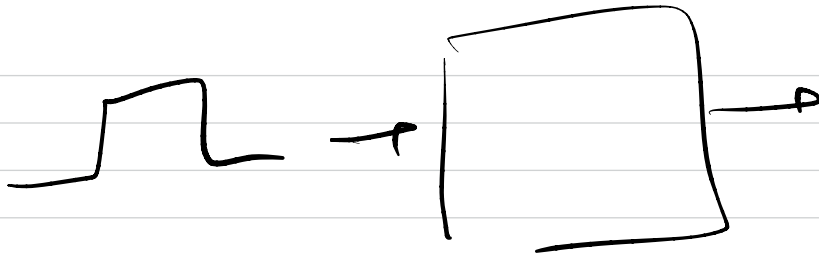
$$u(t) = \tau \left(\frac{d\tilde{v}_c}{dt} + \tilde{v}_c \right) \quad \begin{array}{l} \text{Input \#1} \\ \rightarrow \text{solve} \end{array}$$

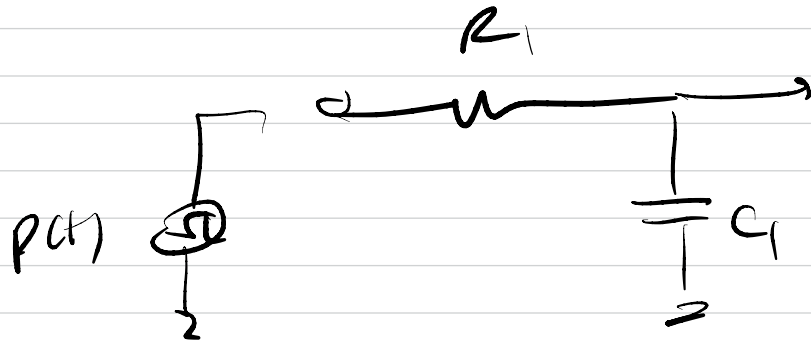
$$u(t-\tau) = \tau \left(\frac{d\tilde{\tilde{v}}_c}{dt} + \tilde{\tilde{v}}_c \right) \quad \begin{array}{l} \text{Input \#2} \\ \rightarrow \text{solve} \end{array}$$



Smearing Out Pulses

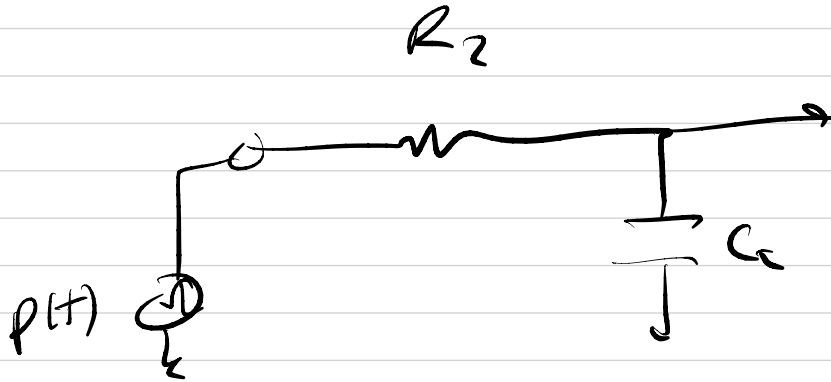






$$T = 1 \text{ ms}$$

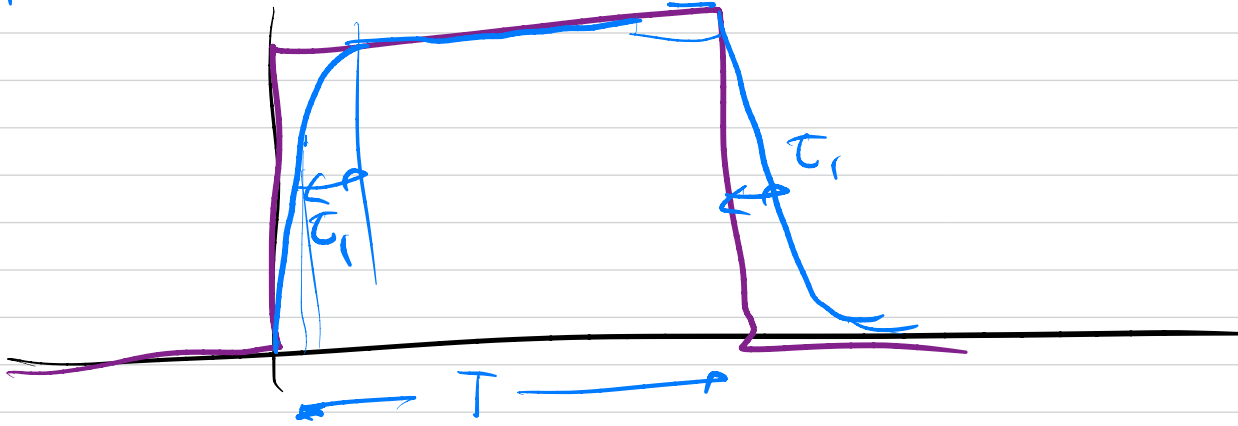
$$\tau_1 = R_1 C_1 = 0.1 \text{ ms}$$



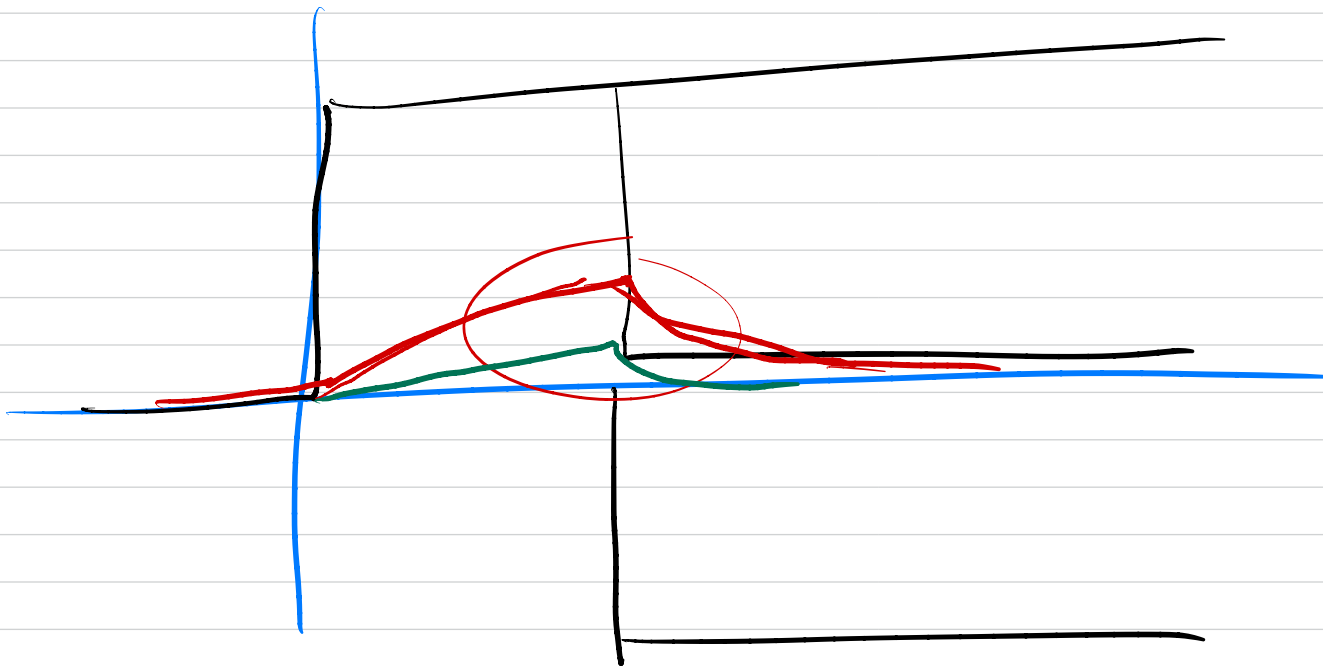
$$\tau_2 = R_2 C_2 = 10 \text{ ms}$$

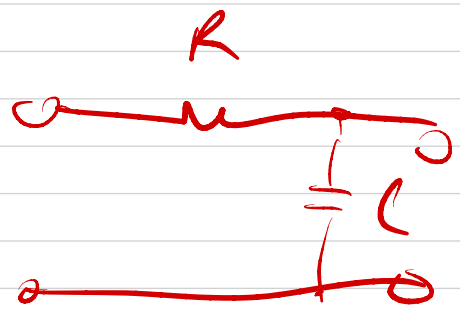
$$\tau_1 = R_1 C_1$$

"FAST CIRCUIT"



$$t_2 = R_2 C_2 \gg T$$





Reformulation of General Solution

$$\begin{aligned}v(t) &= \frac{1}{\tau} \underline{e^{-t/\tau}} \int_{-\infty}^t e^{x/\tau} \underline{v_s(x)} dx \\ &= \frac{1}{\tau} \int_{-\infty}^t e^{-t/\tau} e^{x/\tau} v_s(x) dx \\ &= \frac{1}{\tau} \int_{-\infty}^t e^{(x-t)/\tau} v_s(x) dx\end{aligned}$$

input

weighted

"Moving Average" Interpretation

$$= \frac{1}{\tau} \int_{-\infty}^t e^{(x-t)/\tau} v_s(x) dx$$

$$y = \underline{t} - x$$
$$dy = -dx$$

$$= \frac{1}{\tau} \int_{+\infty}^0 e^{-y/\tau} v_s(t-y) (-dy)$$

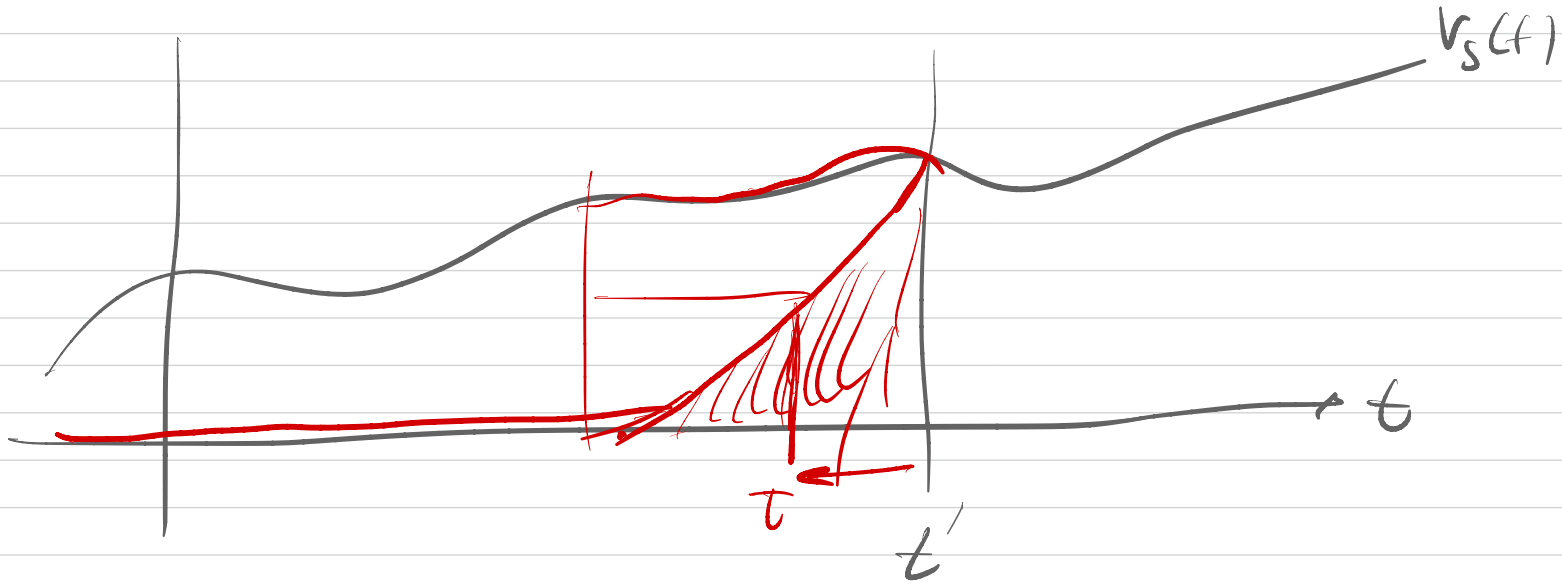
input
past source
 value

$$= \frac{1}{\tau} \int_0^{\infty} e^{-y/\tau} v_s(t-y) dy$$

weight

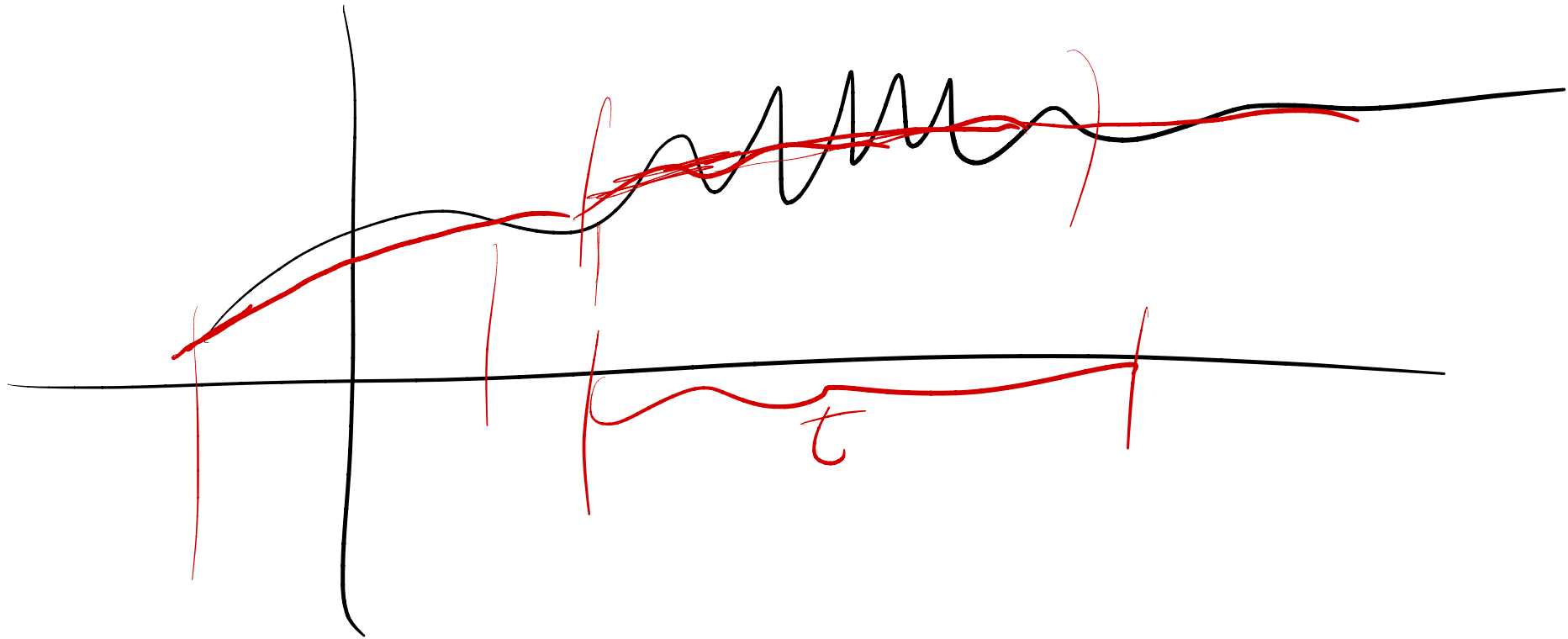
$$= \left(\frac{1}{\tau} \right) \int_0^{\infty} e^{-y/\tau} v_s(t-y) dy$$

The term $v_s(t-y)$ in the integral is highlighted in yellow. An arrow points from the t in the exponent to the t on the horizontal axis of the graph below. Another arrow points from the y in the exponent to the t' on the horizontal axis of the graph below.



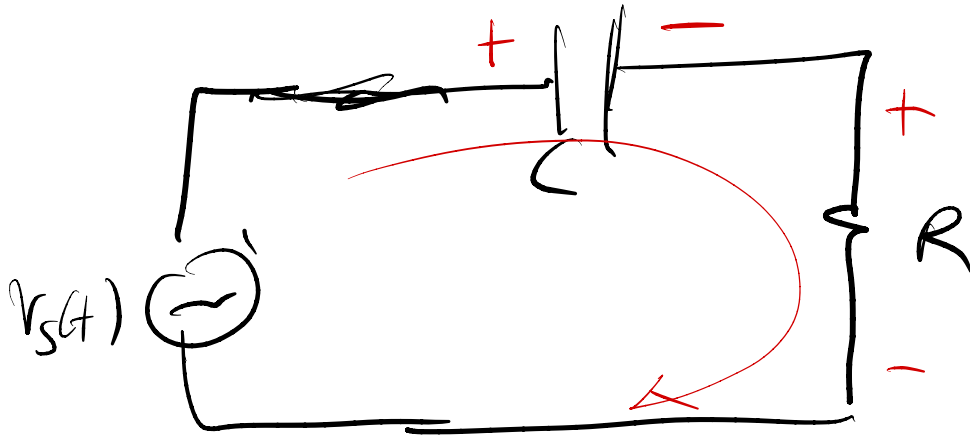
“Slow Pass” Circuit (Low Pass Filter)

- Suppose a function does not change much on the RC time constant scale



“Fast Pass” Circuit (High Pass)

- Now take the output across the resistor. The transfer function can be written as:



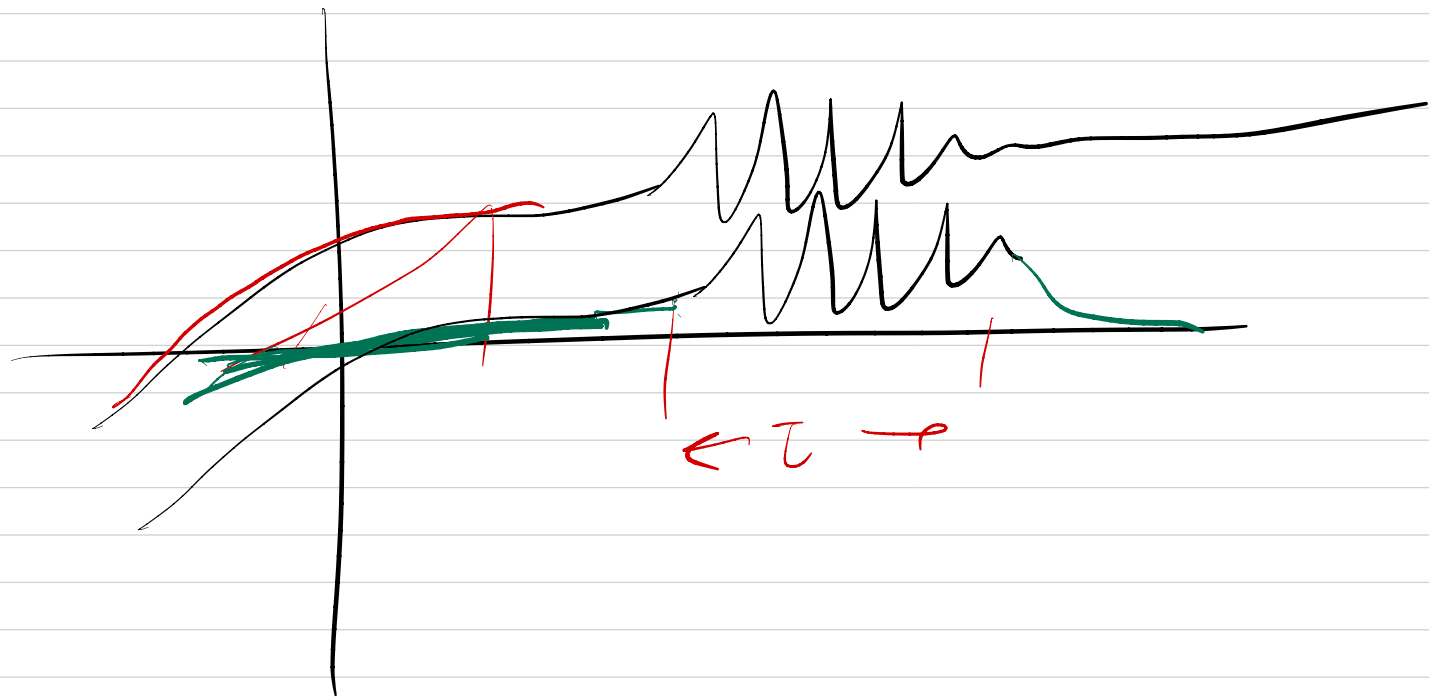
$$v_c(t) = \int_0^{\infty} e^{-y/t} v_s(t-y) dy$$

particular solution

$$v_s = v_c + v_R \quad v_R = v_s - v_c$$

$$v_R = v_s - v_c$$

(weighted average)



Preview: Sinusoidal Steady State

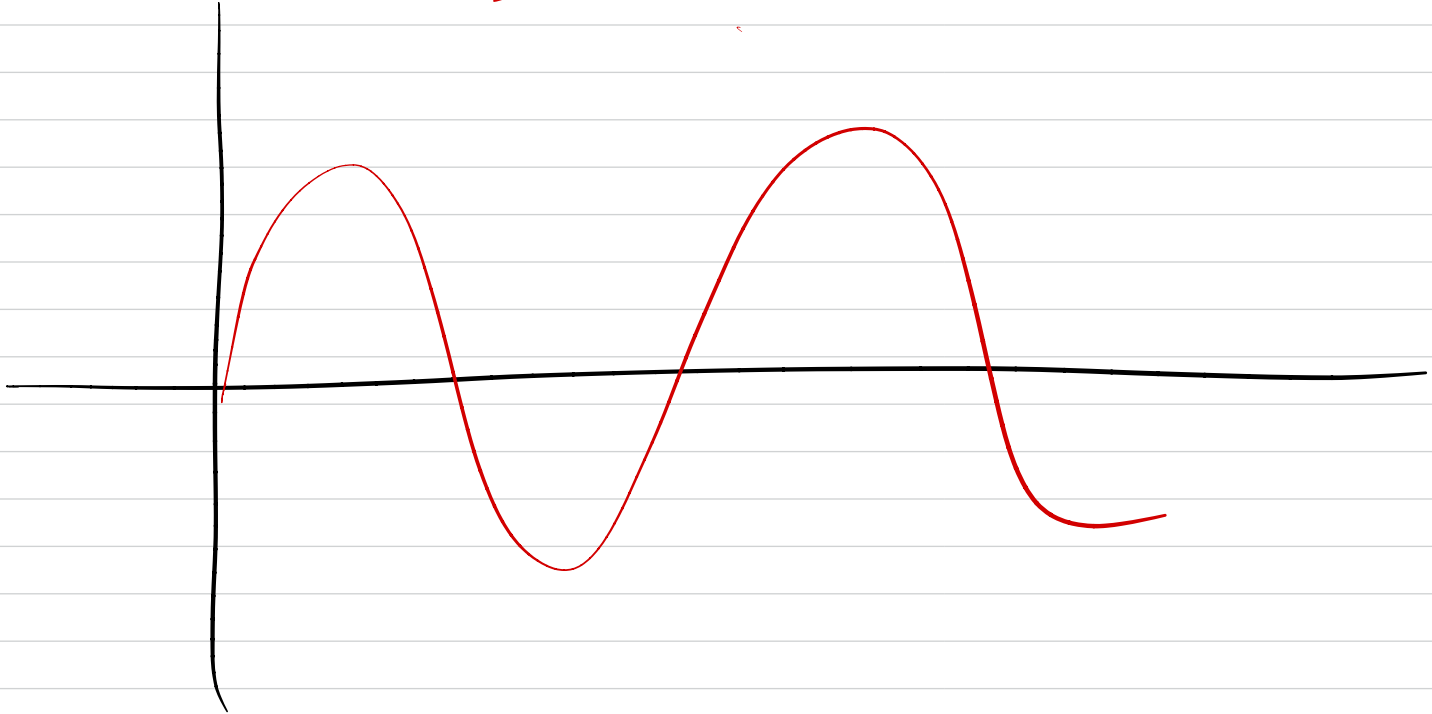
- Suppose we inject a sinusoidal tone. It's much easier to work with complex exponentials and take the real / imag. part later.

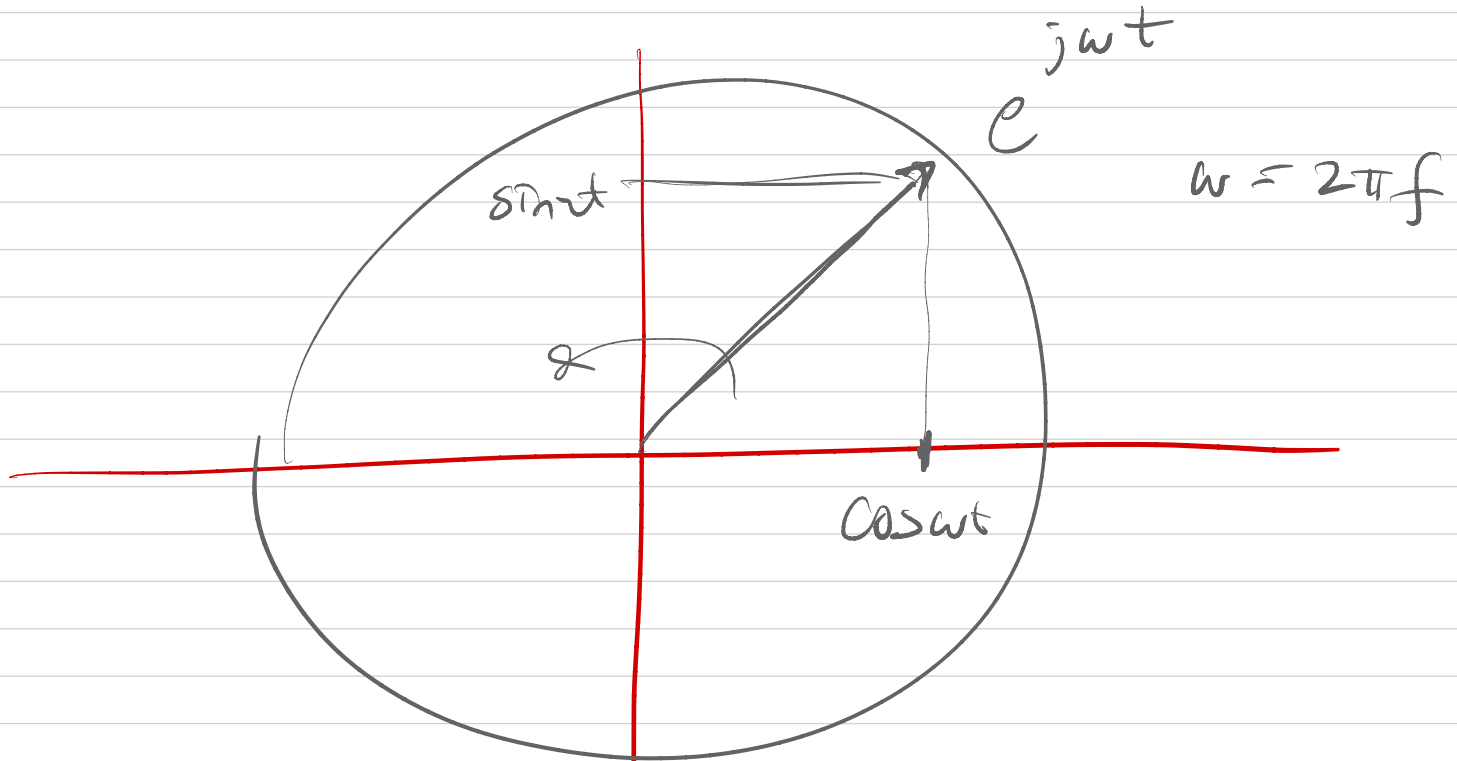
$$V_C(t) = \frac{1}{\tau} \int_0^{\infty} e^{-y/\tau} v_S(t-y) dy$$

$$v_S(t) = e^{j\omega t}$$

$$= \int_0^{\infty} \frac{e^{-y/\tau}}{\tau} \times e^{j\omega(t-y)} dy = \int_0^{\infty} \frac{1}{\tau} e^{j\omega t - j\omega y - y/\tau} dy$$
$$= e^{j\omega t} \int_0^{\infty} \frac{1}{\tau} e^{-(j\omega + \frac{1}{\tau})y} dy$$

$$v_s(t) = A \sin \omega t$$



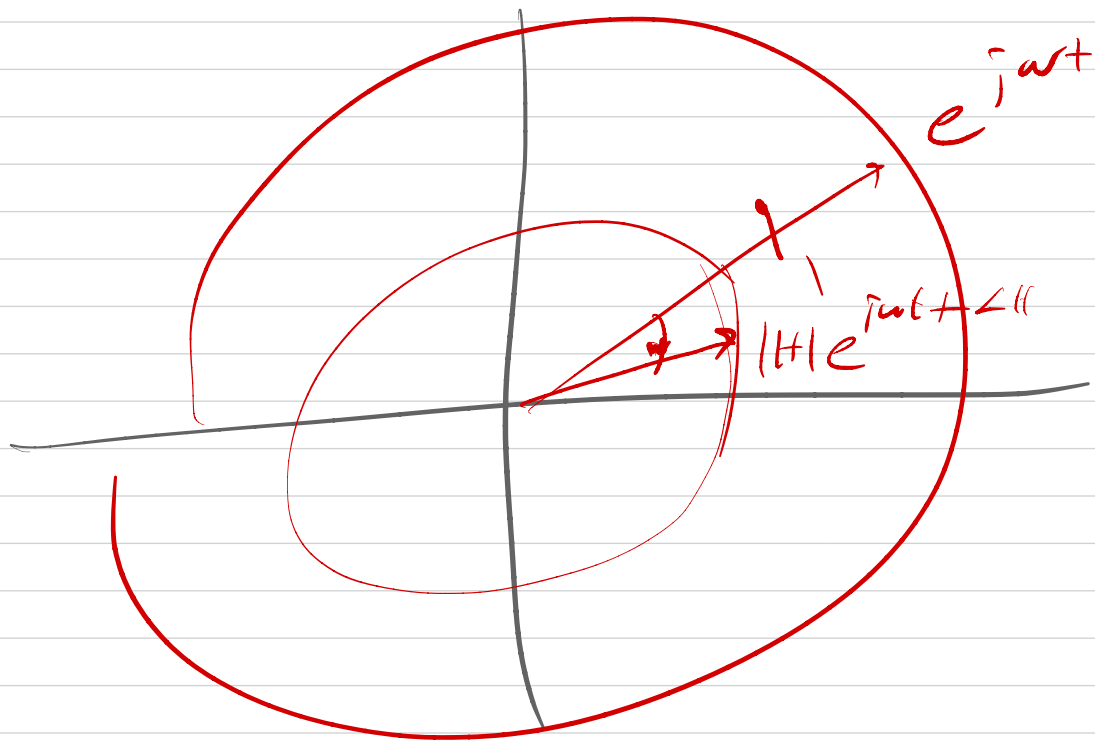


$$e^{j\omega t} = \cos \omega t + j \sin \omega t$$

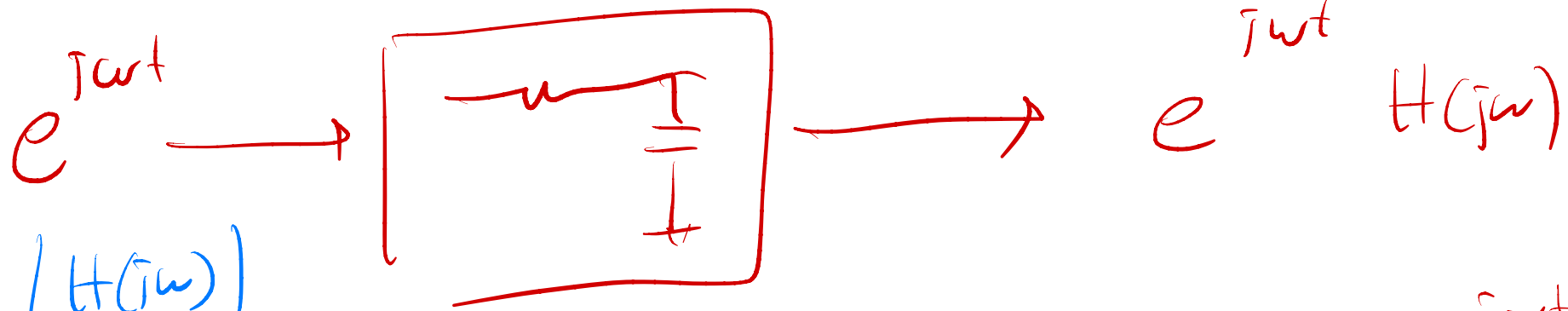
Complex Exponential Solution

$$= e^{j\omega t} \int_0^{\infty} \frac{1}{\tau} e^{-(j\omega + \frac{1}{\tau})y} dy$$

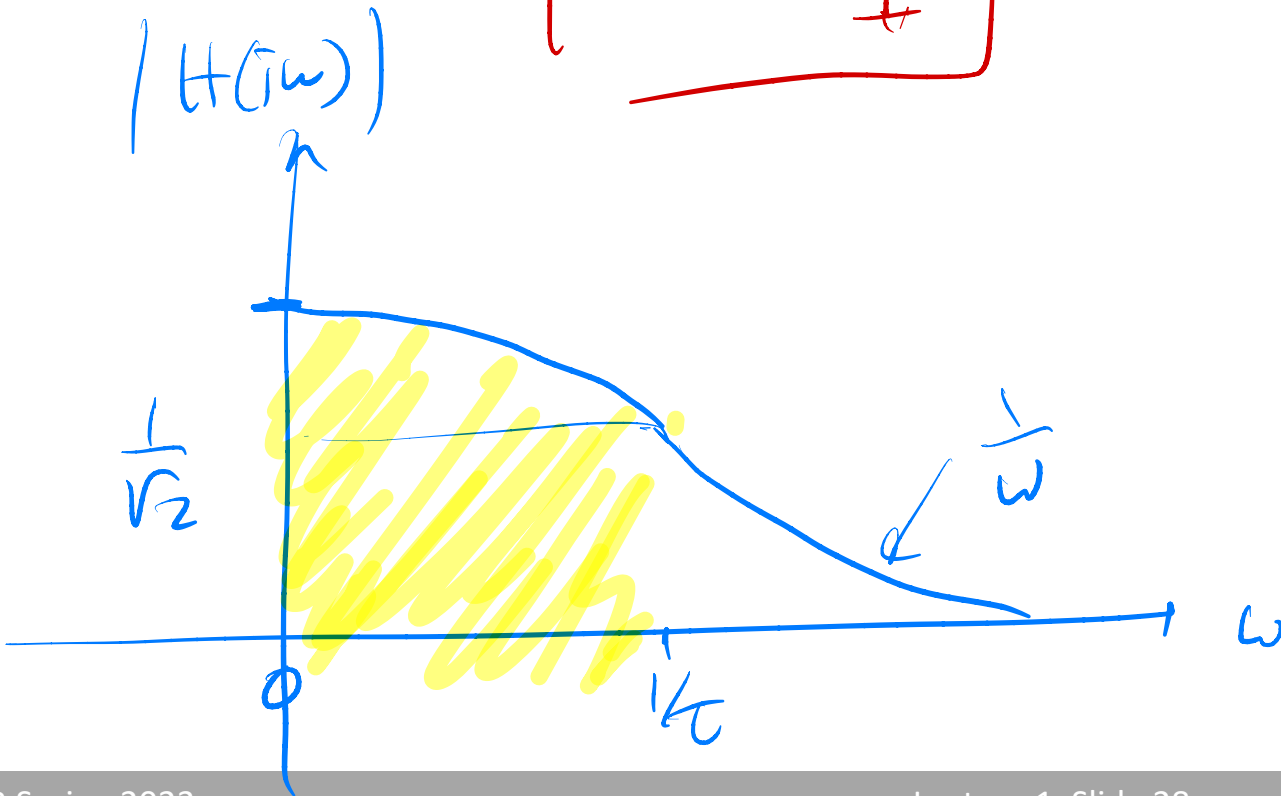
$$= \frac{e^{j\omega t}}{\tau} \left(\frac{-e^{-(j\omega + \frac{1}{\tau})y}}{(j\omega + \frac{1}{\tau})} \right) \Big|_0^{\infty} = \frac{e^{j\omega t}}{\tau} \frac{+1}{j\omega + \frac{1}{\tau}}$$
$$= e^{j\omega t} \underbrace{\left(\frac{+1}{1 + j\omega\tau} \right)}_H$$



Final "Transfer" Function



$$|H(j\omega)| e^{j\omega t + j\Delta\theta}$$



$$H(j\omega) = \frac{1}{1 + j\omega\tau}$$

$$\sim \frac{1}{j\omega\tau}$$

$$e^{j\omega t} = \cos \omega t + j \sin \omega t$$

$$e^{-j\omega t} = \cos \omega t - j \sin \omega t$$

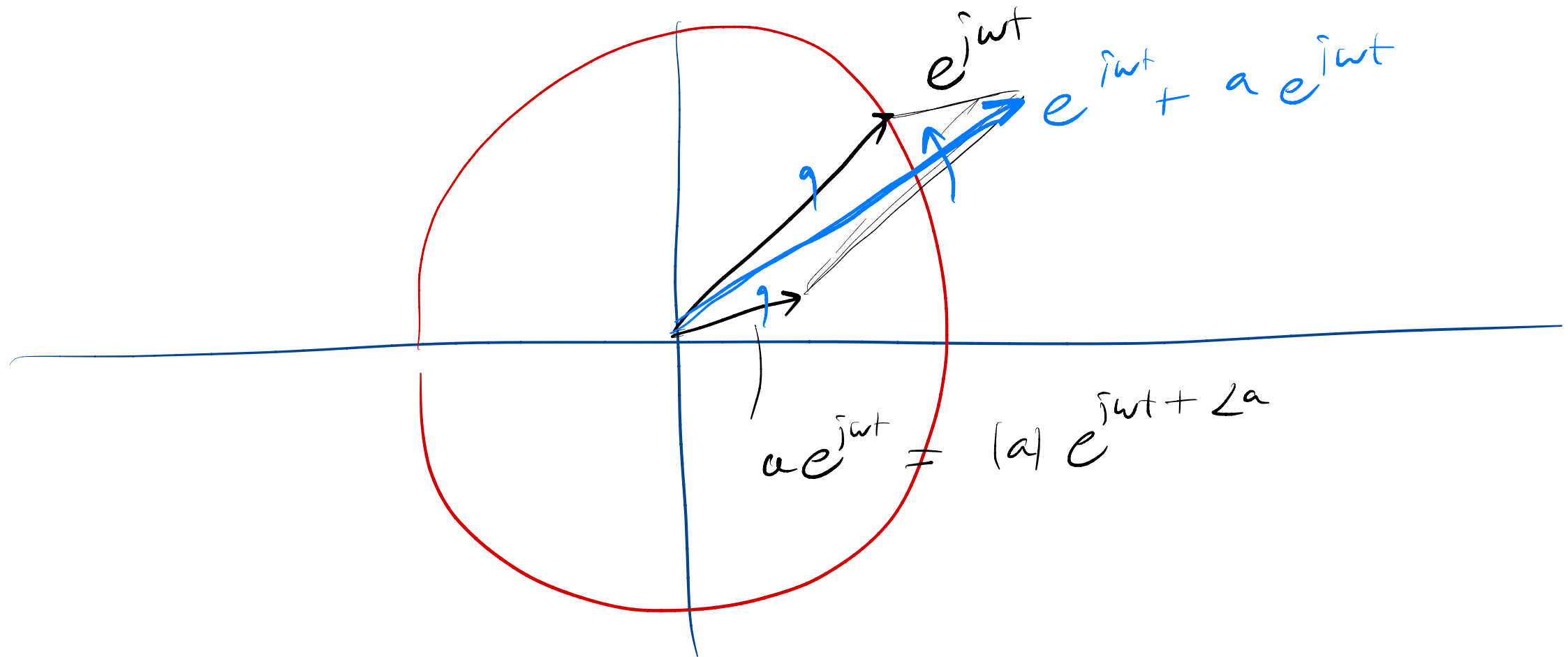
$$e^{j\omega t} + e^{-j\omega t} = 2 \cos \omega t$$

Why It Worked: Going Around a Circle

- Summing many delayed copies of a complex exponential function still results in a complex exponential. Only magnitude and phase changes.

See demos

“Natural” Eigenfunction Solution



Low Pass for Sinusoidal Inputs

Application: Filtering out Noise

- Listen to an audio signal and note that while speech and music has a lot of distinct tones, noise is random, with many high pitched and low-pitched parts.
- What if we use a “low pass” filter to get rid of high-pitched parts?