



The background image shows a detailed microchip layout with various functional blocks highlighted by dashed yellow boxes. The labels include 'RX' (Receiver), 'LO Buffer' (Local Oscillator Buffer), 'Hybrid', 'Wilkinson' (referring to a Wilkinson power divider), 'LO Buffer' (another instance), and 'TX' (Transmitter). The layout features a dense grid of circuit traces and components.

EECS 16B

Designing Information Devices and Systems II

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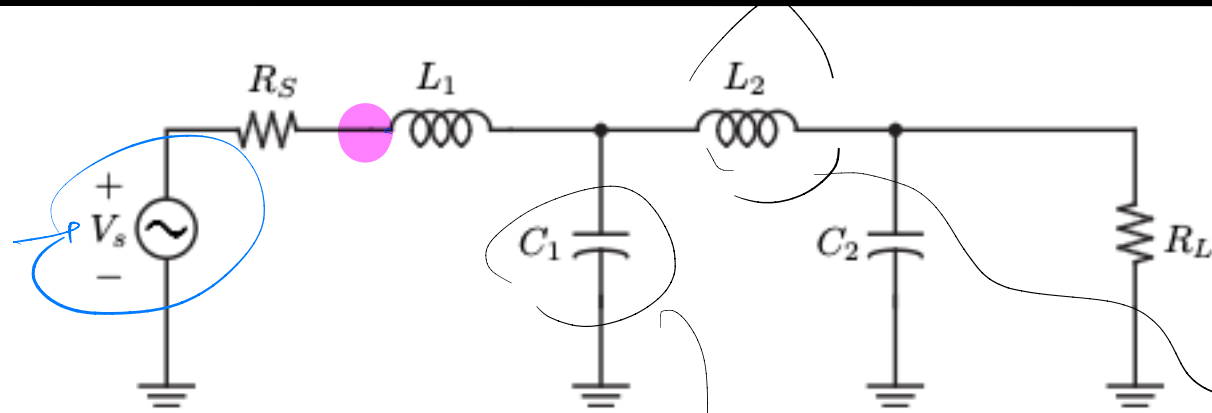
Module 6: Sinusoidal Steady-State Solution to Vector Differential Equations

EECS 16B

Summary

- Solution of VDE in eigenspace with sources
- Steady-state solution of VDE
- Concept of Impedance
- AC Circuits
- Examples

Example Circuit

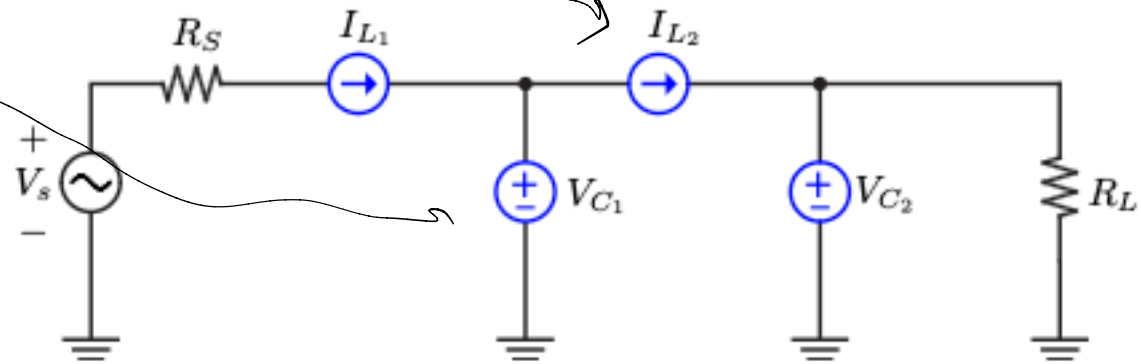


$$\vec{x} = (V_{C_1} \ V_{C_2} \ I_{L_1} \ I_{L_2})^T$$

$$\frac{d}{dt}\vec{x} = A\vec{x} + B\vec{b}_s$$

$$A = \begin{pmatrix} 0 & 0 & 1/C_1 & -1/C_1 \\ 0 & -1/R_L C_2 & 0 & 1/C_2 \\ -1 & 0 & -R_S/L_1 & 0 \\ 1/L_2 & -1/L_2 & 0 & 0 \end{pmatrix}$$

$$B = (0 \ 0 \ 1 \ 0)^T V_s$$



$$\frac{d\vec{x}}{dt} = A\vec{x} + B\vec{b}_s$$

\vec{x} ← State Vector \vec{b}_s ← Ind. Sources

Numerical Example

$$L1 = 7410^{\wedge} - 9; L2 = 114.210^{\wedge} - 9; C1 = 45.61$$

Let's see the eigenvalues for this matrix:

`Eigenvalues[A]//MatrixForm`

$$\lambda_{u+1} = \lambda_u^* \left(\begin{array}{c} \lambda_1 \\ \lambda_2 \\ \lambda_3 \\ \lambda_4 \end{array} \right) = \left(\begin{array}{c} -6.75676 \times 10^8 + 0.i \\ -1.64354 \times 10^8 + 5.88916 \times 10^8 i \\ -1.64354 \times 10^8 - 5.88916 \times 10^8 i \\ -3.47197 \times 10^8 + 0.i \end{array} \right)$$

Real 4 distinct eigenvalues

Complex conjugates

Real

Stability

$$\operatorname{Re}(\lambda_k) < 0$$

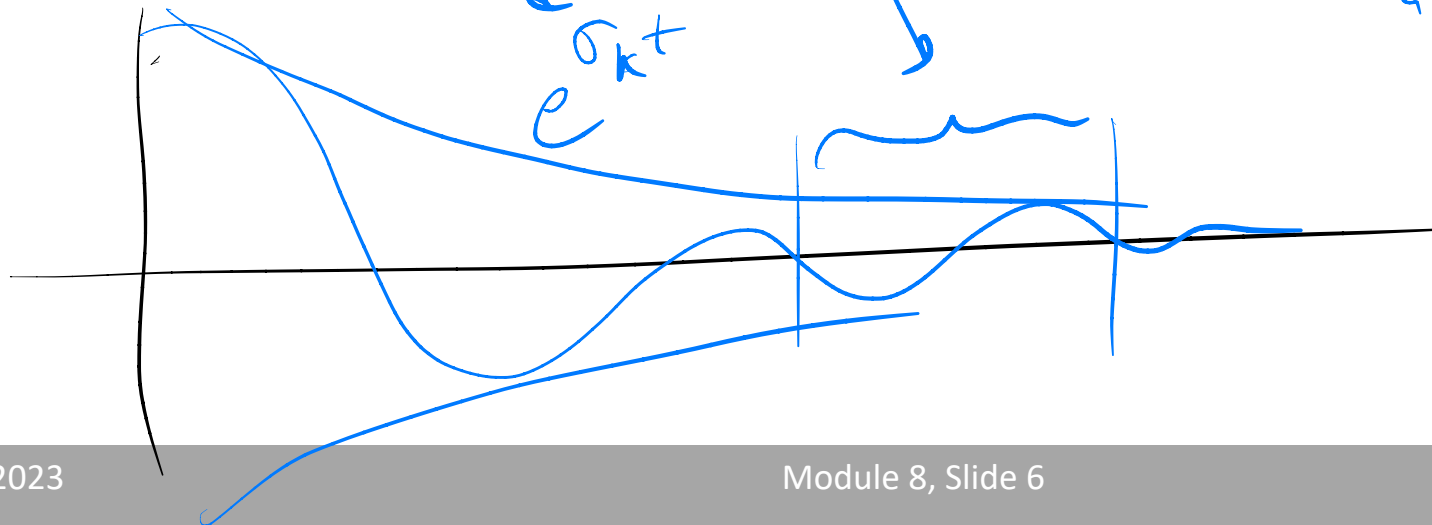
$$q_k(t) = q_{k0} e^{\lambda_k t}$$

λ_k : complex

$$q_k(t) = q_{k0} e^{\sigma_k t} e^{j\omega_k t}$$

$$\lambda_k = \sigma_k + j\omega_k$$

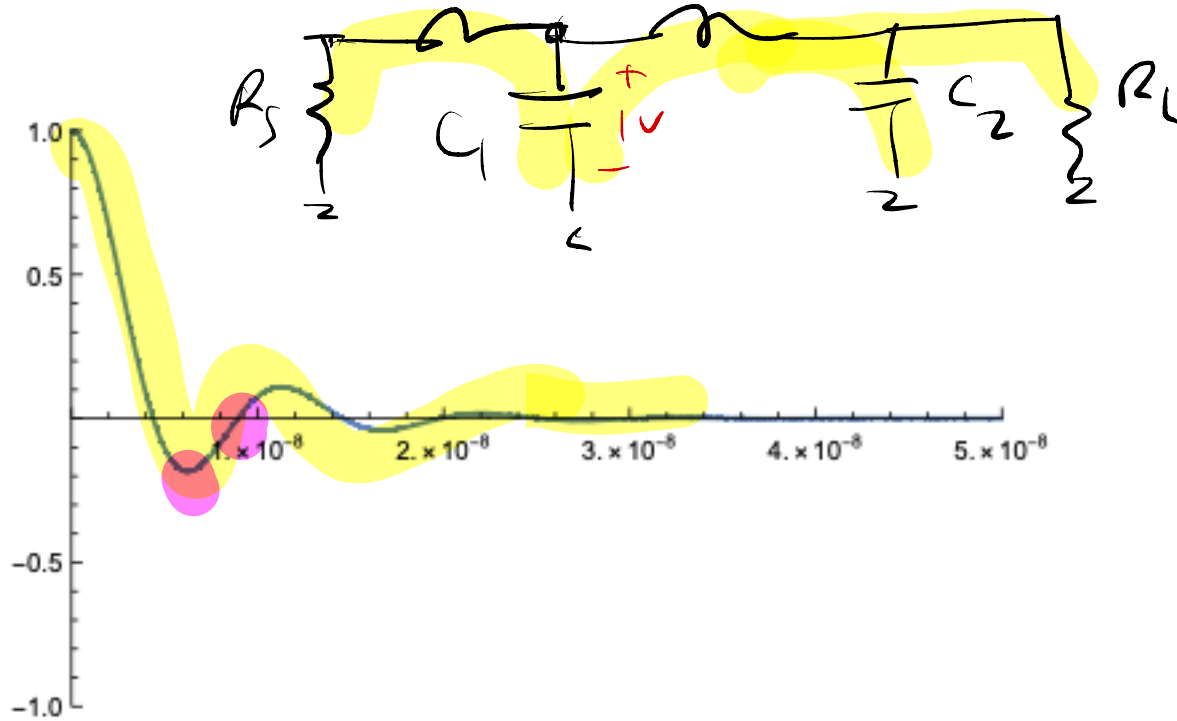
$$= q_{k0} e^{\sigma_k t} (\cos \omega_k t + j \sin \omega_k t)$$



“natural freq”
 ω_k

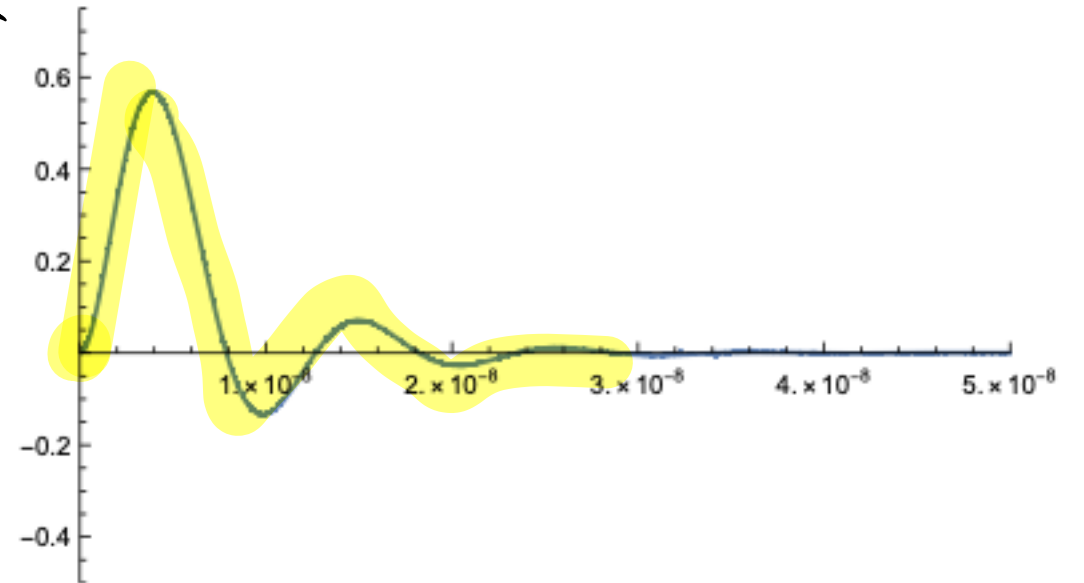
decay rate: σ_k

Homogeneous Solution



State 1

$$X_1 = v_{C_1}$$
$$\vec{X}_0 = (1, 0, 0, 0)^T$$



State 2

$$X_2 = v_{C_2}$$

Forced Response

- Since we've reduced the system to simple constant coefficient linear differential equations, we know the forced response !
- Note that the sources are also transformed into the eigenspace through the matrix Q^{-1}

$$q_k^h(t) = q_k^h(0) e^{\lambda_k t}$$

$$\vec{q}(t) = \vec{q}(0) e^{\Lambda t}$$

Euler
const

Matrix

Notation : $e^{\Lambda} = \begin{bmatrix} e^{\lambda_1} & & & 0 \\ & e^{\lambda_2} & & \\ & & \ddots & \\ 0 & & & e^{\lambda_n} \end{bmatrix}$

Λ : diagonal matrix

$$\vec{x}(t) = Q \vec{q}(t)$$

Eigenvector
matrix

$$\vec{q}(t) = \vec{q}(0) e^{-\Lambda t}$$

$$\vec{x}(t) = Q \vec{q}(t) = \underbrace{Q \vec{q}(0)}_{?} e^{-\Lambda t}$$

$$\vec{q}(0) = Q^{-1} \vec{x}(0)$$

↑
initial
state

↑
transformation
matrix

Steady-State DC Response

$$\cancel{\frac{d\vec{x}}{dt}} = A\vec{x} + \vec{b}_s$$

$$\lim_{t \rightarrow \infty} e^{At} = \vec{0}$$

$$0 = A\vec{x} + \vec{b}_s$$

All eigenvalues have negative real part

$$\begin{aligned}\vec{x} &= -A^{-1}\vec{b}_s \\ &= -A^{-1}B\vec{b}_s\end{aligned}$$

Review: General Solution to 1st-order ODE

- With constant coefficients, we derived

$$\frac{d\vec{x}}{dt} = \underbrace{A}_{\text{matrix}} \vec{x} + B \vec{b}_s \leftarrow \text{vector of sources}$$

$$\begin{aligned} \frac{d\vec{x}}{dt} &= \underbrace{A}_{\text{matrix}} \vec{x} + B \vec{b}_s \\ \frac{d\vec{x}}{dt} &= Q \Lambda Q^{-1} \vec{x} + B \vec{b}_s \\ \frac{d(Q^{-1}\vec{x})}{dt} &= \Lambda Q^{-1} \vec{x} + \underbrace{Q^{-1} B \vec{b}_s}_{\vec{b}_s} \\ \frac{d\vec{q}}{dt} &= \Lambda \vec{q} + \vec{b}_s \end{aligned}$$

Apply Solution to VDE

$$\frac{dq_k}{dt} = \lambda_k q_k + \tilde{b}_{sk}$$

$$e^{-\lambda_k t} \left(\frac{dq_k}{dt} - \lambda_k q_k \right) = \tilde{b}_{sk} e^{-\lambda_k t}$$

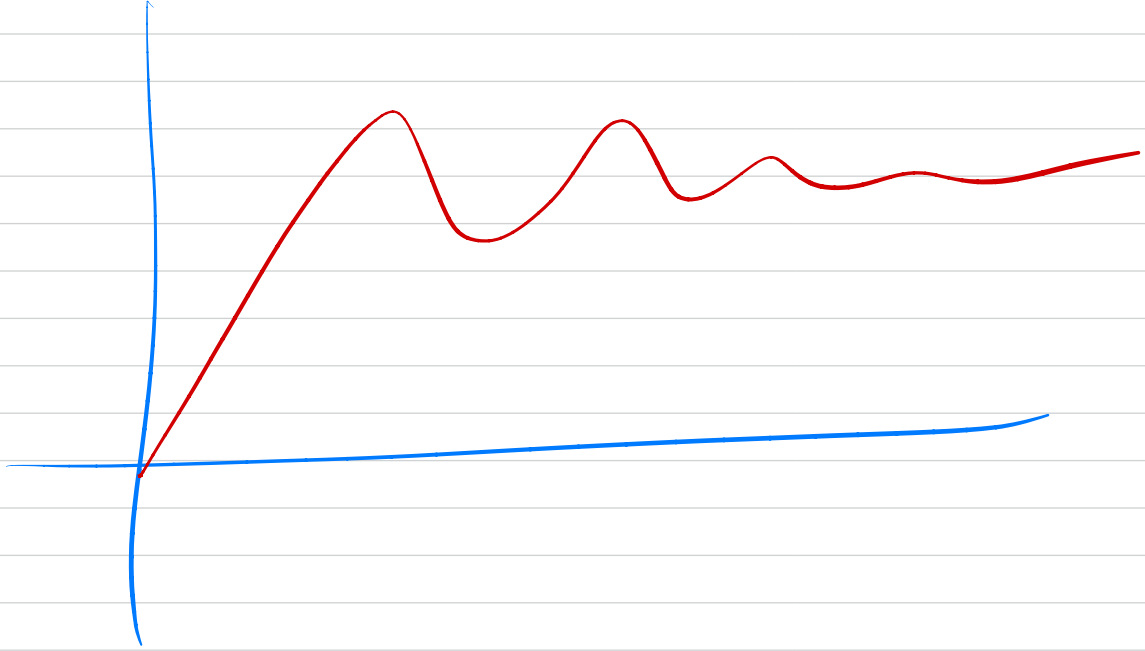
$$\left(e^{-\lambda_k t} \frac{dq_k}{dt} - \lambda_k e^{-\lambda_k t} q_k \right)$$

$$\int \left(q_k(t) e^{-\lambda_k t} \right)' ds = \int_{-\infty}^t \tilde{b}_{sk} e^{-\lambda_k s} ds + K_k$$

$$\int \left(q_k(t) e^{-\lambda_k t} \right)' ds = \int_{-\infty}^t \tilde{b}_{sk} e^{-\lambda_k s} ds + K_k$$

$$q_k(t) = \underbrace{e^{\lambda_k t} \int_{-\infty}^t \tilde{b}_{sk}(s) e^{-\lambda_k s} ds}_{\text{forced solution for zero initial condition}} + \underbrace{e^{\lambda_k t} q_k(0)}_{\text{solution to zero input}}$$

$$\vec{q}(t) = e^{-\Lambda t} \vec{q}(0) + e^{\Lambda t} \int_{-\infty}^t Q^{-1} \vec{b}_s e^{-\Lambda s} ds$$



$$\vec{q}(t) = e^{-\Lambda t} \vec{q}(0) + e^{-\Lambda t} \int_0^t Q^{-1} \vec{b}_s e^{-\Lambda s} ds$$

$$\vec{x}(t) = Q \vec{q}(t) = Q e^{-\Lambda t} Q^{-1} \vec{x}(0) +$$

$$Q e^{-\Lambda t} \int_0^t Q^{-1} \vec{b}_s e^{-\Lambda s} ds$$

$$Q e^{-\Lambda t} Q^{-1} \int_0^t \vec{b}_s e^{-\Lambda s} ds$$

$$\vec{x}(t) = \underbrace{Q e^{At} Q^{-1}}_{e^{At}} \vec{x}(0) + \underbrace{Q e^{At} Q^{-1}}_{e^{At}} \int_0^t \vec{b}_s e^{-As} ds$$

$$\frac{dx}{dt} = ax + b$$

$$\vec{x}(t) = e^{At} \vec{x}(0) + e^{At} \int_0^t \vec{b}_s e^{-As} ds$$

Elegant Notation

- Let's define the matrix exponential
- While for now you can accept this as merely a convenient notation, it turns out to be a more general idea !
(<https://youtu.be/O85OWBJ2ayo>)

$$e^{At} \triangleq \underbrace{Q e^{\Lambda t} Q^{-1}}$$

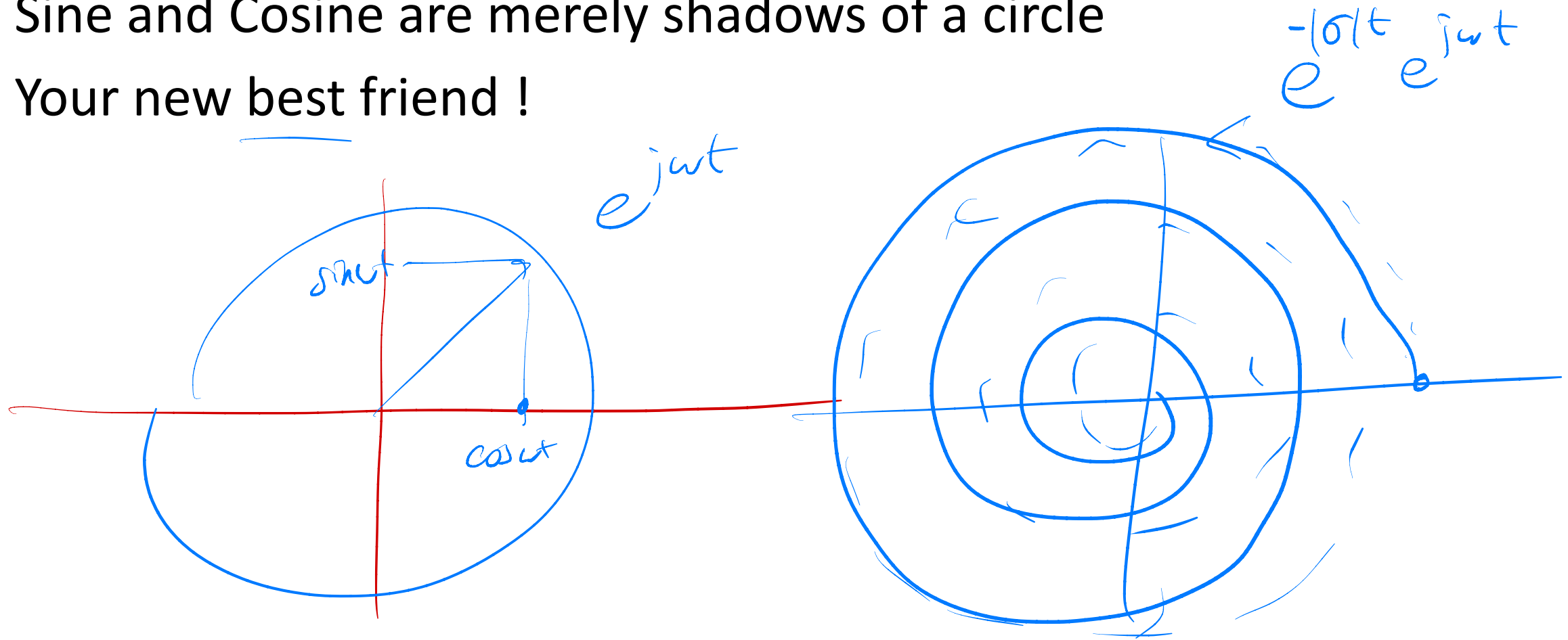
$$e^x = 1 + \frac{x}{1!} + \frac{x^2}{2!} + \dots$$

Forced Response in Steady-State

- Assume source is sinusoidal (very common in practice)
 - RF signals essentially sinusoidal on short time scales
 - Musical notes are superpositions of tones (frequencies)
 - Any general waveform can be decomposed into sinusoids ! (Fourier Series and Transform ... EE120)

Complex Exponential (again)

- Sine and Cosine are merely shadows of a circle
- Your new best friend !



Steady-State Continued

$$q_a(t) = e^{\lambda_a t} q_h(0) + e^{\lambda_a t} \int_{-\infty}^t e^{-\lambda_a s} \hat{b}_{sa}(s) ds$$

steady state

$\lim_{t \rightarrow \infty}$

$$q_a^f(t) = e^{\lambda_a t} \int_{-\infty}^t e^{-\lambda_a s} Q^{-1} \hat{b}_s e^{j\omega s} ds$$

$$\begin{aligned} \hat{b}_{sa} &= Q^{-1} b_s \\ &= Q^{-1} \hat{b}_s e^{j\omega t} \end{aligned}$$

$$= e^{\lambda_a t} Q^{-1} \hat{b}_s \int_{-\infty}^t e^{(j\omega - \lambda_a)s} ds$$

$$= e^{\lambda_a t} Q^{-1} \hat{b}_s \left\{ \frac{e^{(j\omega - \lambda_a)s}}{j\omega - \lambda_a} \right\}_{-\infty}^t = \frac{e^{(j\omega - \lambda_a)t}}{j\omega - \lambda_a} - \left. \frac{e^{j\omega t + \lambda_a t}}{j\omega - \lambda_a} \right|_{t \rightarrow -\infty}$$

by stability
 $\Re(\lambda_a) < 0$

$$\tilde{b}_{sk} = b_1 e^{j(\omega t + \phi_1)} + b_2 e^{j(\omega t + \phi_2)} + b_3 e^{j(\omega t + \phi_3)}$$

$$= b_1 e^{j\omega t} e^{j\phi_1} + b_2 e^{j\omega t} e^{j\phi_2} + b_3 e^{j\omega t} e^{j\phi_3}$$

$$= e^{j\omega t} (b_1 e^{j\phi_1} + b_2 e^{j\phi_2} + \dots)$$

$$(b_1 \cos \phi_1 + b_1 j \sin \phi_1 + b_2 \cos \phi_2 + j b_2 \sin \phi_2 + \dots)$$

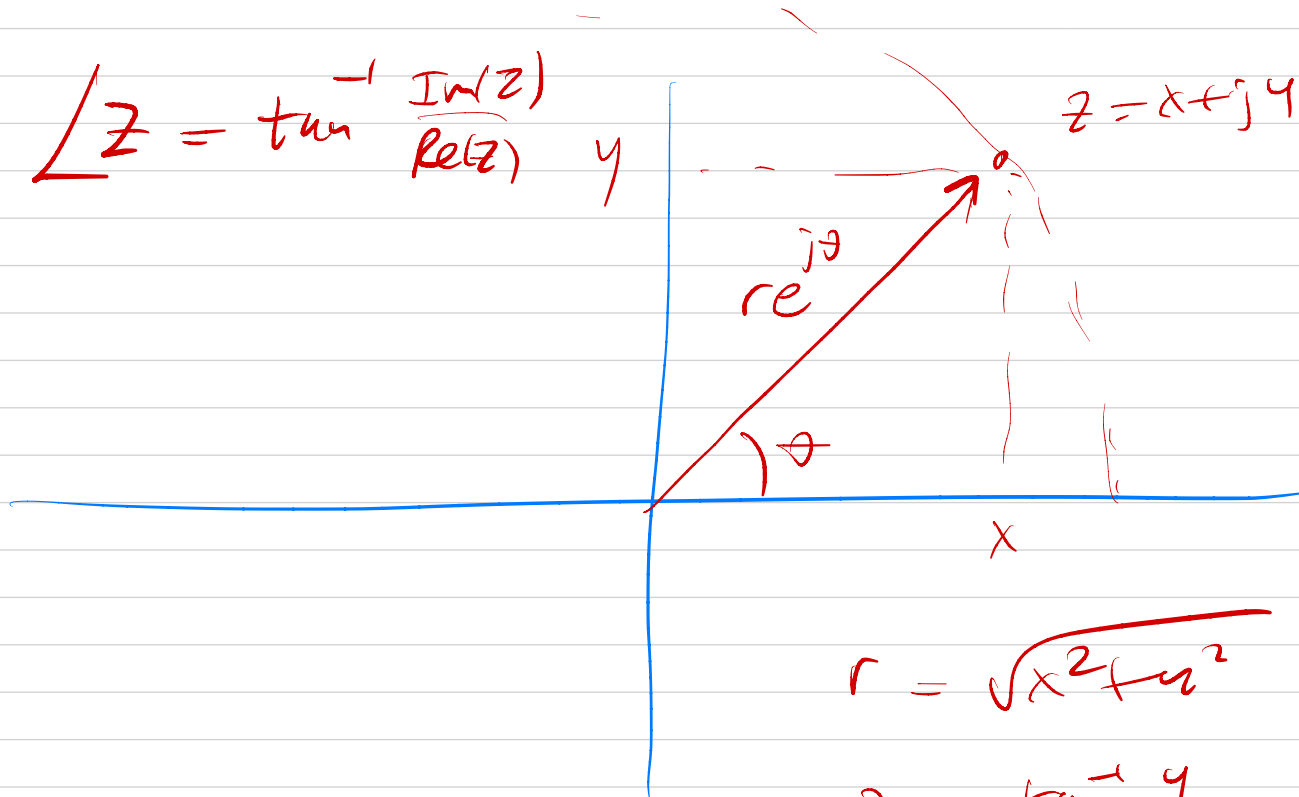
$$= x + jy = r e^{j\theta}$$

$$= \hat{b}_{sk} e^{j\omega t}$$

$$\hat{b}_{sk} = |b_{sk}| e^{j\angle b_{sk}}$$

rotating around
circle

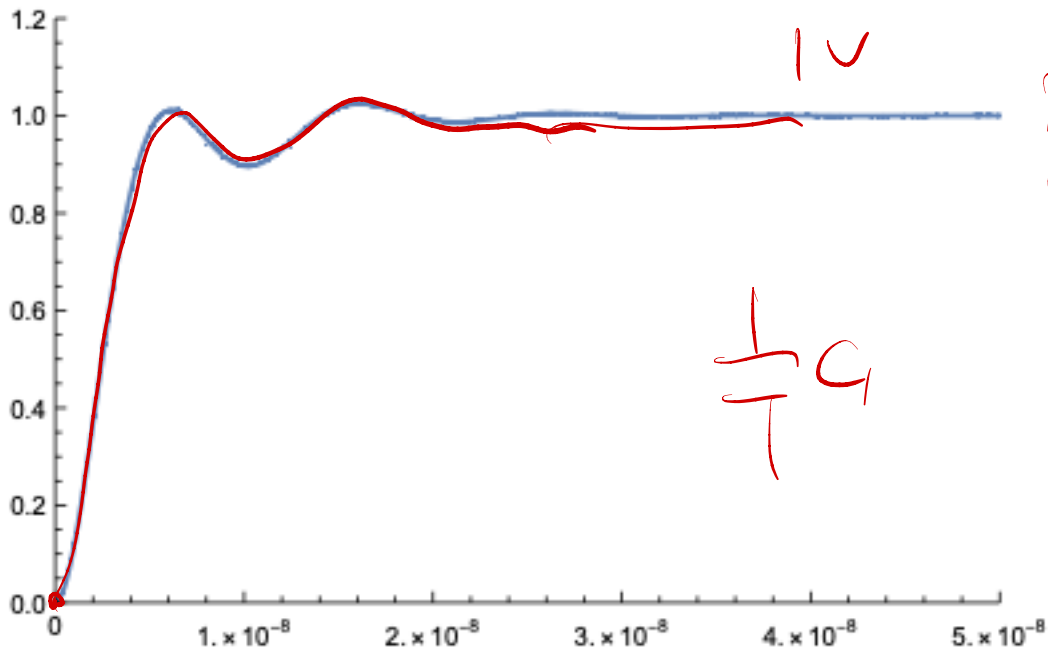
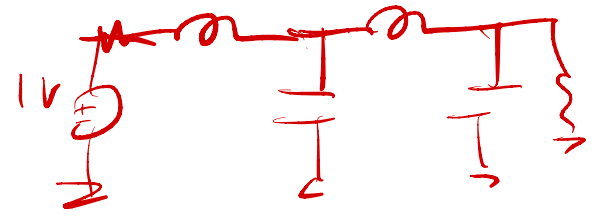
$$\angle z = \tan^{-1} \frac{\text{Im}(z)}{\text{Re}(z)}$$



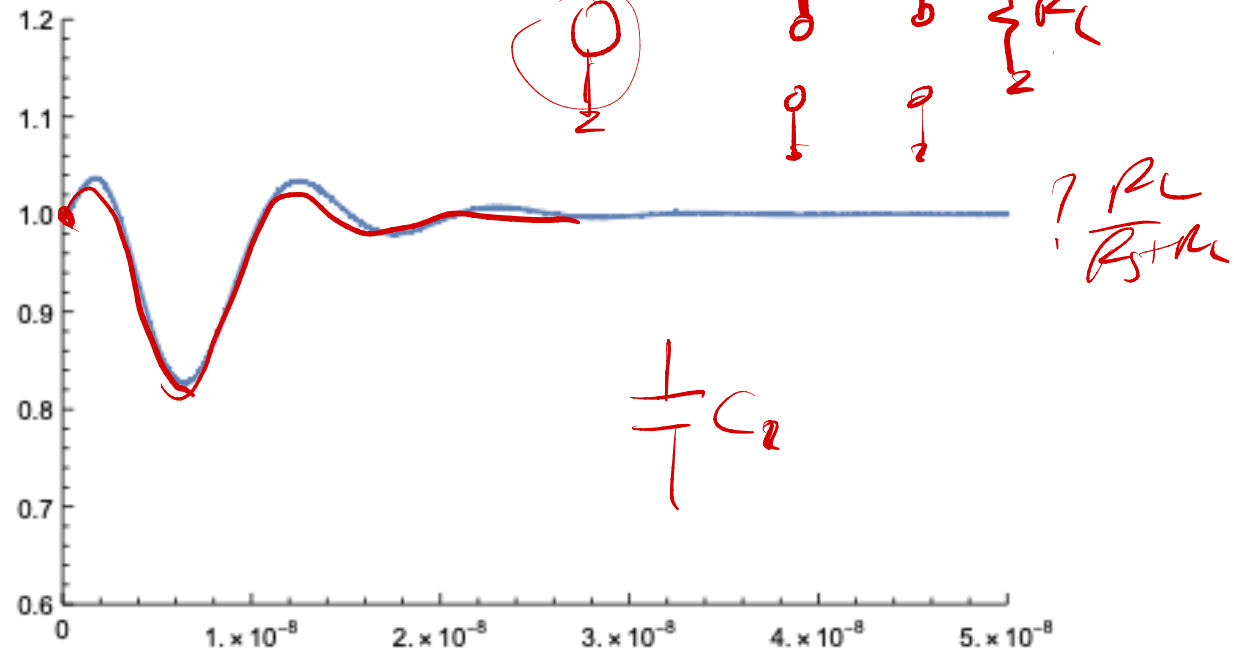
$$r = \sqrt{x^2 + y^2}$$

$$\theta = \tan^{-1} \frac{y}{x}$$

Example: Forced Solution



State 1



State 2

$$\vec{x}(0) = (0, 1, 0, 0)^T$$

Steady-State

$$g_k(t) = \frac{\hat{b}_k}{j\omega - d_k} e^{j\omega t} = g_k e^{j\omega t}$$

some complex #

$$\vec{x} = Q \vec{g} \neq$$

$$x_k(t) = \left(\sum_k \hat{h}_k \right) e^{j\omega t}$$

$$x_k(t) = H_k e^{j\omega t}$$