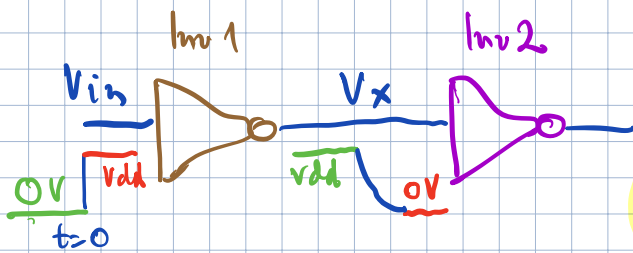


# Lecture 3

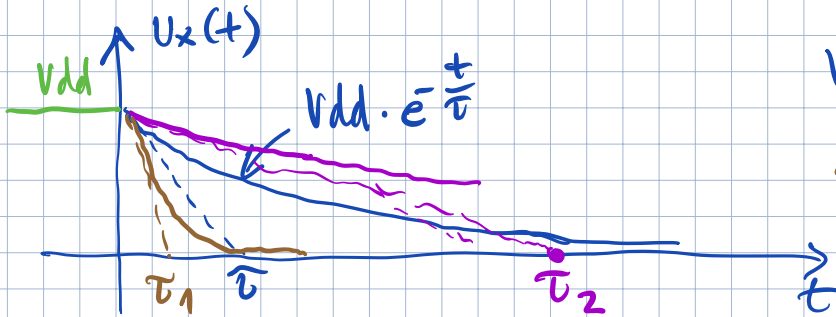
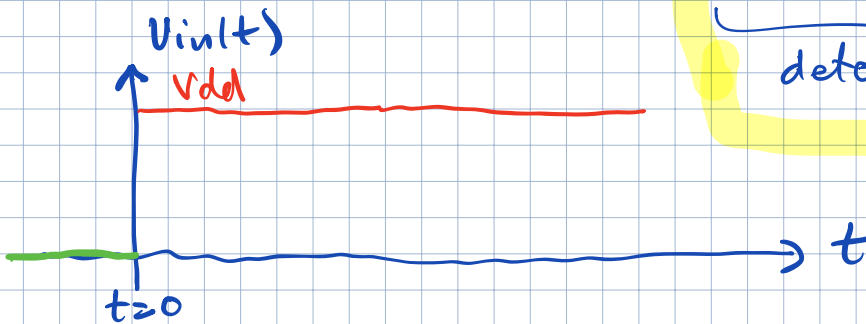
- \* Computing: Transistors & Logic
- \* RC transients finish
- \* Non-homogeneous diff. eqns.
  - \* constant input
  - \* piece-wise constant input
  - \* continuous input
- \* Sensing



$$V_x(t) = V_{dd} e^{-\frac{t}{\tau}}, t \geq 0$$

$$\tau = R_{on, n1} \cdot (C_{Gn2} + C_{Gp2})$$

determines the speed of transition

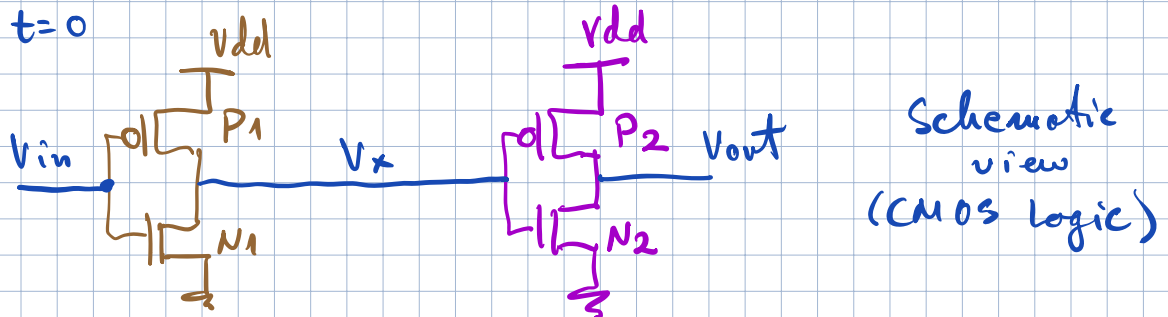
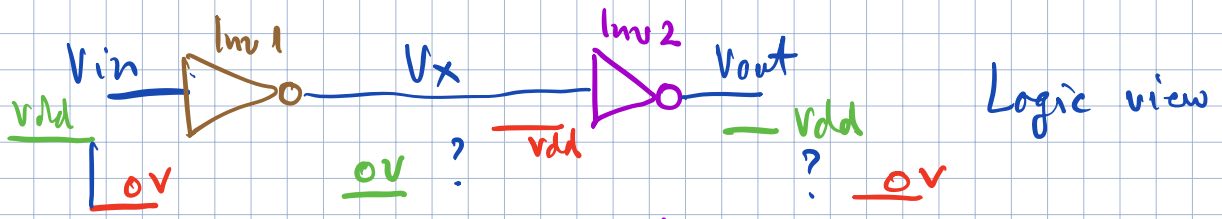


What happens for

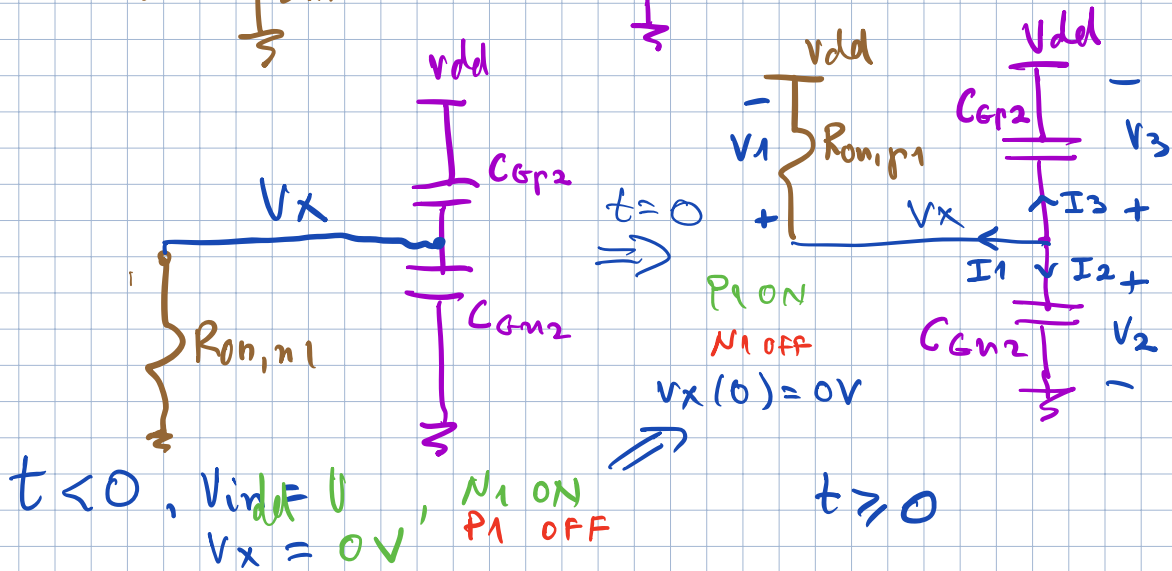
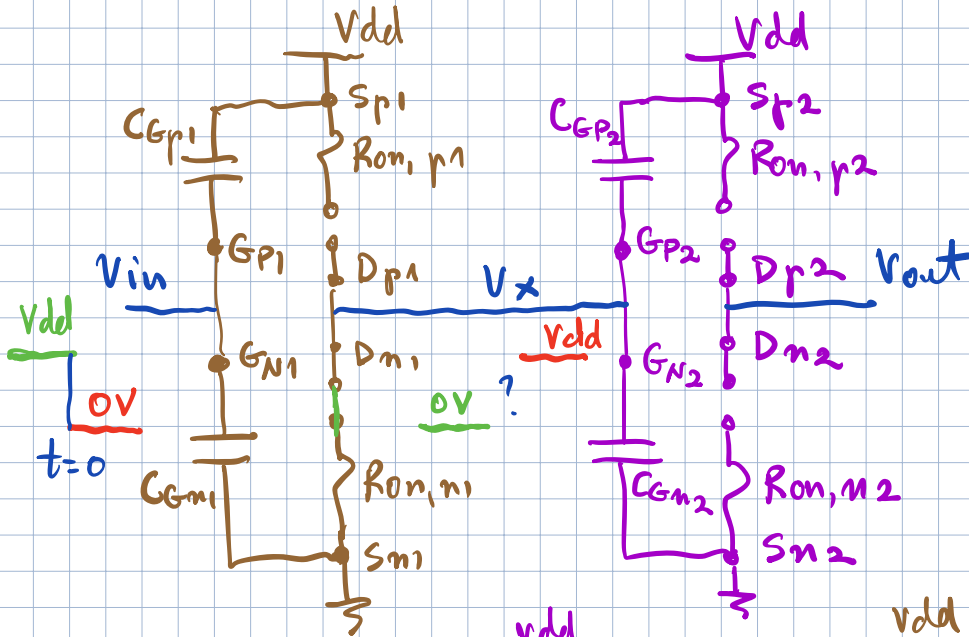
$$\tau_1 < \tau < \tau_2$$

If you make transistors smaller  $\Rightarrow \tau \downarrow$

Demand scaling  $\Rightarrow$  Moore's law  
(economies law)



⇓ RC models



$$\text{KCL: } I_1 + I_2 + I_3 = 0$$

$$\text{Elements: } V_1 = I_1 \cdot R_{on,p1}$$

$$I_2 = C_{Gn2} \cdot \frac{dV_2}{dt}$$

$$I_3 = C_{Gp2} \cdot \frac{dV_3}{dt}$$

Voltages:

$$V_1 = V_x - V_{dd}$$

$$V_2 = V_x$$

$$V_3 = V_x - V_{dd}$$

From KCL & Elements:

$$\underbrace{\frac{V_1}{R_{on,p1}}}_{I_1} + \underbrace{C_{Gn2} \frac{dV_2}{dt}}_{I_2} + \underbrace{C_{Gp2} \frac{dV_3}{dt}}_{I_3} = 0$$

From voltages:

$$\frac{V_x - V_{dd}}{R_{on,p1}} + C_{Gn2} \frac{dV_x}{dt} + C_{Gp2} \frac{d}{dt}(V_x - V_{dd}) = 0$$

$$\left[ \frac{d}{dt} V_{dd} = 0 \right]$$

$$\frac{V_x - V_{dd}}{R_{on,p1}} + C_{Gn2} \frac{dV_x}{dt} + C_{Gp2} \frac{dV_x}{dt} = 0$$

$$(1) \quad \frac{V_x - V_{dd}}{R_{on,p1}} + (C_{Gn2} + C_{Gp2}) \frac{dV_x}{dt} = 0$$

$$\frac{dV_x}{dt} = \underbrace{-\frac{V_x}{R_{on,p1} (C_{Gn2} + C_{Gp2})}}_{\text{homogeneous term}} + \underbrace{\frac{V_{dd}}{R_{on,p1} (C_{Gn2} + C_{Gp2})}}_{\text{non-homogeneous term}}$$

Form:  $\frac{d}{dt} x(t) = \lambda x(t)$  (homogeneous)

$$\frac{d}{dt} x(t) = \lambda x(t) + a$$

(non-homogeneous)

Go back to (1)

$$\frac{V_x - V_{dd}}{R_{on,1n}} + (C_{m2} + C_{p2}) \cdot \frac{d}{dt} (V_x - V_{dd}) = 0$$

Try change of variables to transform the problem into one we know how to solve.

$$\tilde{V}_x = V_x - V_{dd}$$

$$\frac{\tilde{V}_x}{R_{on,1n}} + (C_{m2} + C_{p2}) \frac{d}{dt} \tilde{V}_x = 0$$

$$\frac{d}{dt} \tilde{V}_x = - \frac{\tilde{V}_x}{R_{on,1n} \cdot (C_{m2} + C_{p2})}$$

We already know how to solve this! ☺

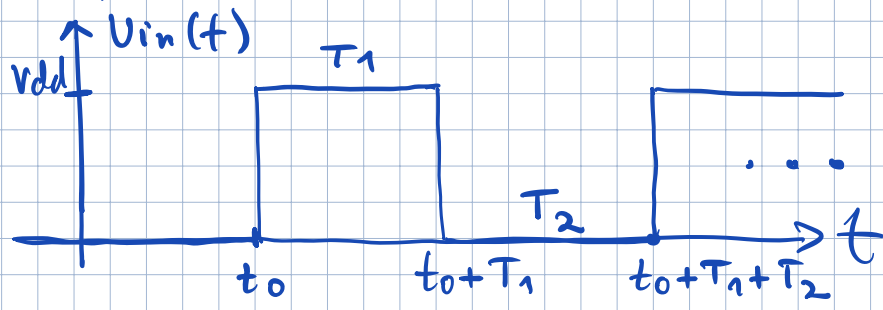
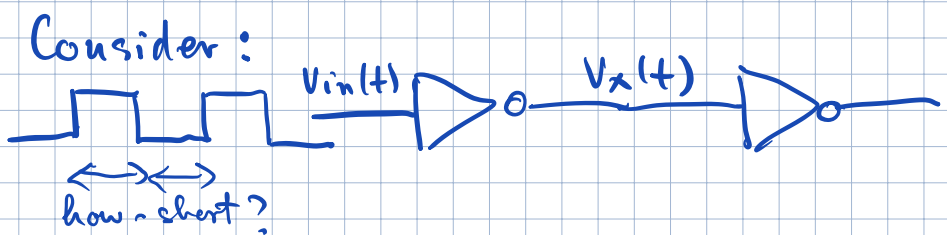
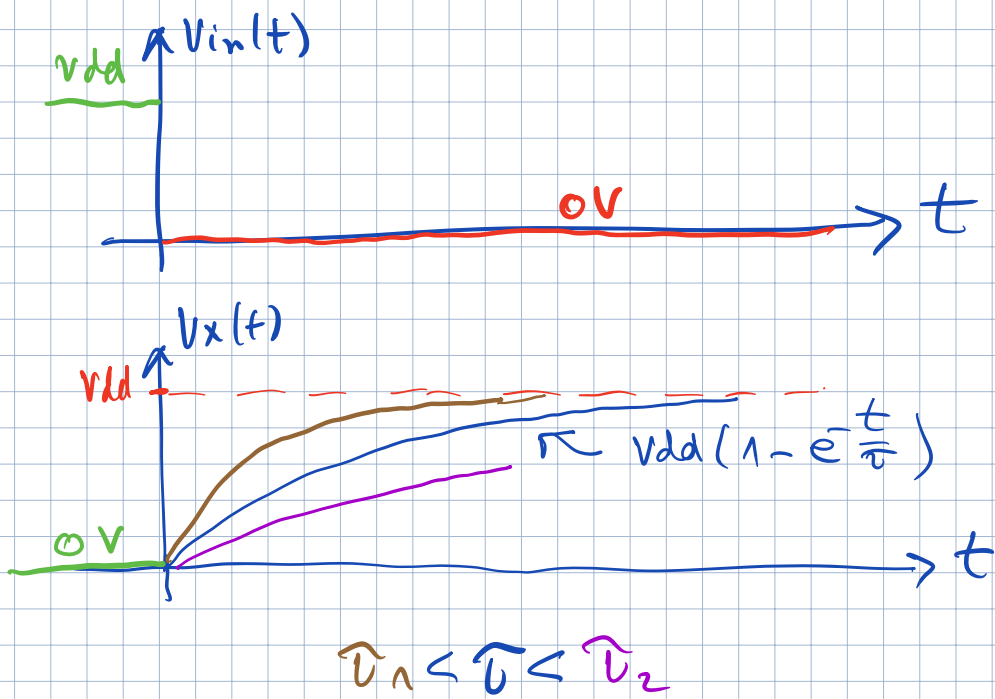
$$\tau = R_{on,1n} (C_{m2} + C_{p2})$$

homogeneous diff. eqn.

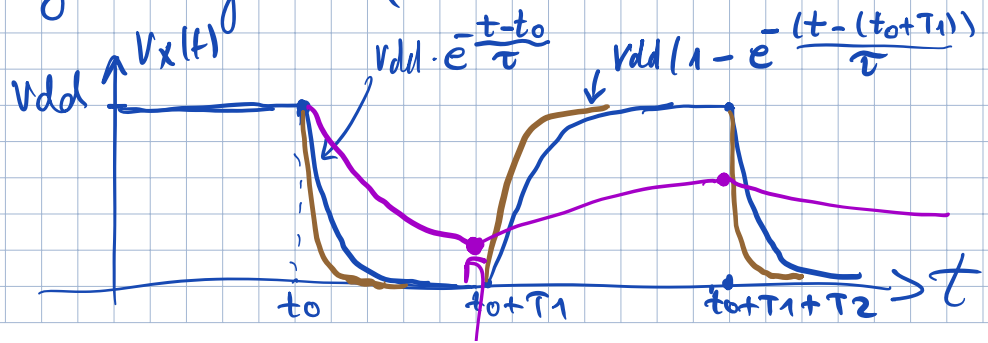
$$\tilde{V}_x(t) = \tilde{V}_x(0) \cdot e^{-\frac{t}{\tau}}, t \geq 0$$

$$V_x(t) - V_{dd} = (V_x(0) - V_{dd}) \cdot e^{-\frac{t}{\tau}} \quad V_x(0) = 0V$$

$$V_x(t) = V_{dd} (1 - e^{-\frac{t}{\tau}}), t \geq 0$$



Will  $V_x(t)$  be able to follow these changes as a "logic" signal (i.e. to reach  $0V$  or  $V_{dd}$ )?



$$\tau_1 < \tau < \tau_2$$

init. condition is no longer  
it is actually  $V_x(t_0 + T_1) =$  or.  
 $= V_{dd} \cdot e^{-\frac{t_0 + T_1 - t_0}{\tau_2}} =$   
 $= V_{dd} \cdot e^{-\frac{T_1}{\tau_2}}$

Use previous  $V_x(t)$  solution as an initial condition for the next interval.

Solutions for piece-wise constant input:

Form:  $\frac{d}{dt} x(t) = \lambda x(t) - \lambda u(t) \leftarrow \text{constant}$   
 or piece-wise constant

What we also want to solve is  $u(t) = u_c(t)$

$u_c(t)$



↑  
continuous time.

$$u(t) \neq u_c(t)$$

$$u(t) \xrightarrow{\Delta \rightarrow 0} u_c(t)$$

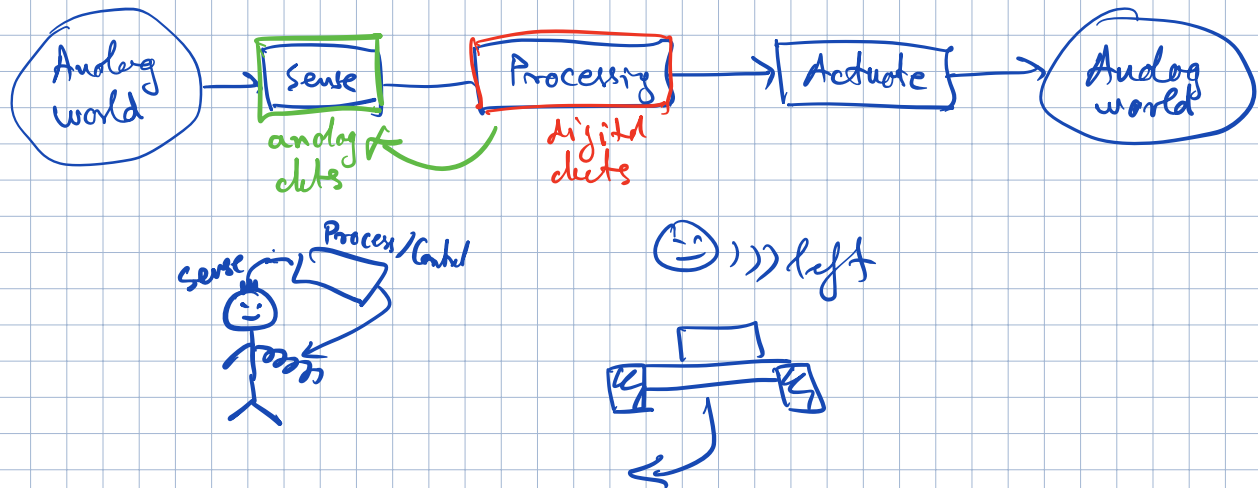
$$u(t) = \text{const}, t \in [t_0, t_0 + \Delta)$$

iterate & use the previous solution as initial condition

then let  $\Delta \rightarrow 0$  for  $u(t)$  to approach  $u_c(t)$   
in the limit (disc. + hw)

Why do we want to know the response to continuous time input?

## EECS 16AB Pipeline



Sensing: hear signals or voice signals

Signal of interest + ~~interference~~

(AC power, wifi/cellular, others talking in the lab, ...)

Design sensor ckt to pick this up

unwanted ☹️

The goal:

Filter/select signals of interest and reject interference.

How can a circuit become a filter - process the input continuous-time signal?