

University of California, Berkeley  
 College of Engineering  
 Department of Electrical Engineering and Computer Science

EE240B Spring 2018  
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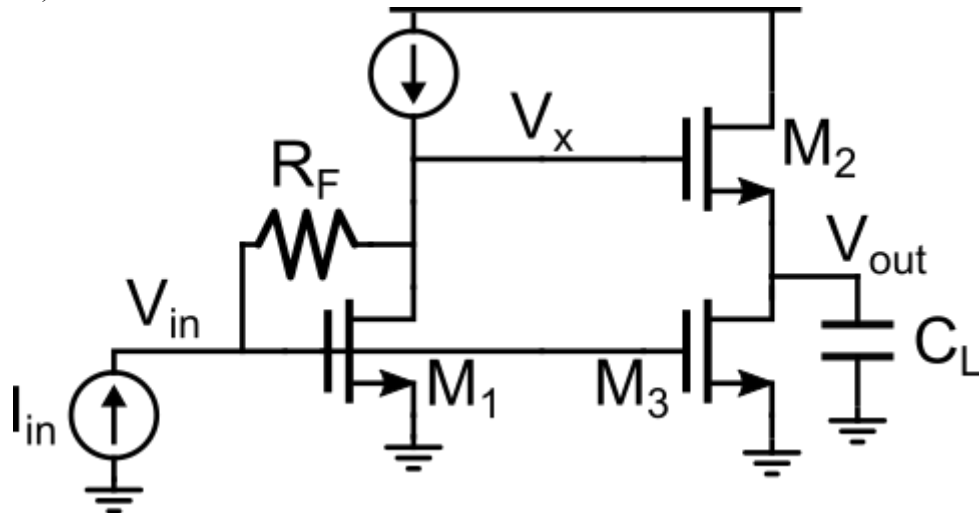
**HW2**

**Due: Thursday, February 15 at 5pm PST**

This is an individual assignment. Make sure that you explain all of your answers. For these problems you may ignore body effect unless specifically told otherwise.

**1. TIA Noise analysis**

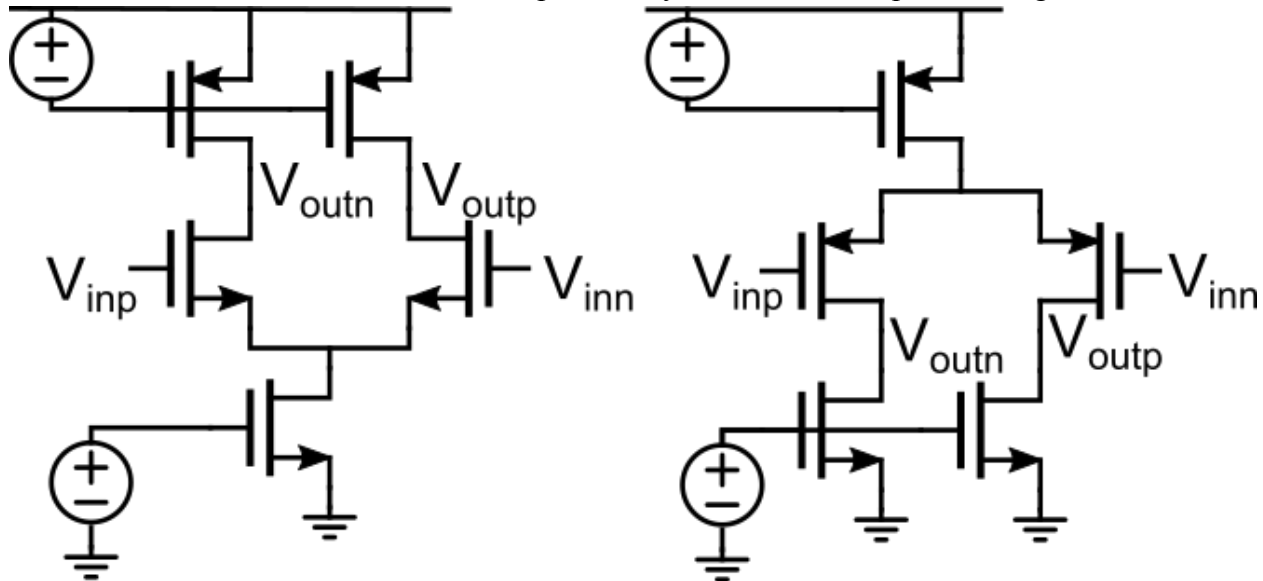
Consider the following circuit. Ignore all capacitors not explicitly drawn, and assume that all transistors have infinite  $r_o$ . Further, please assume that M1 and M3 have the same  $g_m$  ( $g_{m1}$ ), but that M2 has a different  $g_m$  ( $g_{m2}$ ). (We will look at how to pick this  $g_{m2}$  relative to  $g_{m1}$  as a part of this problem.)



- Compute  $v_{in}/i_{in}$  and  $v_x/i_{in}$ .
- Compute  $v_{in}/i_{n1}$  and  $v_x/i_{n1}$ , where  $i_{n1}$  is the noise current of M1.
- Find the transfer function  $v_{out}/i_{in}$  and the integrated output noise voltage variance due to  $i_{n1}$ .
- Relative to  $g_{m1}$ , what value of  $g_{m2}$  minimizes the output voltage noise variance due to  $i_{n1}$ ?
- Now assume that the  $C_{gg}$ 's associated with M1 and M3 add some total capacitance  $C_{in}$  to the input node  $V_{in}$ . Using the same (relative) value of  $g_{m2}$  you found in part d), repeat parts b) and c). Why is the result so qualitatively different than the minimum noise variance you found in part d)?

## 2. Noise-limited Design Methodology (Simple OTA)

In this problem you will be developing a methodology to design a simple CMOS OTA based on either total integrated noise or output noise density constraints. Two examples of such a simple OTA (one with PMOS input and one with NMOS input) are shown below. As this design has many degrees of freedom (just like in practical circuit), please feel free to include additional constraints/assumptions to make the design process easier (especially when you first start). However, you should clearly state these constraints/assumptions, and briefly explain under which conditions these constraints/assumptions may result in a sub-optimal design.



As a reminder, if you wish to get accurate matching between calculation and simulation, feel free to generate additional characterization tables for your design – e.g., characterizing the noise  $\gamma$  factor across various bias points.

As usual, the goal for your methodology should be to minimize the power dissipated by the circuit. The input specifications for your design methodology (generator) are listed below. Along with each specification, for those that are input parameters, we will provide in parentheses representative values that you should use for preliminary evaluations of your methodology.

- Use transistor finger widths of only  $0.5\mu\text{m}$ . You are free to choose the channel length of your device. However, you must only use one channel length for all transistors.
- Supply voltage  $V_{DD}$ . (Example value:  $V_{DD} = 1.2\text{V}$ )
- You are free to choose your input common mode voltage, as long as it is between 0 and  $V_{DD}$ .
- Minimum load capacitance  $C_{load}$ . This represents the minimum capacitance at the output of your OTA; you may add extra load capacitance beyond this if you wish. (Example value:  $C_{load} = 10\text{fF}$ )

- Output common mode voltage  $V_{outcm}$ . Note that this common mode voltage specification is measured with zero differential input voltage and the input common mode at whatever value you have chosen. (Example value:  $V_{outcm} = 600mV$ )
- Minimum tail current source  $V_{DS,min}$ . Set the tail transistor's  $V^*$  to match that of the input transistors. (Example value:  $V_{DS,min} = 200mV$ )
- Input-referred maximum linear amplitude  $V_{imax}$ . You can either use this specification to directly set the  $V^*$  of the input devices (as discussed in lecture), or you can instead use an either large signal or small signal gain variation specification. (Example value:  $V_{imax} = 150 mV$ )
- Minimum DC gain  $A_{min}$ . (Example value:  $A_{min} = 8 V/V$ ).
- The sinusoidal input signal amplitude  $V_{sig}$ . (Example values:  $V_{sig} = 50 mV$  for integrated noise, and  $V_{sig} = 20 mV$  for noise density)
- Minimum 3-dB bandwidth  $f_{3dB}$ . (Example values:  $f_{3dB} = 10GHz$  for integrated noise,  $f_{3dB} = 2GHz$  for noise density)
- Noise integration interval  $[f_{start}, f_{stop}]$ . (Example values: for integrated noise,  $[1MHz, 100GHz]$ ; for noise density,  $[1.4GHz, 1.6GHz]$ )  
NOTE: for simulating total integrated noise, the exact integration interval often depends on the application. However, for most circuits, a general guideline is to set  $f_{start}$  to be 3 to 6 decades below the signal bandwidth, and set  $f_{stop}$  to 1 to 3 decades above the signal bandwidth.
- Minimum SNR  $SNR_{min}$ . (Example value:  $SNR_{min} = 50dB$ ).

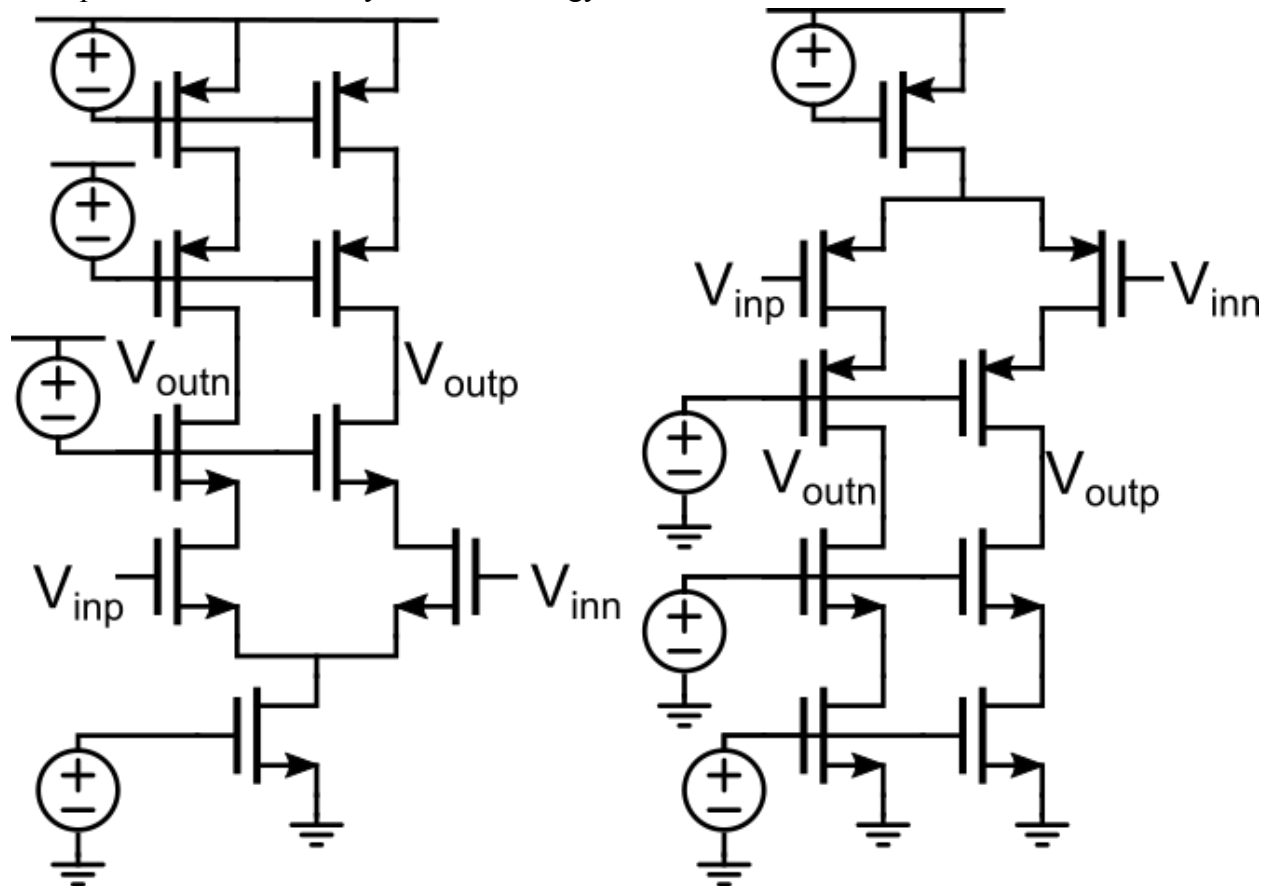
As usual, please submit a single script file that performs the computations need to design the amplifier. For the representative input values, you should print out all of the relevant sizing/biasing results, and you should compute the error between the specified performance and a simulation of the design.

NOTE: In this technology, if you use minimum channel length device, flicker-noise is very high, so your noise calculation for the total-integrated noise case may deviate significantly from simulation (up to 2X) if you do not take flicker noise in to account. If you didn't do anything special to account for flicker-noise, don't worry about it.

### 3. Noise-limited Design Methodology (Cascode)

In this problem we will develop a design methodology (much like we did in problem 2) for a telescopic cascoded differential OTA. Unlike problem 2 however, for the sake of simplicity, this time we will develop a methodology only for the noise density-limited case. As shown in the example schematic below, you are free to use ideal voltage sources for the cascode gate biases, and you are free to set the values of those voltage sources (as long as they are between 0 and  $V_{DD}$ ). To simplify your methodology (and for layout-related reasons that we will discuss later in

class), your cascode transistors must use finger widths of  $0.5\mu\text{m}$  (just like all of the other transistors), but the total width of the cascode devices must be between 1-4X the total width of the transistor that it is stacked on top of (e.g., for an NMOS input OTA, the NMOS cascode devices must have 1-4X the total width of the NMOS input devices). The input specifications (parameters) for this design should be identical to problem 2, but you should use the following example values to evaluate your methodology:



- $C_{load} = 10\text{fF}$ .
- $V_{outcm} = 600\text{mV}$ .
- $V_{DST,min} = 150\text{mV}$ .
- $V_{imax} = 150\text{mV}$ .
- $A_{min} = 30\text{ V/V}$
- $SNR_{min} = 50\text{ dB}$ .
- $V_{sig} = 10\text{ mV}$
- $f_{3db} = 500\text{ MHz}$
- $[f_{start}, f_{stop}] = [100\text{MHz}, 200\text{MHz}]$