

# EE 247B / ME 218 Discussion 10

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# EQUIVALENT CIRCUITS & SENSING

Let's do some analysis on the resonance behavior of this comb-drive structure

## Structural Material Properties:

Young's Modulus,  $E = 150 \text{ GPa}$ ; Density,  $\rho = 2,300 \text{ kg/m}^3$

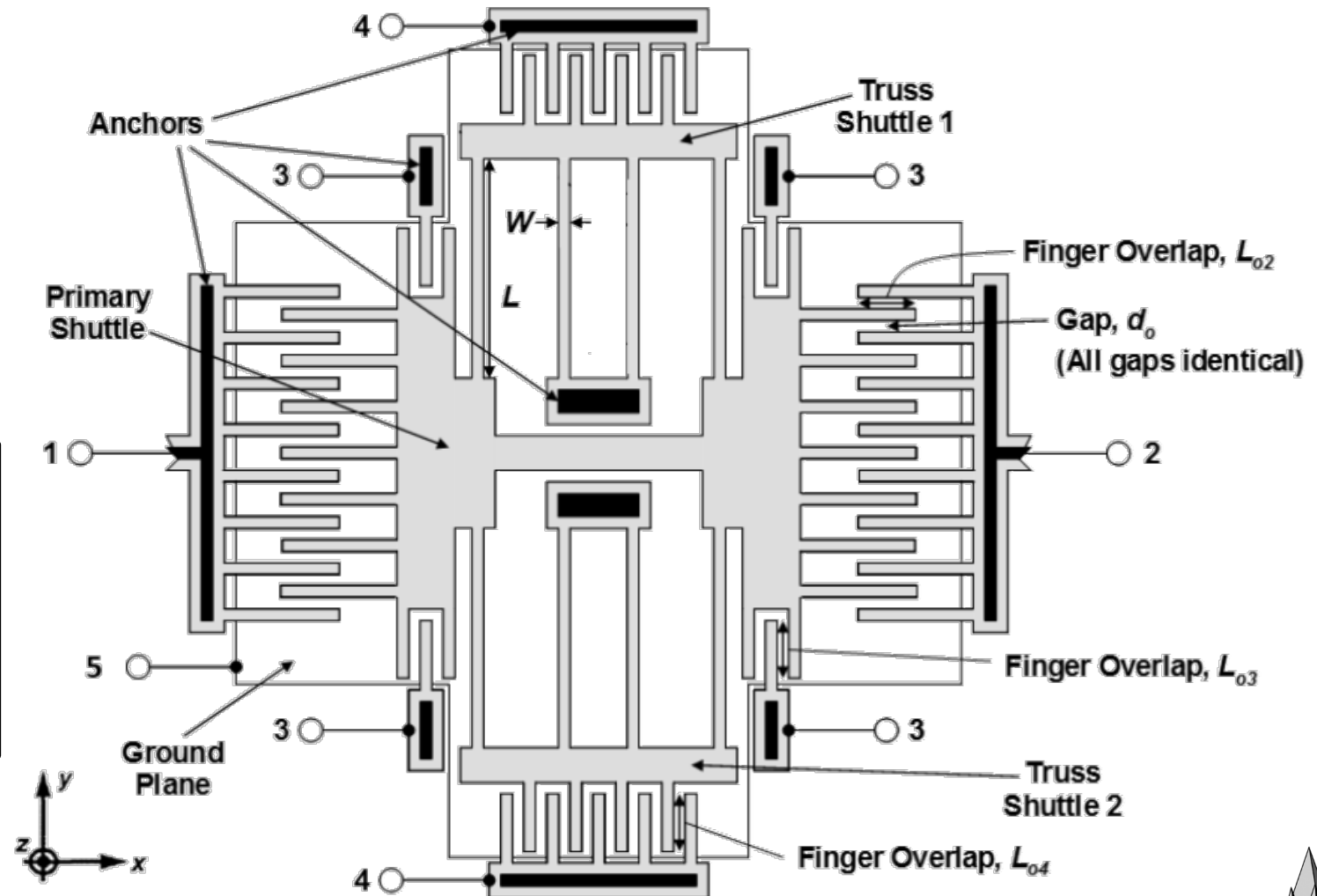
Poisson ratio,  $\nu = 0.226$ ;  $Q = 100,000$

## Geometric Dimensions:

$L = 50 \mu\text{m}$ ;  $W = 2 \mu\text{m}$ ; Thickness,  $h = 2 \mu\text{m}$ ; All Finger Gaps,  $d_o = 1 \mu\text{m}$

All Finger Overlaps,  $L_o = 10 \mu\text{m}$ , Truss Shuttle 1 Area =  $300 \mu\text{m}^2$

Truss Shuttle 2 Area =  $300 \mu\text{m}^2$ , Primary Shuttle Area =  $4,000 \mu\text{m}^2$



# x-DIRECTION RESONANCE FREQUENCY

First, let's find  $f_0$  when all ports are grounded

$$f_0 = \sqrt{\frac{k_s}{m_s}} \frac{1}{2\pi} \quad k_s = k_c = \frac{2Ew^3h}{L^3} = \frac{2(150G)(2\mu)^4}{(50\mu m)^3} = 38.4 \text{ N/m}$$

$$m_s = M_s + \frac{1}{4}M_t + \frac{12}{35}M_b = 20.35 \text{ ng}$$

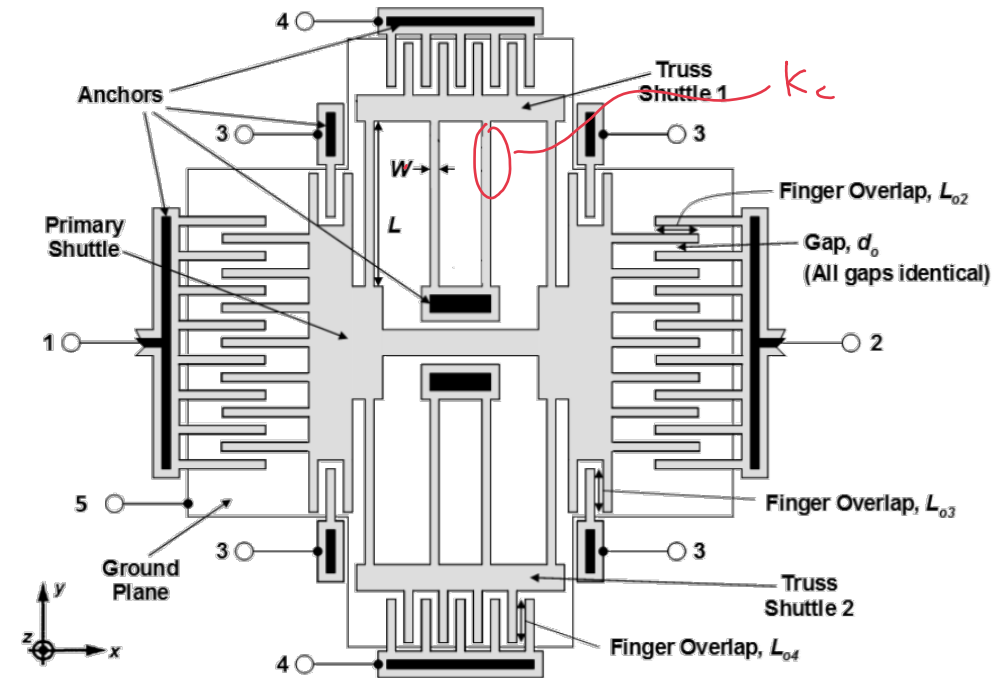
$$M_s = \rho h A_s$$

$$M_t = 2\rho h A_t$$

$$M_b = 8\rho h L W$$

$$\omega_0 = \sqrt{\frac{38.4}{20.3 \text{ n}}} = 1.37 \frac{\text{Mrad}}{\text{s}}$$

$$\hookrightarrow f_0 = 218.6 \text{ kHz}$$



# x-DIRECTION RESONANCE FREQUENCY

Now, let's find  $f_0$  when ports 1, 2 & 4 are grounded, and all other ports are biased to 50 V

$$f_0' = f_0 \sqrt{1 - \frac{k_{eq}}{k_t}}$$

$$k_{eq} = V_p^2 \frac{C_{o4}}{d_o^2} = V_p^2 \frac{\epsilon_0 (2N_f h L_o)}{d_o^3} = 7 \frac{N}{m}$$

$$\frac{1}{2} m_t v_t^2 = \frac{1}{2} m_s v_s^2$$

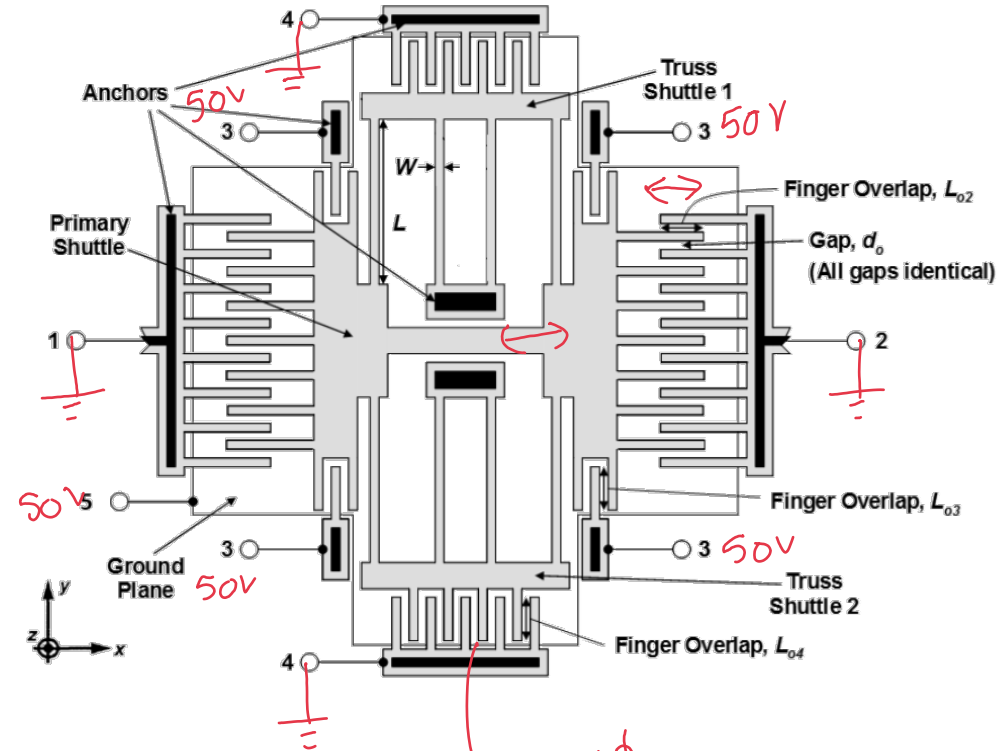
$$m_t = \left(\frac{v_s}{v_t}\right)^2 m_s = 4 m_s \Rightarrow k_t = 4 k_s = 154 \frac{N}{m}$$

$$x_t = \frac{1}{2} x_s$$

$$v_t = \frac{1}{2} v_s$$

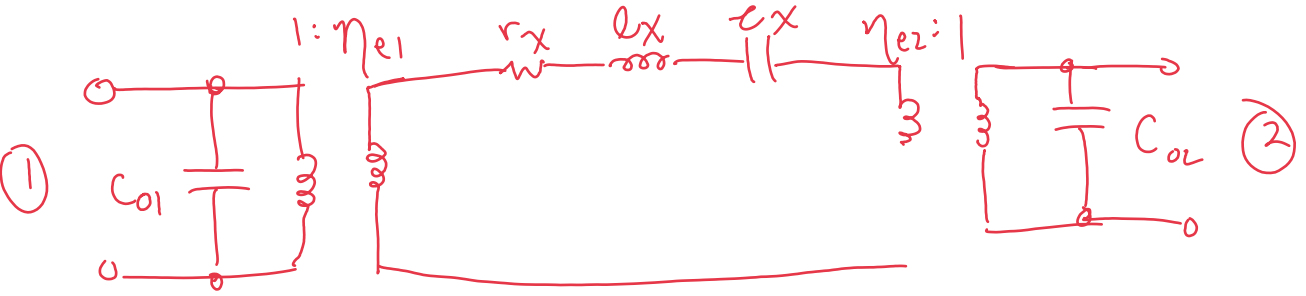
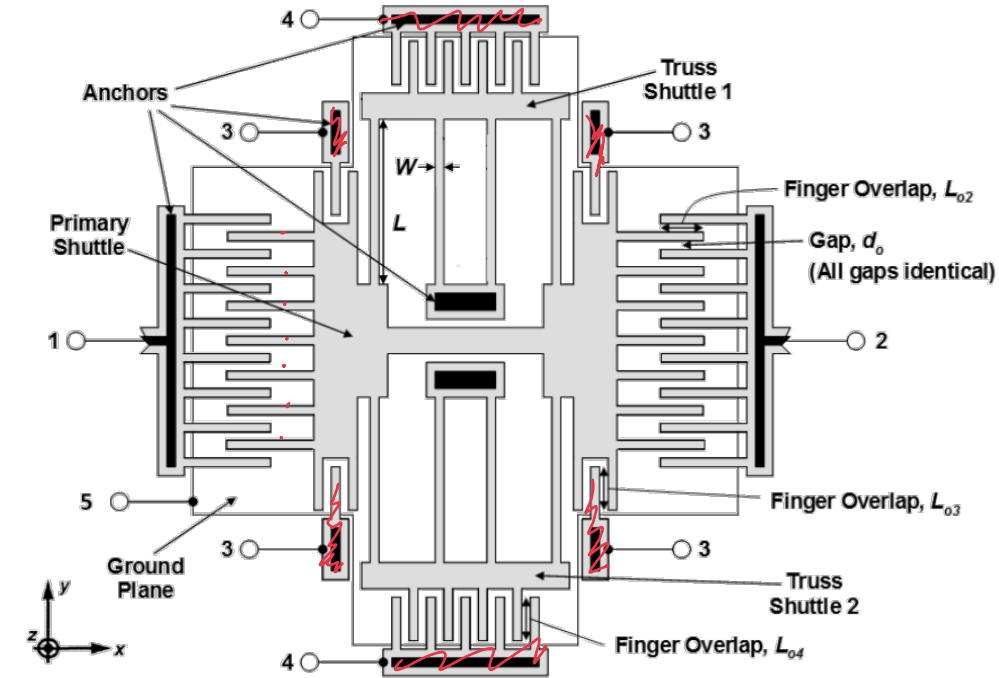
$$f_0' = 0.977 f_0 = 213.5 \text{ kHz}$$

$$\sqrt{1 - k_{eq}/k_t}$$



# EQUIVALENT CIRCUIT

Now draw the transformer-based equivalent circuit (between ports 1 & 2) with other ports biased to 50 V



$$L_x = m_s = 2.035 \times 10^{-11} \text{ kg (H)}$$

$$z_x = \frac{1}{k_s} = 0.026 \frac{\text{m}}{\text{N}} \text{ (F)}$$

$$r_x = b_{re} = \frac{\sqrt{k_s m_s}}{\varphi} = 0.28 \frac{\text{nkgy}}{\text{s}} \text{ (n}\Omega\text{)}$$

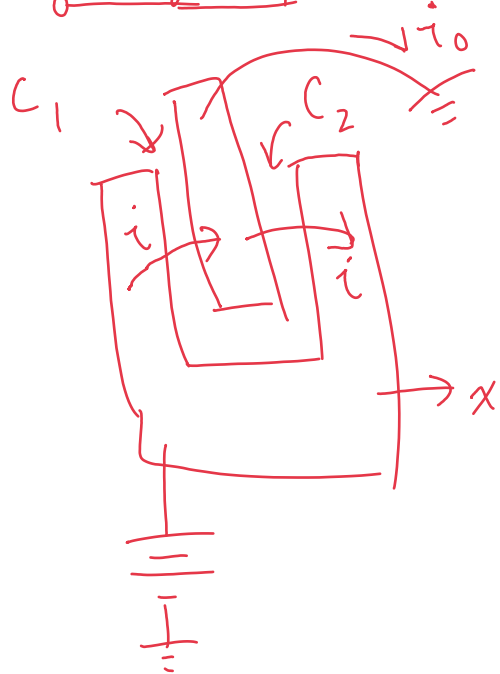
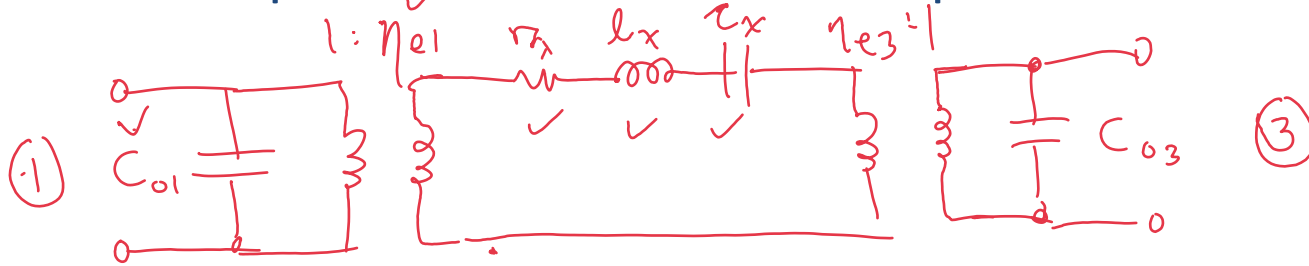
$$\eta_{e1} = \eta_{e2} = V_p \frac{\partial C}{\partial x} = V_p \frac{2N f_1 \epsilon_0 h}{d_0}$$

$$= 1.24 \times 10^{-8} \text{ C/m}$$

$$C_{01} = C_{02} = \frac{\epsilon_0 h L_0 (2N f_1)}{d_0} = 2.48 \text{ fF}$$

# EQUIVALENT CIRCUIT

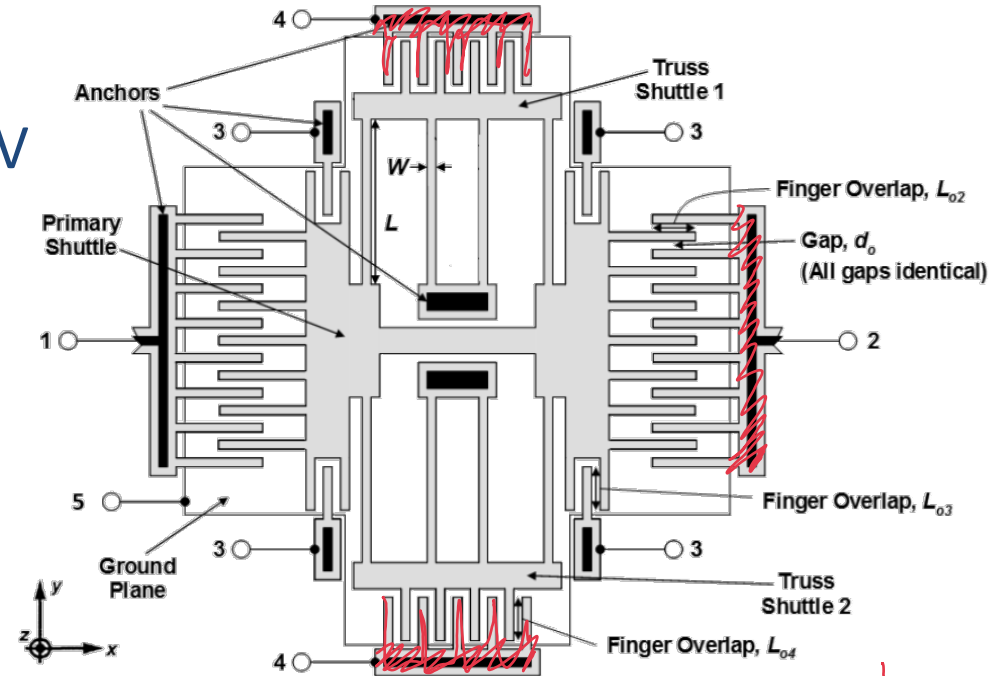
Next, draw the transformer-based equivalent circuit between ports 1 & 3 with all other ports are biased to 50 V



$$\frac{\partial C_1}{\partial x} \approx \frac{C_{03}}{8d_0} \quad \frac{\partial C_2}{\partial x} \approx -\frac{C_{02}}{8d_0}$$

$$i_0 = V_p \underbrace{\left( \frac{\partial C_1}{\partial x} + \frac{\partial C_2}{\partial x} \right)}_{N_{e3} = 0} \frac{dx}{dt} = 0$$

$$C_{03} = \frac{\epsilon_0 h L_{03} 2 N f \cdot 4}{d_0}$$



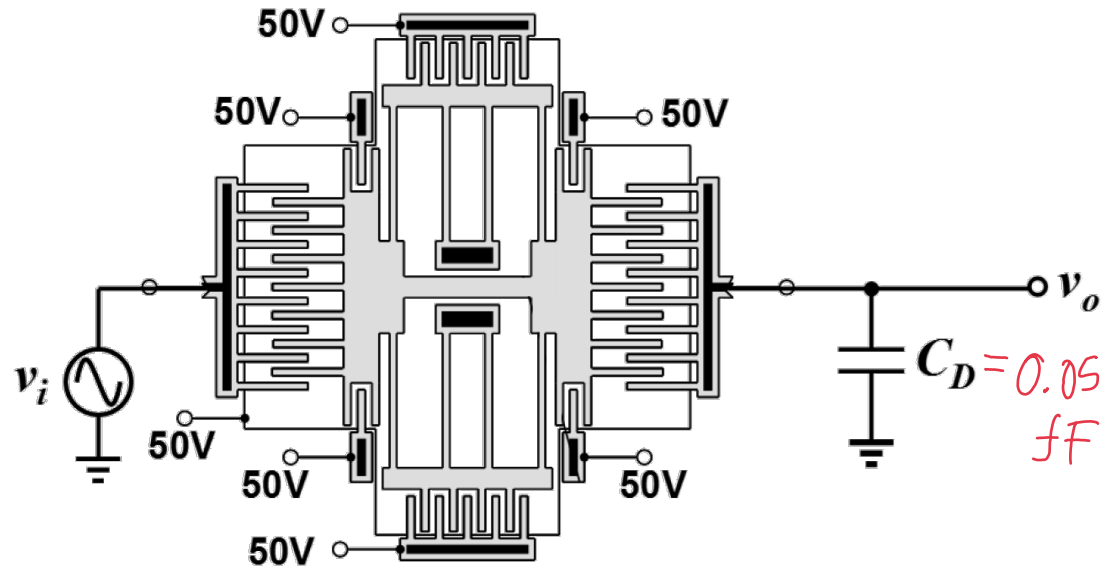
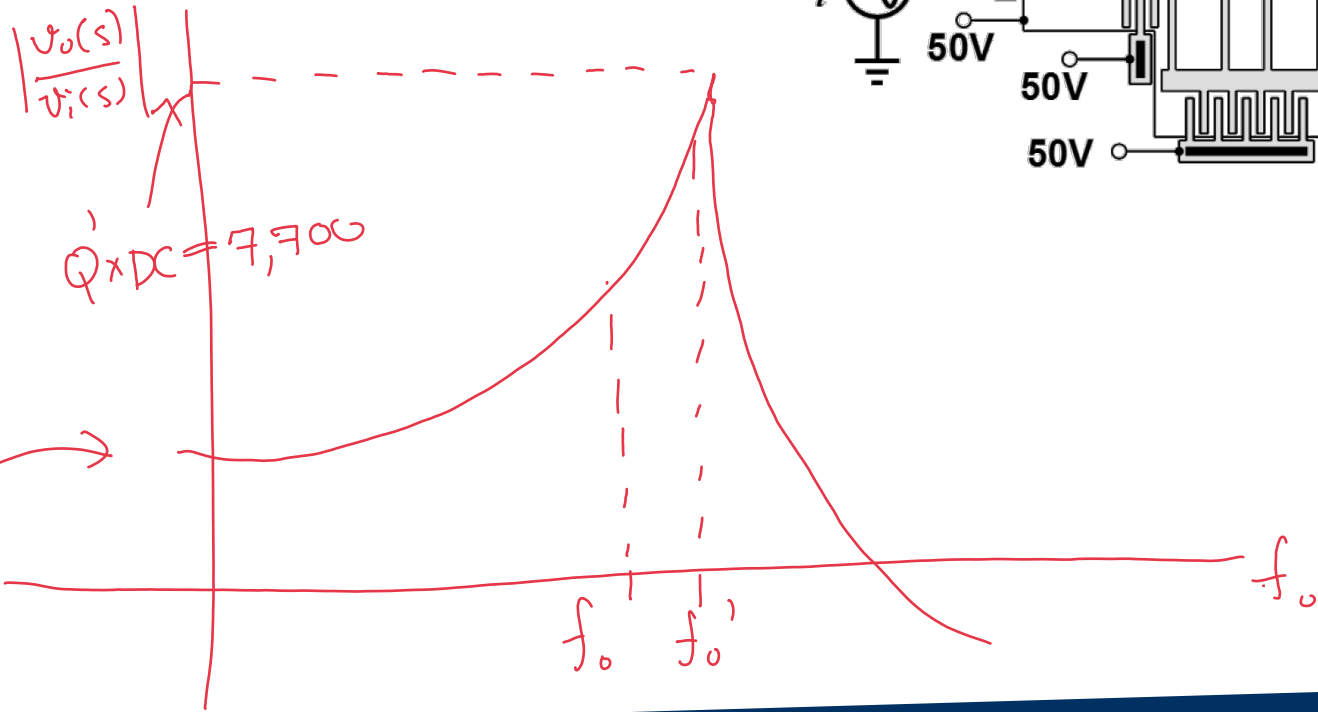
# SENSING

$$\left| \frac{v_o(s)}{v_i(s)} \right| = \underbrace{\frac{C_x / C_D}{1 - C_x / C_D}}_{\text{DC gain}} \cdot \underbrace{\frac{(\omega_o')^2}{s^2 + \left(\frac{\omega_o'}{Q'}\right)s + (\omega_o')^2}}_{\text{low-pass biquad}}$$

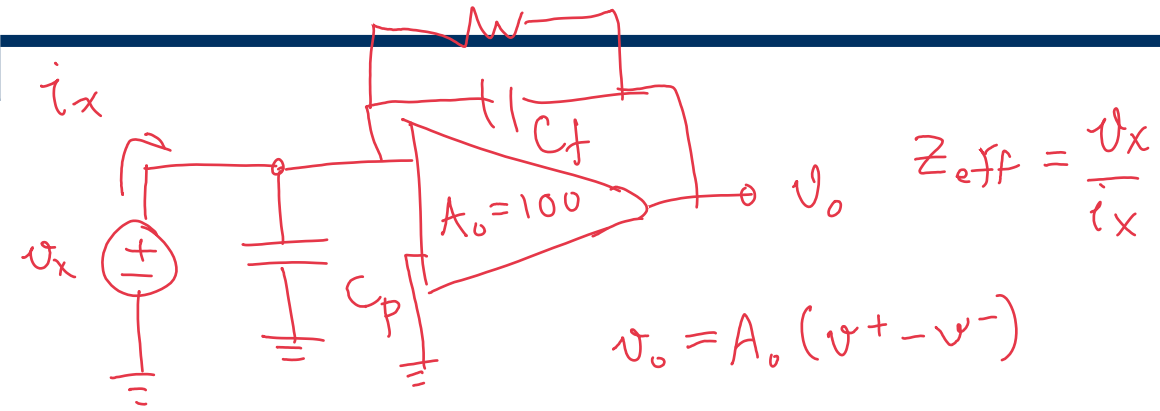
$$\omega_o' = \omega_o \sqrt{1 + \frac{C_x}{C_D}}$$

$$Q' = Q \sqrt{1 + \frac{C_x}{C_D}}$$

$$C_x = \eta_{ei}^2 \epsilon_x \approx 4 \text{ aF}$$



# SENSING



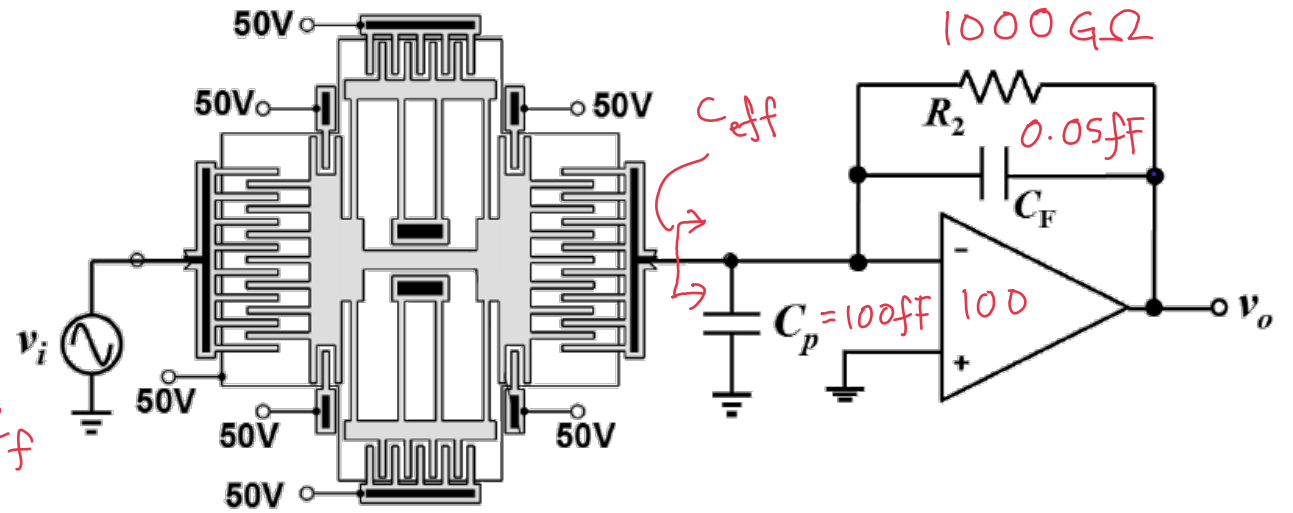
$$Z_{eff} = \frac{1}{s [C_p + (1+A_o)C_f]} \rightarrow C_{eff} = C_p + (1+A_o)C_f$$

$$C_{eff} \approx 105 \text{ fF}$$

$$f_o' = f_o \left( 1 + \frac{4 \text{ aF}}{105 \text{ fF}} \right)^{1/2} = 1.00004 f_o$$

↳ much closer to  $f_o$

$$\frac{v_o(s)}{v_i(s)} = \frac{C_x/C_{eff} (\omega_o')^2}{1 + C_x/C_{eff} s^2 + \left(\frac{\omega_o'}{Q'}\right)s + (\omega_o')^2} \underbrace{(-A_o)}_{\frac{v_o}{v^-}}$$



$$v_o = A_o (v^+ - v^-)$$

$$= -A_o v^-$$

$$\frac{v_o}{v^-} = -A_o$$