

Lecture 13: Beam Combos I

- Announcements:
- HW#3 due Tuesday, 3/10, at 8 a.m.
- Midterm Exam about 2 weeks away, Thursday, March 19, 9:30-11:00 a.m., 521 Cory (right here)

- Reading: Senturia, Chpt. 9

- Lecture Topics:

- ↳ Bending of beams
- ↳ Cantilever beam under small deflections
- ↳ Combining cantilevers in series and parallel
- ↳ Folded suspensions
- ↳ Design implications of residual stress and stress gradients

- Last Time:

- Finished stress gradients
- Now, move into beam combos



Bending Due to Stress/Strain Gradients

Find the radius of curvature:

Prior to release, axial stress: $\sigma = \sigma_0 - \frac{\sigma_1}{(H/2)} z$

The internal moment:

$$M_x = \int_{-H/2}^{H/2} [(W \cdot dz) \sigma] \cdot z = \int_{-H/2}^{H/2} W \left(z \sigma_0 - \frac{\sigma_1 z^2}{(H/2)} \right) dz$$

$$= W \left(\frac{1}{2} \sigma_0 z^2 - \frac{2 \sigma_1 z^3}{3H} \right) \Big|_{-H/2}^{H/2}$$

$$= W \left(\frac{1}{2} \sigma_0 \frac{H^2}{4} - \frac{2}{3} \sigma_1 \frac{H^3}{8} - \frac{1}{2} \sigma_0 \frac{H^2}{4} + \frac{2}{3} \sigma_1 \frac{H^3}{8} \right)$$

average stress cancel out

$$M_x = -\frac{1}{6} \sigma_1 W H^2$$

Thus, the radius of curvature:

$$\frac{1}{R} = -\frac{M_x}{E'I} \rightarrow R = \frac{E'I}{M_x} = \frac{1}{2} \frac{E'H}{\sigma_1}$$

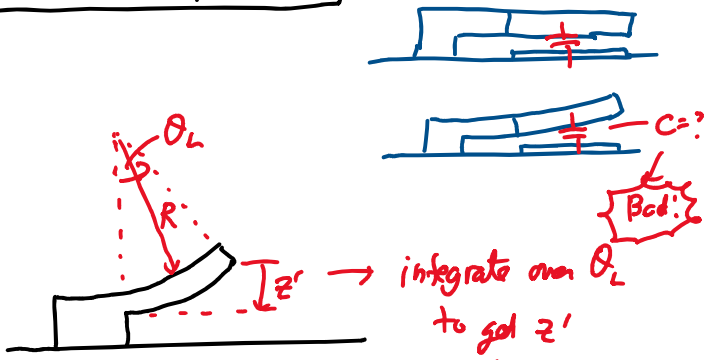
[I = $\frac{1}{12} W H^3$]

Biaxial Modulus
(if W is large)

$$R = \frac{1}{2} \frac{E}{(1-\nu)} \frac{H}{\sigma_1}$$

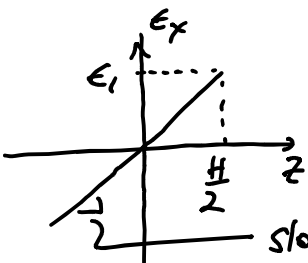
Radius of Curvature for a Cantilever w/ a Stress Gradient

Radius of Curvature $\rightarrow z'$



integrate over θ_L
 to get z'
 ↓
 Do this in homework ...

Definition. Strain Gradient

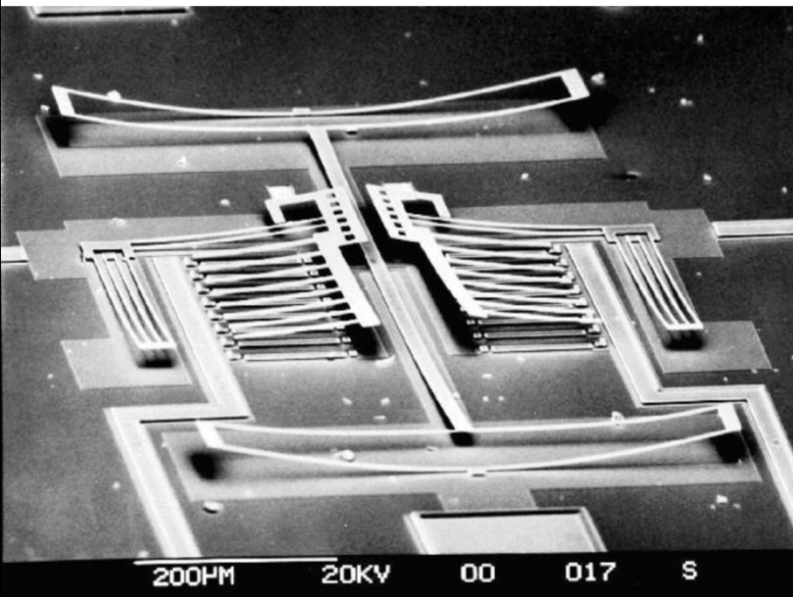


slope \triangleq Strain Gradient: Γ

$$R = \frac{1}{2} \frac{E}{1-\nu} \frac{H}{\sigma_1} = \frac{H}{2} \frac{E'}{\sigma_1} = \frac{(H/2)}{\epsilon_1} = \frac{1}{\Gamma} \rightarrow \boxed{\Gamma = \frac{1}{R}} \checkmark$$

3

• ... and the result:



• We just quantified this

4

Folded-Beam Suspension

⇒ Module 8, slide 22

① During deposition @ high T
↳ stress free

② Cool to room temp (RT)
↳ stress

Substrate force } compressive stress

How to defend against this?

- ① Δ process parameters → e.g. the deposition recipe
↳ problem: can't always do this
- ② Design → folded-beam!

5

Analyzing an Interconnected Ensemble of Beams (Springs) & Masses

Typical Questions: → all demand that we know $\alpha = f(F)$

- ① How does the structure move in response to a force at a specific location.
↳ that we know
- ② What is the frequency response to an AC force applied at a specific location.
↳ the stiffness!
- ③ Noise?
- ④ Response to environmental stimuli? (e.g., rotation)
- ⑤ How does stress affect the behavior of the structure?

6

Procedure: (to get stiffness)

① Build the ckt. (Extract the ckt.) → in the x-direction (for this example)

Anchor

Anchor

② Analyze to get $x = f(F)$
 ↑ force
 ↓ displacement

$F = kx \Rightarrow x = \frac{F}{k} = \left(\frac{1}{k}\right)F$
 ↑ compliance

(a) Case 1: Series

← across variable
 ← thru variable
 ← across variable
 ← thru variable

want this ∴ need k_{tot}
 $x_{tot} = \left(\frac{1}{k_{tot}}\right)F$

series because one must go thru both k_1 & k_2 to get from anchor to the forcing pt.

7

* $x_{tot} = x_1 + x_2 = F \left(\frac{1}{k_1} + \frac{1}{k_2} \right) = \frac{F}{\left(\frac{1}{k_1} + \frac{1}{k_2} \right)} = \frac{F}{k_{tot}}$
 identifies series

["||" operator $\hat{=} A || B = \frac{1}{\frac{1}{A} + \frac{1}{B}} = \frac{AB}{A+B}$]

$k_{tot} = k_1 || k_2$ (for k_1 & k_2 in series)

For EEs: same as capacitors (springs combine like capacitors)

$\frac{1}{C_1} || \frac{1}{C_2} \hat{=} \frac{1}{C_1 || C_2}$

(b) Case 2: Parallel Springs

$x_1 \rightarrow F_1 = k_1 x_1 = k_1 x_{tot}$
 $F_2 = k_2 x_{tot}$
 $F = k_{tot} x_{tot}$
 $x_{tot} = x_1 = x_2$

indicates parallel
 or → only need to go through one of the springs to get from the anchor to the forcing pt.

8

$F = F_1 + F_2 = (k_1 + k_2) x_{tot}$
 \downarrow
 K_{tot}
 \downarrow
 $K_{tot} = k_1 + k_2$ (for k_1 & k_2 in parallel)

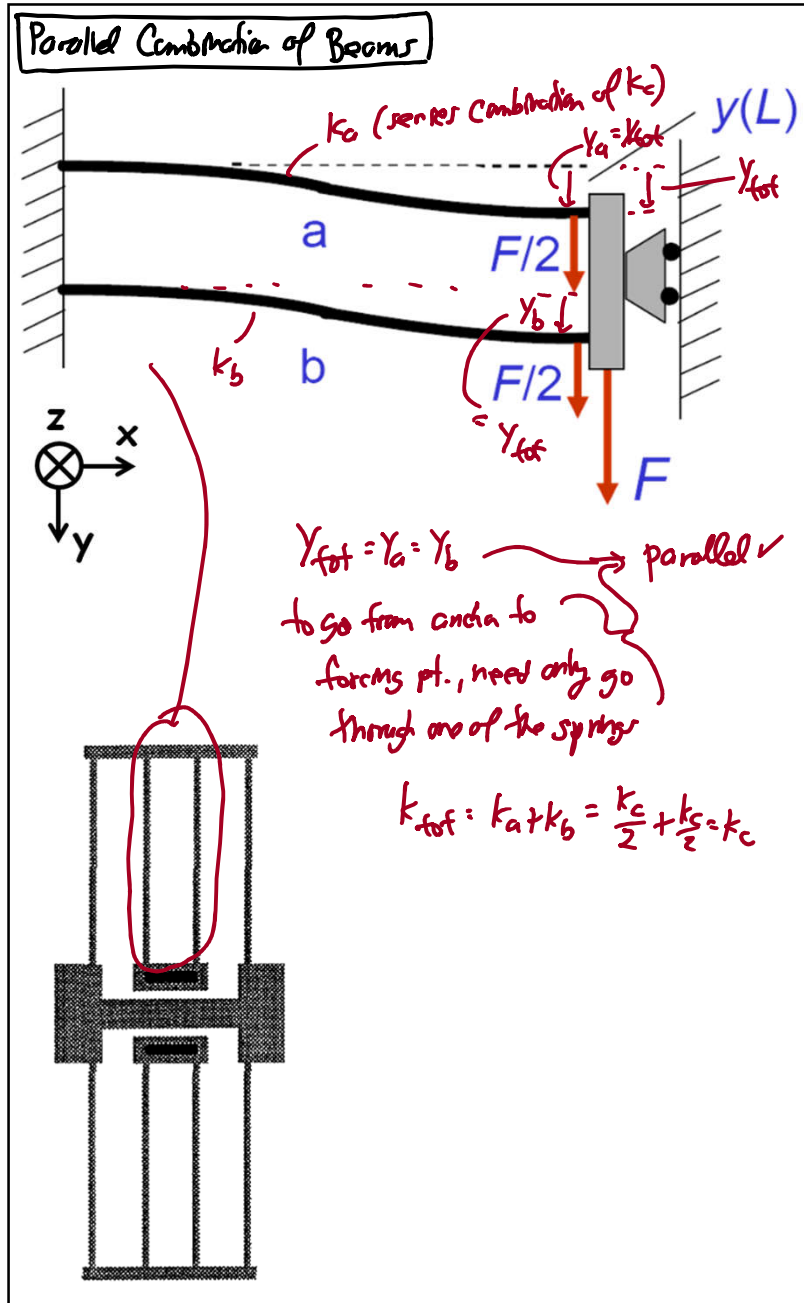
Series Combination of Springs

Anchored: Clamped B.C. (maintains 90°)
 Free B.C. (just like cantilever)
 Guided B.C. (maintains 90°)
 $L = 2L_c$
 $F \leftarrow$ forcing pt.
 $y_{tot} = y_1 + y_2 \therefore$ series ✓
 series ✓ $\left\{ \begin{array}{l} \text{Also must go thru both springs} \\ \text{to get from anchor to forcing pt.} \end{array} \right.$

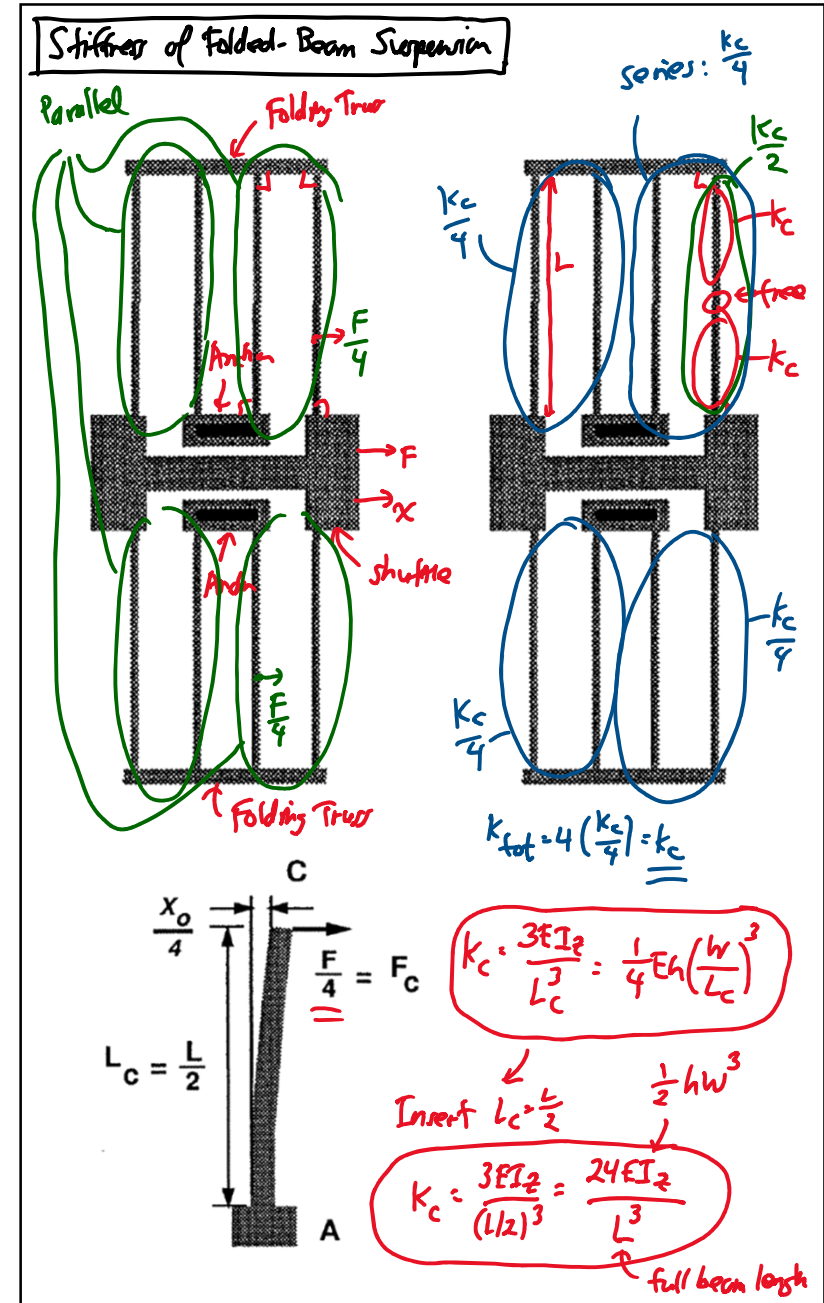
$$k_{tot} = k_1 || k_2 = \frac{1}{\frac{1}{k_1} + \frac{1}{k_2}} = \frac{k_1 k_2}{k_1 + k_2}$$

$$\left. \begin{array}{l} k_2 = k_c \\ k_1 = k_c \end{array} \right\} k_1 = k_2 = k_c \Rightarrow k_{tot} = \frac{k_c}{2}$$

 \uparrow
 cantilever stiffness



11



12

Micromedical Filtration

Input Electrode, Suspension Beam, Coupling Beam, Output Electrode, Anchors, Shuttle 1, Folding Truss, Shuttle 2.

Dimensions: $L_{cs} = 200 \mu\text{m}$, $100 \mu\text{m}$, $2 \mu\text{m}$.

Force F applied at point A, displacement x_A .

Stiffness k_c .

m_1 , m_2 (shuttle 2)

\Rightarrow Find the stiffness at point A.

apply F @ A \rightarrow what is x_A ? $\left. \vphantom{\begin{matrix} \text{apply } F \text{ @ A} \\ \rightarrow \text{ what is } x_A \end{matrix}} \right\} x_A = \frac{F}{k_A}$

$k_A \triangleq$ stiffness @ point A

want this

Assume: shuttle & Folding truss are rigid.
 beams are small \therefore neglect their mass

Equivalent model: m_1 and m_2 connected by k_b . m_1 connected to anchor by k_c . m_2 connected to anchor by k_c . Force F at point A, displacement x_A .

need this k_b

13

Get k_b :

Series \downarrow $k_{cs} \frac{1}{4}$

parallel $\rightarrow \frac{k_{cs}}{2} = k_b$

free

cantilever $\rightarrow k_{cs}$ "coupling springs"

series $\rightarrow \frac{k_{cs}}{2}$

$\therefore k_A = k_c + k_{combined}$
 $= k_c + k_c \parallel k_b = k_c + k_c \parallel \frac{k_{cs}}{2} = k_A$

where $k_c = \frac{24EI_z}{L^3}$

$k_{cs} = \frac{24EI_z}{L_{cs}^3}$

14