

Lecture 22: Gyroscopes & Sensing Circuits I

- Announcements:
- Project Slide Set #2 due Friday, April 17
- HW#6 online and due Friday, 5/1, at 8 a.m.
- Module 14 on "Sensing Circuits" online
- Module 15 on "Gyros, Noise, & MDS" online (actually with last lecture)
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- Reading: Senturia, Chpt. 14, Chpt. 16, Chpt. 21
- Lecture Topics:
 - ↳ Gyroscopes
- Reading: Senturia, Chpt. 14
- Lecture Topics:
 - ↳ Detection Circuits
 - Velocity Sensing
 - Position Sensing
-
- Last Time:
- Finished equivalent circuits
- Now, move on to gyroscopes using Module 15

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Velocity-to-Voltage Conversion

represent velocity
 V_o
 R_D
 cantilever
 V_i
 V_P
 i_o
 in phase w/ velocity
 (and 90° phase-shifted from displacement)
 $\left| \frac{V_o}{V_i} \right|$
 ω

Get output current i_o into ground!

N_i
 F_{dl}
 i_o
 V_P

$$\frac{x}{F_{dl}} = \frac{1}{k} @ DC$$

$$\frac{x}{F_{dl}} \Big|_{\omega_0} = \frac{Q}{jk} = \frac{1}{k} \frac{Q}{j}$$

$$\frac{\dot{x}}{F_{dl}}(s) = \frac{\omega_0 Q}{k} \textcircled{+}(s) \quad \leftarrow \text{f/ last time}$$

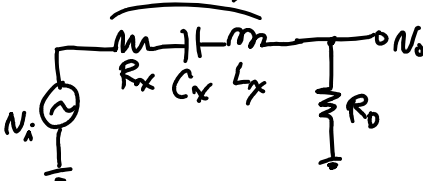
$$[F_{dl} = \eta e_1 N_i] \Rightarrow \frac{\dot{x}}{N_i}(s) = \eta e_1 \frac{\omega_0 Q}{k} \textcircled{+}(s)$$

$$[i_o = \eta e_2 \dot{x}] \Rightarrow \frac{i_o}{N_i}(s) = \eta e_1 \eta e_2 \frac{\omega_0 Q}{k} \textcircled{+}(s) = \frac{\eta e_1 \eta e_2 Q}{m \omega_0} \textcircled{+}(s)$$

$\frac{1}{R_{x12}}$

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Now, include R_D : $Q = \frac{\omega_0 L_x}{R_x}$



$$\frac{N_o}{N_i}(s) = \frac{R_D}{R_x + \frac{1}{sC_x} + sL_x + R_D} = \dots \text{math} \dots$$

$$= \frac{R_D}{R_x + R_D} \frac{s \left(\frac{R_x + R_D}{L_x} \right)}{s^2 + s \left(\frac{R_x + R_D}{L_x} \right) + \frac{1}{L_x C_x}}$$

Gain Term Freq. Shaping Term

$$\left[Q = \frac{\omega_0 L_x}{R_x} \rightarrow Q' = \frac{\omega_0 L_x}{R_x + R_D} \rightarrow \frac{R_x + R_D}{L_x} = \frac{\omega_0}{Q'} \right]$$

$$\frac{N_o}{N_i}(s) = \frac{R_D}{R_x + R_D} \frac{s(\omega_0/Q')}{s^2 + s(\omega_0/Q') + \omega_0^2}$$

$$\frac{N_o}{N_i}(s) = \frac{R_D}{R_x + R_D} \cdot \mathcal{H}(s, Q')$$

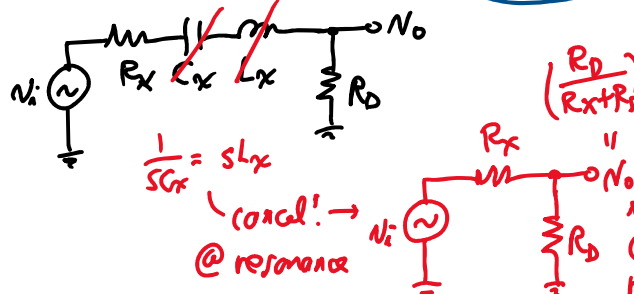
$Q' < Q$ X → not good

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Original "unsensed" mechanical detke
 i_o goes to ground
 \downarrow
 $Q = \text{large}$

$\left| \frac{N_o}{N_i}(s) \right|$ sensed by R_D : $Q' < Q$
 $Q \left(\frac{R_x}{R_x + R_D} \right)$ } Big Problem!
 < 1

Analysis @ Resonance:



$\frac{1}{sC_x} = sL_x$
cancel! → @ resonance

$\left(\frac{R_D}{R_x + R_D} \right) N_i$
@ Resonance

cannot to general freqs.: $X \mathcal{H}(s, Q')$

$$\frac{N_o}{N_i}(s) = \frac{R_D}{R_x + R_D} \mathcal{H}(s, Q'), \text{ where } Q' = Q \left(\frac{R_x}{R_x + R_D} \right)$$

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* The Problem is actually much bigger!

Next Step
 $\frac{1}{3R_L} \frac{1}{C_L}$
Load R_L

Includes C_o , line C , bond pad C , and next stage C

to sense velocity

Now, we get:

$$\frac{N_o}{N_i}(s) \sim \frac{R_o || R_L}{R_x + R_o || R_L} \cdot \frac{1}{1 + \frac{s}{\omega_p}} \cdot \mathcal{H}(s, \omega_o, Q')$$

$$\omega_p = \frac{1}{(R_x || R_o || R_L) C_p}$$

↑
from mechanical device

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if $C_p = \text{large}$

$C_p = \text{small}$

OK

Problems w/ Purely Resistive Detection

- ① Need large R_D for large gain... but...
- ② $R_D \uparrow \rightarrow Q \downarrow$
- ③ $R_D \uparrow \rightarrow \frac{1}{R_D C_p} \downarrow \rightarrow$ get undesirable LPF cut-off freq.
- ④ Load $R_L \rightarrow$ affects gain! \rightarrow lose control of gain!

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