

UC Berkeley

EE C247B - ME C218 Introduction to MEMS Design Fall 2020

Prof. Clark T.-C. Nguyen

Dept. of Electrical Engineering & Computer Sciences
 University of California at Berkeley
 Berkeley, CA 94720

Module 17: Noise & MDS

EEC247B/MEC218: Introduction to MEMS Design LecM 17 C. Nguyen 11/18/08 1

1

UC Berkeley

Lecture Outline

- Reading: Senturia Chpt. 16
- Lecture Topics:
 - ↳ Minimum Detectable Signal
 - ↳ Noise
 - Circuit Noise Calculations
 - Noise Sources
 - Equivalent Input-Referred Noise
 - ↳ Gyro MDS
 - Equivalent Noise Circuit
 - Example ARW Determination

EEC247B/MEC218: Introduction to MEMS Design LecM 17 C. Nguyen 11/18/08 2

2

UC Berkeley

Determining Sensor Resolution

EEC247B/MEC218: Introduction to MEMS Design LecM 17 C. Nguyen 11/18/08 3

3

UC Berkeley

Minimum Detectable Signal (MDS)

- **Minimum Detectable Signal (MDS):** Input signal level when the signal-to-noise ratio (SNR) is equal to unity

Includes desired output plus noise

- The sensor scale factor is governed by the sensor type
- The effect of noise is best determined via analysis of the equivalent circuit for the system

EEC247B/MEC218: Introduction to MEMS Design LecM 17 C. Nguyen 11/18/08 4

4

UC Berkeley

Noise

EEC247B/MEC218: Introduction to MEMS Design LecM 17 C. Nguyen 11/18/08 5

5

UC Berkeley

Noise

- **Noise:** Random fluctuation of a given parameter $I(t)$
- In addition, a noise waveform has a zero average value

Avg. value (e.g. could be DC current)

- We can't handle noise at instantaneous times
- But we can handle some of the averaged effects of random fluctuations by giving noise a power spectral density representation
- Thus, represent noise by its mean-square value:

Let $i(t) = I(t) - I_D$

Then $\overline{i^2} = \overline{(I - I_D)^2} = \lim_{T \rightarrow \infty} \frac{1}{T} \int_0^T |I - I_D|^2 dt$

EEC247B/MEC218: Introduction to MEMS Design LecM 17 C. Nguyen 11/18/08 6

6

UC Berkeley

Noise Spectral Density

- We can plot the spectral density of this mean-square value:

EEC247B/MEC218: Introduction to MEMS Design LecM 17 C. Nguyen 11/18/08 7

7

UC Berkeley

Noise Sources

EEC247B/MEC218: Introduction to MEMS Design LecM 17 C. Nguyen 11/18/08 12

12

Thermal Noise

UC Berkeley

- Thermal Noise in Electronics:** (Johnson noise, Nyquist noise)
 - Produced as a result of the thermally excited random motion of free e^- 's in a conducting medium
 - Path of e^- 's randomly oriented due to collisions
- Thermal Noise in Mechanics:** (Brownian motion noise)
 - Thermal noise is associated with all dissipative processes that couple to the thermal domain
 - Any damping generates thermal noise, including gas damping, internal losses, etc.
- Properties:**
 - Thermal noise is white (i.e., constant w/ frequency)
 - Proportional to temperature
 - Not associated with current
 - Present in any real physical resistor

EE247B/ME218: Introduction to MEMS Design LecM 17 C. Nguyen 11/18/08 13

13

Circuit Representation of Thermal Noise

UC Berkeley

- Thermal Noise can be shown to be represented by a series voltage generator $\overline{v_R^2}$ or a shunt current generator $\overline{i_R^2}$

Note: These are one-sided mean-square spectral densities! To make them 2-sided, must divide by 2.

where $4kT = 1.66 \times 10^{-20} \text{ V} \cdot \text{C}$ and where these are spectral densities.

EE247B/ME218: Introduction to MEMS Design LecM 17 C. Nguyen 11/18/08 14

14

Noise in Capacitors and Inductors?

UC Berkeley

- Resistors generate thermal noise
- Capacitors and inductors are noiseless \rightarrow why?

Need to add a forcing function, like a noise voltage $\overline{v_R^2}$ to keep the motion going \rightarrow and this noise source is associated with R

EE247B/ME218: Introduction to MEMS Design LecM 17 C. Nguyen 11/18/08 15

15

Why 4kTR?

UC Berkeley

- Why is $\overline{v_R^2} = 4kTR\Delta f$ (a heuristic argument)
- The **Equipartition Theorem of Statistical Thermodynamics** says that there is a mean energy $(1/2)kT$ associated w/ each degree of freedom in a given system
- An electronic circuit possesses two degrees of freedom:
 - Current, i , and voltage, v
 - Thus, we can write:

$$\frac{1}{2} Li^2 = \frac{1}{2} k_B T \quad , \quad \frac{1}{2} Cv^2 = \frac{1}{2} k_B T$$
- Similar expressions can be written for mechanical systems
 - For example: for displacement, x

$$\text{Spring constant} \quad \frac{1}{2} kx^2 = \frac{1}{2} k_B T$$

EE247B/ME218: Introduction to MEMS Design LecM 17 C. Nguyen 11/18/08 16

16

Shot Noise

UC Berkeley

- Associated with direct current flow in diodes and bipolar junction transistors
- Arises from the random nature by which e-'s and h+'s surmount the potential barrier at a pn junction
- The DC current in a forward-biased diode is composed of h+'s from the p-region and e-'s from the n-region that have sufficient energy to overcome the potential barrier at the junction
 → noise process should be proportional to DC current

pn-junction

$$\frac{\overline{i_n^2}}{\Delta f} = 2qI_D$$

Charge on an e⁻ (=1.6x10⁻¹⁹C)
 DC Current

- Attributes:**
 - Related to DC current over a barrier
 - Independent of temperature
 - White (i.e., const. w/ frequency)
 - Noise power ~ I_D & bandwidth

EEC247B/MEC218: Introduction to MEMS Design LecM 17 C. Nguyen 11/18/08 19

19

Flicker (1/f) Noise

UC Berkeley

- In general, associated w/ random trapping & release of carriers from "slow" states
- Time constant associated with this process gives rise to a noise signal w/ energy concentrated at low frequencies
- Often, get a mean-square noise spectral density that looks like this:

$$\frac{\overline{i_n^2}}{\Delta f} = 2qI_D + K \left(\frac{I_D^a}{f^b} \right)$$

I_b = DC current
 K = const. for a particular device
 a = 0.5 → 2
 b ~ 1

1/f Noise Corner Frequency

EEC247B/MEC218: Introduction to MEMS Design LecM 17 C. Nguyen 11/18/08 20

20