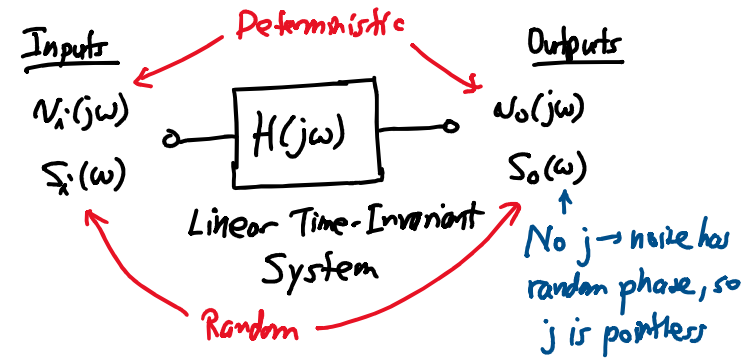


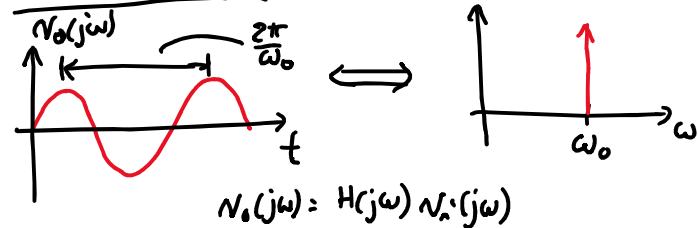
Lecture 24: Noise I

- Announcements:
- Project Slide Set #3 due Friday, April 24
- HW#6 online and due Friday, 5/1, at 8 a.m.
- Module 17 is online (on Noise and MDS)
- -----
- Reading: Senturia Chpt. 16
- Lecture Topics:
 - ↳ Minimum Detectable Signal
 - ↳ Noise
 - Circuit Noise Calculations
 - Noise Sources
 - Equivalent Input-Referred Noise
 - ↳ Gyro MDS
 - Equivalent Noise Circuit
 - Example ARW Determination
- -----
- Last Time:
- Finished MEMS/transistor integration
- Now move on to noise, beginning in Module 17 ...

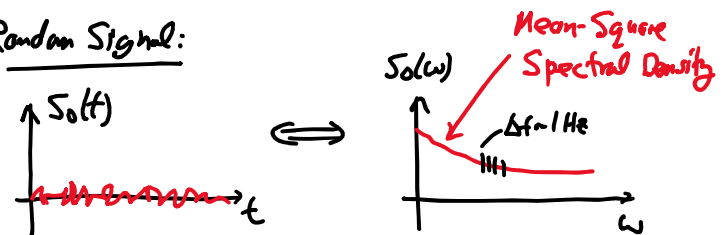
Circuit Noise Calculations



Deterministic Signal:



Random Signal:



$$S_o(\omega) = [H(j\omega)H^*(j\omega)]S_i(\omega) = |H(j\omega)|^2 S_i(\omega)$$

$$\sqrt{S_o(\omega)} = |H(j\omega)|\sqrt{S_i(\omega)} \rightarrow \text{How is it we can do this?}$$

root mean-square values

Handling Noise Quasi-Deterministically

$$\frac{\overline{N_{ni}^2}}{\Delta f} = S_i(f) \rightarrow N_{ni} = \sqrt{S_i(f)B}$$
 bandwidth

Can approximate this by a sinusoidal voltage generator (esp. when B is small, e.g., 1Hz)

Why is this the case?

white noise

Neither the amplitude nor the phase of a signal can change appreciably within a time period $\frac{1}{B}$!

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Noise Source Correlation

Case ①: Single Noise Source

This is correlated w/ this, since it derives from it!

Thus, can write:

$$N_{o1} = H(j\omega)N_{n1}$$

Case ②: Multiple Noise Sources

Can write: $N_{o1} = H_1(j\omega)N_{n1}$
 $N_{o2} = H_2(j\omega)i_{n2}$

But $N_o \neq N_{o1} + N_{o2} \rightarrow$ since these are not correlated

Rather: $\overline{N_o^2} = \overline{N_{o1}^2} + \overline{N_{o2}^2}$ (must add powers!)

4

Systematic Noise Calculation Procedure

General Ckt. w/ Several Noise Sources

Assume noise sources are uncorrelated.

- ① For i_{n1}^2 , replace w/ a source i_{n1}
- ② Calculate $N_{on1}(\omega) = |H_1(j\omega)|^2 i_{n1}^2$
(treating it like a deterministic signal)
- ③ Determine $N_{on1}^2 = |H_1(j\omega)|^2 i_{n1}^2$
- ④ Repeat for each noise source: i_{n4}
get $N_{on2}, N_{on3}, N_{on4}, \dots$ → output
- ⑤ Add noise powers (mean-square values):

$$N_{onTOT}^2 = N_{on1}^2 + N_{on2}^2 + N_{on3}^2 + N_{on4}^2 + \dots$$

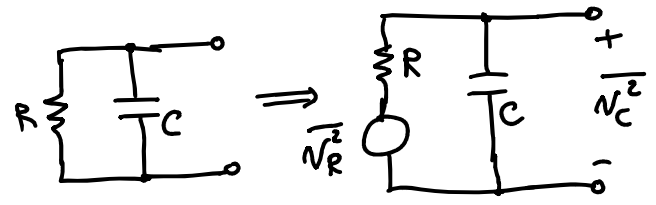
$$N_{onTOT} = \sqrt{N_{on1}^2 + N_{on2}^2 + N_{on3}^2 + N_{on4}^2 + \dots}$$
 ↑
total rms value

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• Go through Module 17, slides 12-16

Why $\frac{N_{NR}^2}{\Delta f} = 4kTR$? (a heuristic argument)

Consider an RC ckt:



$$E = \frac{1}{2}kT = \frac{1}{2}CN_C^2$$

∴ $N_C^2 = \frac{kT}{C}$ ← integrated noise over all freqs. → total mean-square output voltage integrated over all freqs.

Question: What value of $\frac{N_R^2}{\Delta f}$ gives us this (assuming white noise)

$$N_C^2 = \int_0^\infty \left| \frac{1}{1+j\omega RC} \right|^2 \frac{N_R^2}{\Delta f} d\omega$$

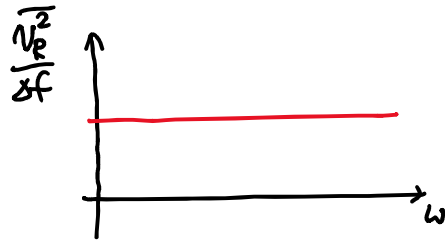
[noise is white] → $= \frac{1}{2\pi} \frac{N_R^2}{\Delta f} \int_0^\infty \frac{\omega_b^2}{\omega_b^2 + \omega^2} d\omega$
 $\omega_b = \frac{1}{RC}$

$\left[\int \frac{dx}{x^2+a^2} = \frac{1}{a} \tan^{-1}\left(\frac{x}{a}\right) \right]$

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$$\begin{aligned} \overline{v_n^2} &= \frac{1}{2\pi} \frac{\overline{N_R^2}}{\Delta f} \frac{\omega_b^2}{\omega_b} \tan^{-1}\left(\frac{\omega}{\omega_b}\right) \Big|_0^\infty \\ &= \frac{1}{2\pi} \frac{\overline{N_R^2}}{\Delta f} \left(\frac{\pi}{2} \omega_b - 0\right) = \frac{1}{4} \omega_b \frac{\overline{N_R^2}}{\Delta f} = \frac{kT}{C} \end{aligned}$$

$\frac{\overline{N_R^2}}{\Delta f} = 4kT \underbrace{\left(\frac{1}{\omega_b C}\right)}_R \Rightarrow \boxed{\frac{\overline{N_R^2}}{\Delta f} = 4kTR} \checkmark$



- Go through Module 17, slides 19-20