

### Flicker (1/f) Noise

- In general, associated w/ random trapping & release of carriers from "slow" states
- Time constant associated with this process gives rise to a noise signal w/ energy concentrated at low frequencies
- Often, get a mean-square noise spectral density that looks like this:

$$\frac{\overline{i_n^2}}{\Delta f} = 2qI_D + K \left( \frac{I_D^a}{f^b} \right)$$

$I_D$  = DC current  
 $K$  = const. for a particular device  
 $a = 0.5 \rightarrow 2$   
 $b \sim 1$

1/f Noise Corner Frequency

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### Example: Typical Noise Numbers

- Hookup the circuit below and make some measurements

$\overline{v_n^2}$      $\overline{v_o^2}$   
 Measure w/ AC voltmeter  
 Measure w/ spectrum analyzer  
 ← Get Gaussian amplitude distribution

$4kTR$      $\frac{N_R^2}{\Delta f}$      $\frac{1}{2\pi RC}$      $\text{area} \sim N_n^2$

Probability    Amplitude  
 68% within  $\pm \sigma$   
 99.7% within  $\pm 3\sigma$

$\sqrt{(1.66 \times 10^{-20})(1k)}$      $1k\Omega: 4nV/\sqrt{Hz}$  (for every 1k of R)  
 $1pF \cdot \sqrt{\frac{kT}{C}} = 64\mu V \text{ rms}$

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### Example: Typical Noise Numbers

- Hookup the circuit below and make some measurements

Measure w/ AC voltmeter  
 Measure w/ spectrum analyzer

**AC Voltmeter**  
 $\sqrt{N_o^2} = (100)(64\mu V \text{ rms}) = 6.4 \text{ mV rms}$

**Spectrum Analyzer**  
 $\frac{1}{(2\pi)(1k)(1p)} = 60 \text{ MHz}$   
 $400 \text{ nV}/\sqrt{Hz}$      $20 \text{ dB/dec}$     one-sided spectral density

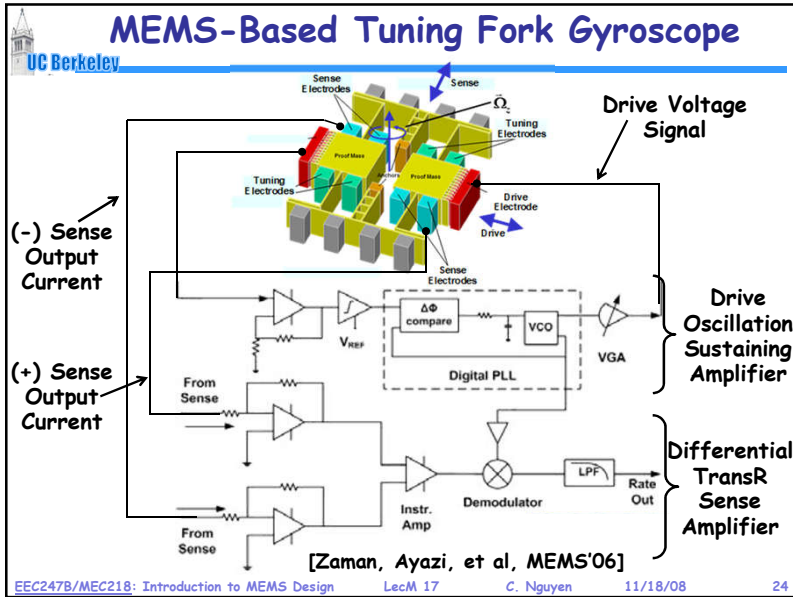
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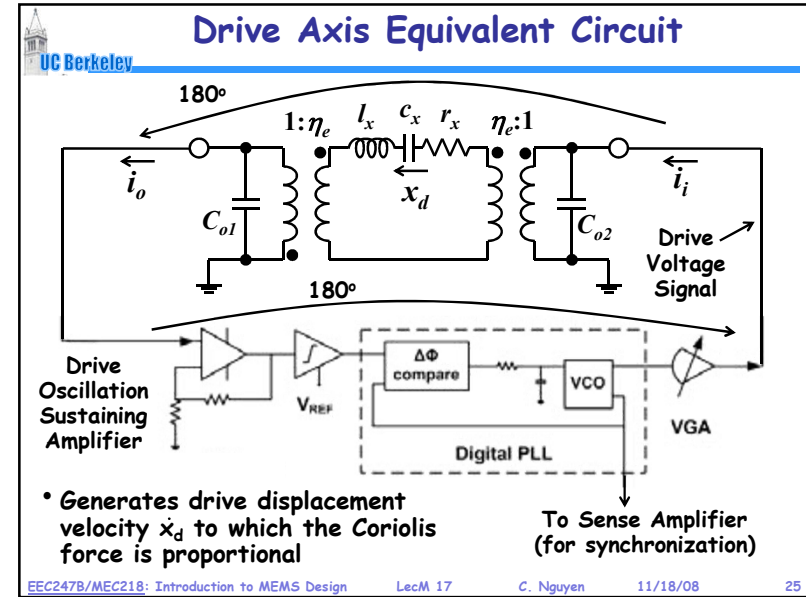
## Back to Determining Sensor Resolution

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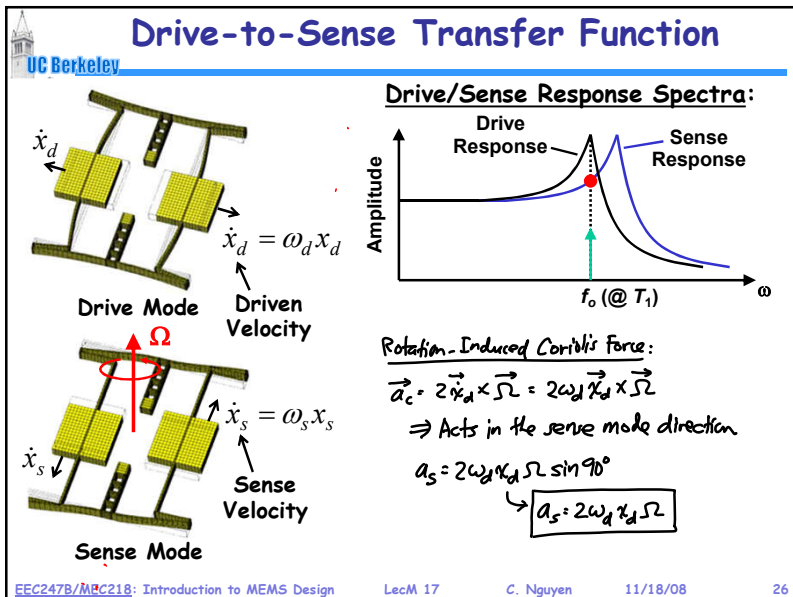
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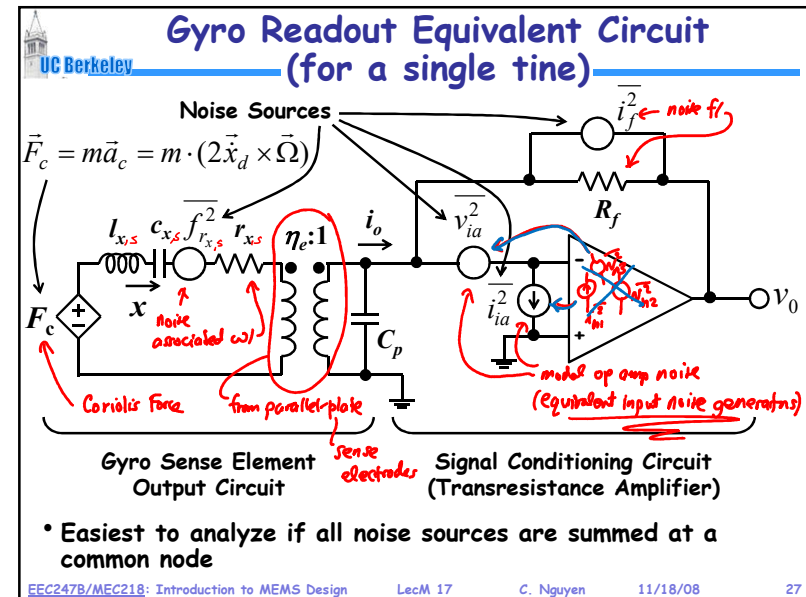
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### Minimum Detectable Signal (MDS)

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- Minimum Detectable Signal (MDS): Input signal level when the signal-to-noise ratio (SNR) is equal to unity

$\Omega$  Sensed Signal

$\Omega_{min} = \frac{N_{on}}{A}$

Scale factor  $A$

$v_o$

$N_{on}^2$

Includes desired output plus noise

Sensor

Signal Conditioning Circuit

- The sensor scale factor is governed by the sensor type
- The effect of noise is best determined via analysis of the equivalent circuit for the system

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### Move Noise Sources to a Common Point

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- Move noise sources so that all sum at the input to the amplifier circuit (i.e., at the output of the sense element)
- Then, can compare the output of the sensed signal directly to the noise at this node to get the MDS

Sensed Signal

Sensor

Signal Conditioning Circuit

Output

Includes desired output plus noise

can do the analysis only up to this node

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### Equivalent Input-Referred Voltage and Current Noise Sources

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### Equivalent Input $v, i$ Noise Generators

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- Take a noisy 2-port network and represent it by a noiseless network with input  $v$  and  $i$  noise generators that generate the same total output noise

Noisy Network

Noiseless

$v_{eq}^2$

$i_{eq}^2$

$4kTR_1$

$4kTR_2$

$N_{i1}^2$

$N_{i2}^2$

- Remarks:
  - Works for linear time-invariant networks
  - $v_{eq}$  and  $i_{eq}$  are generally correlated (since they are derived from the same sources)
  - In many practical circuits, one of  $v_{eq}$  and  $i_{eq}$  dominates, which removes the need to address correlation
  - If correlation is important  $\rightarrow$  easier to return to original network with internal noise sources

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### Calculation of $\overline{v_{eq}^2}$ and $\overline{i_{eq}^2}$

a) To get  $\overline{v_{eq}^2}$  for a two-port:

Case I

Case II

- 1) Short input, find  $\overline{v_{0I}^2}$  (or  $\overline{i_{0I}^2}$ )
- 2) For eq. network, short input, find  $\overline{v_{0II}^2}$  (or  $\overline{i_{0II}^2}$ )

$$\parallel \qquad \parallel$$

$$f(\overline{v_{eq}^2}) \qquad f(\overline{v_{eq}^2})$$

- 3) Set  $\overline{v_{0I}^2} = \overline{v_{0II}^2} \rightarrow$  solve for  $\overline{v_{eq}^2}$  (or  $\overline{i_{0I}^2} = \overline{i_{0II}^2}$ )

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### Calculation of $\overline{v_{eq}^2}$ and $\overline{i_{eq}^2}$ (cont)

b) To get  $\overline{i_{eq}^2}$  for a 2-port:

- 1) Open input, find  $\overline{v_{0I}^2}$  (or  $\overline{i_{0I}^2}$ )
- 2) Open input for eq. circuit, find  $\overline{v_{0II}^2}$  (or  $\overline{i_{0II}^2}$ )
- 3) Set  $\overline{v_{0I}^2} = \overline{v_{0II}^2} \rightarrow$  solve for  $\overline{i_{eq}^2}$  (or  $\overline{i_{0I}^2} = \overline{i_{0II}^2}$ )

• Once the equivalent input-referred noise generators are found, noise calculations become straightforward as long as the noise generators can be treated as uncorrelated

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### Cases Where Correlation Is Not Important

- There are two common cases where correlation can be ignored:
  1. Source resistance  $R_s$  is **small** compared to input resistance  $R_i \rightarrow$  i.e., voltage source input
  2. Source resistance  $R_s$  is **large** compared to input resistance  $R_i \rightarrow$  i.e., current source input

1)  $R_s = \text{small}$  (ideally = 0 for an ideal voltage source):

$\overline{i_{eq}^2}$  Current shorted out!

$\therefore$  For  $R_s = \text{small}$ ,  $\overline{i_{eq}^2}$  can be neglected  $\rightarrow$  only  $\overline{v_{eq}^2}$  is important!  
(Thus, we need not deal with correlation)

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### Cases Where Correlation Is Not Important

2)  $R_s = \text{large}$  (Ideally =  $\infty$  for an ideal current source)

Voltage  $\overline{v_{eq}^2}$  effectively "opened" out!

$v_i = \frac{R_{in}}{\infty + R_{in}} v_{eq} = 0!$

$\therefore$  For  $R_s = \text{large}$ ,  $\overline{v_{eq}^2}$  can be neglected!  
 $\rightarrow$  only  $\overline{i_{eq}^2}$  is important!  
(... and again, we need not deal with correlation)

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