EE C247B – ME C218
Introduction to MEMS Design
Spring 2020

Prof. Clark T.-C. Nguyen

Dept. of Electrical Engineering & Computer Sciences
University of California at Berkeley
Berkeley, CA 94720

Lecture Module 13: Equivalent Circuits II

Lecture Outline

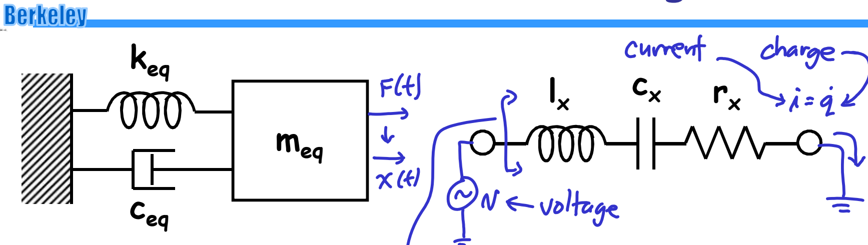
- Reading: Senturia, Chpt. 6, Chpt. 14
- Lecture Topics:
  - Input Modeling
    - Force-to-Velocity Equiv. Ckt.
    - Input Equivalent Ckt.
  - Current Modeling
    - Output Current Into Ground
    - Input Current
    - Complete Electrical-Port Equiv. Ckt.
  - Impedance & Transfer Functions

UC Berkeley

Input Modeling

UC Berkeley

Electromechanical Analogies



$F(t) = F\cos(\omega t) \rightarrow x(t) = X\cos\omega t$

Equation of Motion:

$m_{eq}\ddot{x} + c_{eq}\dot{x} + k_{eq}x = F(t)$

⇒ using phasor concepts:

$F = j\omega m_{eq}\dot{x} + \frac{k_{eq}}{j\omega}\dot{x} + c_{eq}\dot{x}$

$v(t) = V\cos\omega t \rightarrow i(t) = I\cos\omega t$

Impedance looking in:

$\frac{v}{i} = j\omega l_x + \frac{1}{j\omega c_x} + r_x$

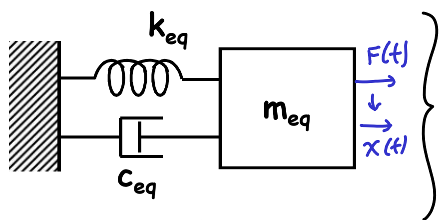
$v = j\omega l_x i + \frac{(1/c_x)}{j\omega} i + r_x i$

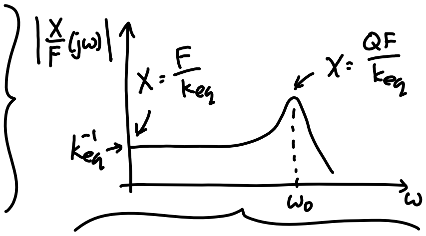
⇒ by analogy:

$$\boxed{\begin{array}{lll} F \rightarrow v & m_{eq} \rightarrow l_x & c_{eq} \rightarrow r_x \\ \dot{x} \rightarrow i & k_{eq} \rightarrow \frac{1}{c_x} & \end{array}}$$

[Parameter Relationships in the Current Analogy]

Bandpass Biquad Transfer Function





$$\frac{X}{F}(j\omega) = \boxed{\frac{k_{eq}^{-1}}{1-\left(\frac{\omega}{\omega_o}\right)^2 + j\frac{\omega}{Q\omega_o}}}$$

$$F = j\omega m_{eq}\dot{x} + \frac{k_{eq}}{j\omega}\dot{x} + c_{eq}\dot{x}$$

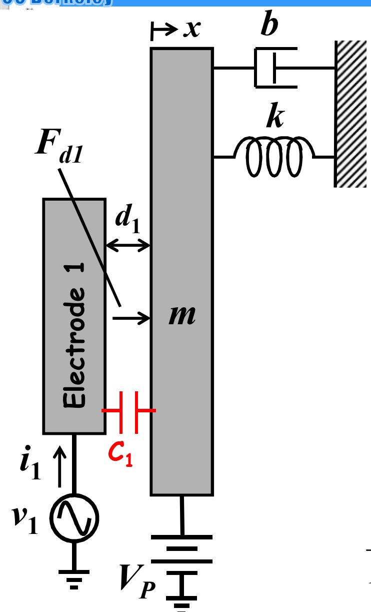
⇒ converting to full phasor form:

$$F = (j\omega)(j\omega X)m_{eq} + \frac{k_{eq}}{\cancel{j\omega}}(\cancel{j\omega}X) + c_{eq}(j\omega X)$$

$$\frac{X}{F}(j\omega) = \frac{1}{k_{eq}}\left[-\omega^2\frac{m_{eq}}{k_{eq}} + 1 + j\frac{c_{eq}\omega}{k_{eq}}\right]^{-1} = \frac{1}{k_{eq}}\left[-\left(\frac{\omega}{\omega_o}\right)^2 + 1 + j\frac{\omega}{Q\omega_o}\right]^{-1}$$

$$\left[\frac{k_{eq}}{m_{eq}} = \omega_o^2,\ Q = \frac{m_{eq}\omega_o}{c_{eq}} = \frac{k_{eq}}{\omega_o c_{eq}} \rightarrow \frac{k_{eq}}{c_{eq}} = Q\omega_o\right]$$

Force-to-Velocity Relationship



- The relationship between input voltage v_1 and force F_{d1}:

$$F_{d1} \approx -V_P \frac{\partial C_1}{\partial x} v_1$$

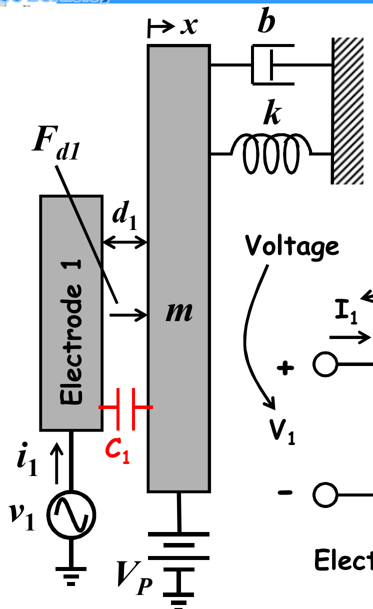
- When displacement x is the mechanical output variable:

$$\frac{X(s)}{F_{d1}(s)} = \frac{1}{k}\frac{\omega_o^2}{s^2 + (\omega_o/Q)s + \omega_o^2}$$

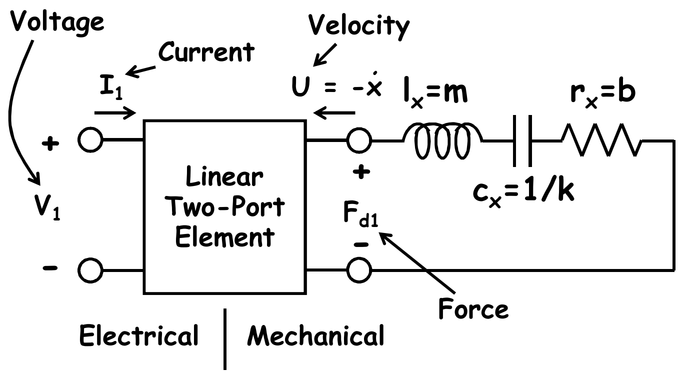
- When velocity υ is the mechanical output variable:

$$\frac{\upsilon(s)}{F_{d1}(s)} = \frac{sX(s)}{F_{d1}(s)} = \frac{1}{k}\frac{\omega_o^2 s}{s^2 + (\omega_o/Q)s + \omega_o^2}$$

Force-to-Velocity Equiv. Ckt.



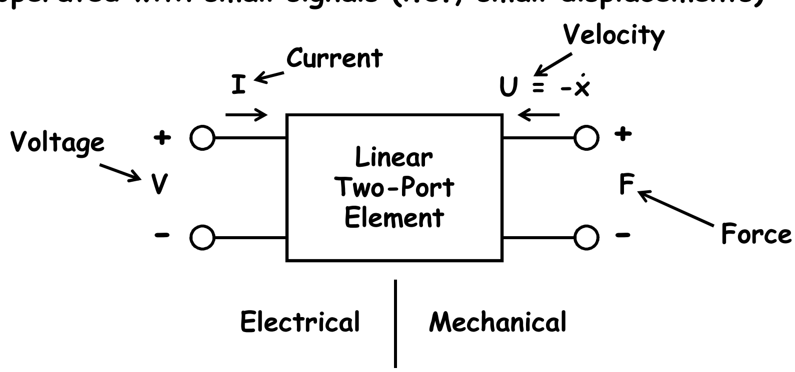
- Combine the previous lumped LCR mechanical equivalent circuit with a circuit modeling the capacitive transducer → circuit model for voltage-to-velocity



7

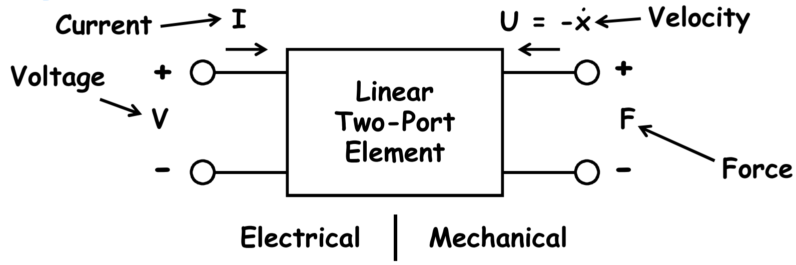
Equiv. Circuit for a Linear Transducer

- A transducer …
  - converts energy from one domain (e.g., electrical) to another (e.g., mechanical)
  - has at least two ports
  - is not generally linear, but is virtually linear when operated with small signals (i.e., small displacements)

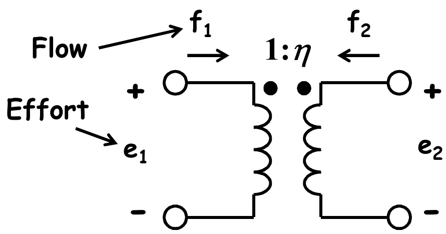


8

Equiv. Circuit for a Linear Transducer



- For physical consistency, use a transformer equivalent circuit to model the energy conversion from the electrical domain to mechanical domain



$$\begin{bmatrix} e_2 \\ f_2 \end{bmatrix} = \begin{bmatrix} \eta & 0 \\ 0 & -\dfrac{1}{\eta} \end{bmatrix} \begin{bmatrix} e_1 \\ f_1 \end{bmatrix}$$

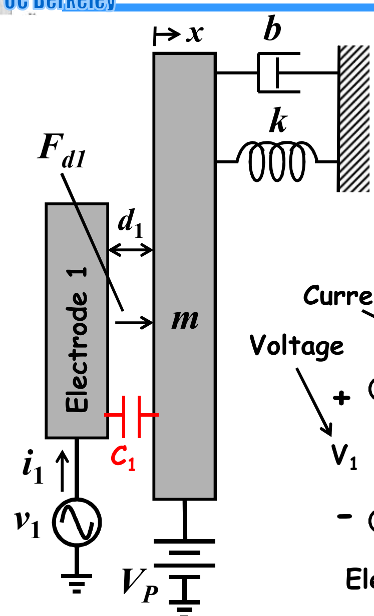
Describing Matrix

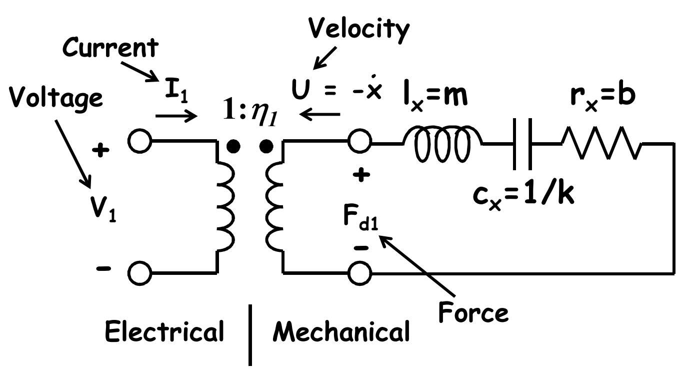
9

Electromechanical Equivalent Circuit

- $e_2=F_{d1}$, $e_1=v_1$, just need η_1:
- From the matrix: $e_2=\eta e_1$

$$F_{d1} \approx -V_P \frac{\partial C_1}{\partial x} v_1 \longrightarrow \boxed{\eta_1 = \left| V_P \frac{\partial C_1}{\partial x} \right|}$$





10

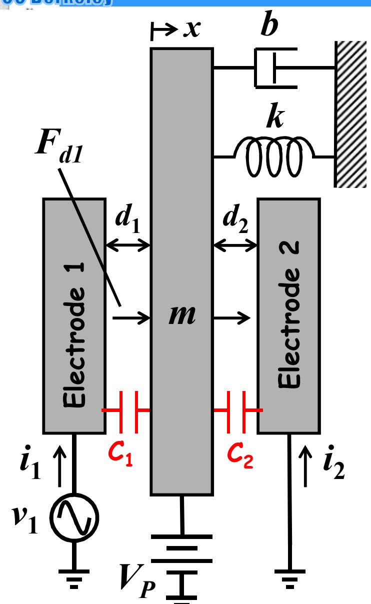
UC Berkeley

Output Modeling

11

UC Berkeley

Output Current Into Ground



- When the mass moves with time-dependent displacement x(t), the electrode-to-mass capacitors C_1(x,t) and C_2(x,t) vary with time
- This generates an output current:

$$[q = CV] \Rightarrow i = \frac{dq}{dt} = C\frac{\partial V}{\partial t} + V\frac{\partial C}{\partial t}$$

$$i_2(t) = C_2(x,t)\frac{dV_2(t)}{dt} + V_2(t)\frac{dC_2(x,t)}{dt}$$

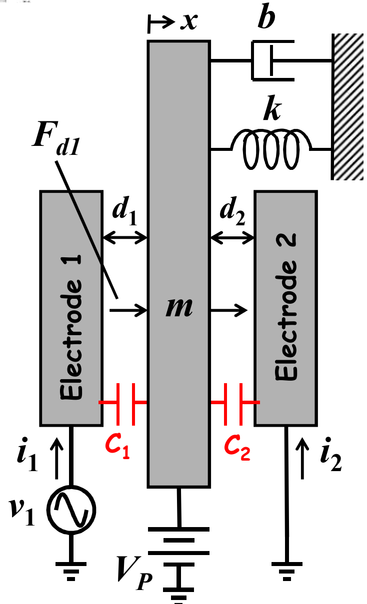
$$[V_2(t) = -V_P] \Rightarrow i_2 = -V_P\frac{dC_2}{dt} = -V_P\frac{\partial C_2}{\partial x}\frac{\partial x}{\partial t}$$

In phasor form: $I_2(j\omega) = -V_P\frac{\partial C_2}{\partial x}(j\omega X)$

$$\boxed{I_2(j\omega) = -j\omega V_P\frac{\partial C_2}{\partial x}X}$$

12

Output Current Into Ground

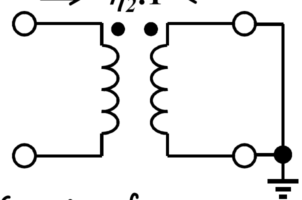


$I_2(j\omega) = -j\omega V_P \frac{\partial C_2}{\partial x} X = -V_P \frac{\partial C}{\partial x} U$

90° phase lag (+) (+) → $I_2 = (-)$ when $x = (+)$ ✓

- Again, model with a transformer:

Velocity → $U = \dot{x}$ $\eta_2 : 1$ I_2 ← Current



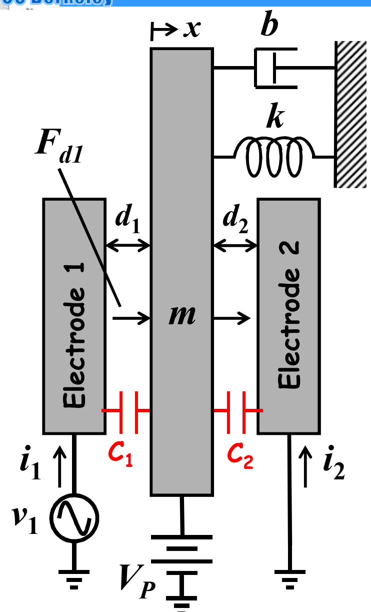
$f_2 = -\frac{1}{\eta_2} f_1 \rightarrow f_1 = -\eta_2 f_2$

$[f_1 = I_2,\ f_2 = U] \Rightarrow I_2 = -\eta_2 U$

$\therefore \boxed{\eta_2 = \left|V_P \frac{\partial C}{\partial x}\right|}$

13

Input Current Expression



Get $I_1(j\omega)$:

$i_1(t) = C_1(x,t)\frac{dV_1(t)}{dt} + V_1(t)\frac{dC_1(x,t)}{dt}$

$[V_1(t) = v_1 - V_P] \Rightarrow i_1 = C_1 \frac{dv_1}{dt} + [v_1 - V_P]\frac{\partial C_1}{\partial x}\frac{\partial x}{\partial t}$

$\therefore I_1(j\omega) = C_1(j\omega V_1) + V_1 \frac{\partial C_1}{\partial x}(j\omega X) - V_P\frac{\partial C_1}{\partial x}(j\omega X)$

$= j\omega C_1 V_1 + j\omega V_1 \frac{\partial C_1}{\partial x}X - j\omega V_P \frac{\partial C_1}{\partial x}X$

$[V_1 \ll V_P] \Rightarrow I_1(j\omega) = \underbrace{j\omega C_1 V_1}_{\text{Feedthrough Current}} - \underbrace{j\omega V_P \frac{\partial C_1}{\partial x} X}_{\text{Motional Current}}$ (due to mass motion)

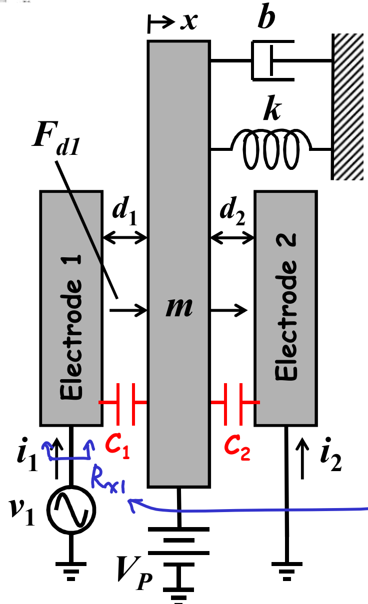
@ DC: $x = \frac{F_{d1}}{k} = -\frac{1}{k} V_P \left(\frac{\partial C_1}{\partial x}\right) v_1$

@ resonance: $x = \frac{Q F_{d1}}{jk} = \frac{-Q}{jk} V_P \frac{\partial C_1}{\partial x} v_1$

90° phase lag

14

Input Current Expression (cont)



Thus: (@ resonance)

$I_1(j\omega) = j\omega_o C_1 V_1 + j\omega_o \left(V_P \frac{\partial C_1}{\partial x}\right)^2 \frac{Q}{jk} V_1$

$= j\omega_o C_1 V_1 + \omega_o \frac{Q}{k} \eta_1^2 V_1$

90° phase-shifted from V_1 → This is a Capacitor in shunt w/ the input.

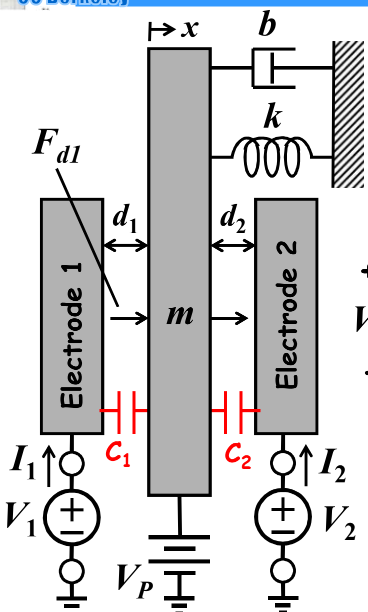
In phase w/ V_1 → This is an effective resistance seen looking into Electrode 1

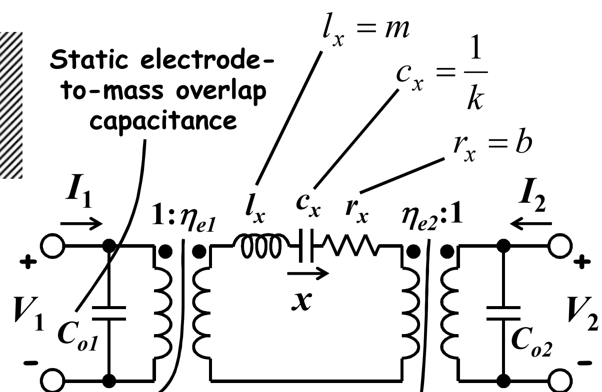
Motional Resistance:

$R_{x1} = \frac{V_1}{I_1} = \frac{k}{\omega_o Q \eta_1^2} = \frac{m\omega_o}{Q\eta_1^2} = \boxed{\frac{b}{\eta_1^2} = R_{x1}}$

(The equivalent ckt. better get this right!)

Complete Electrical-Port Equiv. Circuit

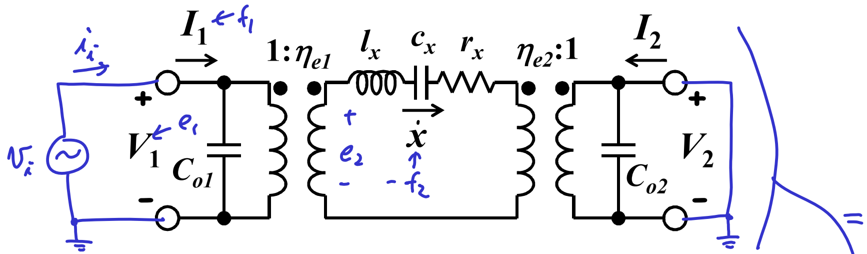




$\eta_{e1} = V_P \frac{\partial C_1}{\partial x} = V_P \frac{C_{o1}}{d_1}$

$\eta_{e2} = V_P \frac{\partial C_2}{\partial x} = V_P \frac{C_{o2}}{d_2}$

Input Impedance Into Port 1

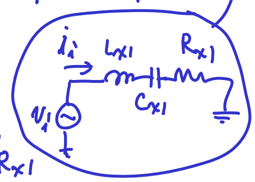


- What is the impedance seen looking into port 1 with port 2 shorted to ground?

From our transformer model: $\begin{bmatrix} e_2 \\ f_2 \end{bmatrix} = \begin{bmatrix} \eta & 0 \\ 0 & -\frac{1}{\eta} \end{bmatrix}\begin{bmatrix} e_1 \\ f_1 \end{bmatrix} \Rightarrow$ $e_2 = \eta e_1 \rightarrow e_1 = \frac{e_2}{\eta}$, $f_2 = -\frac{1}{\eta} f_1 \rightarrow f_1 = -\eta f_2$

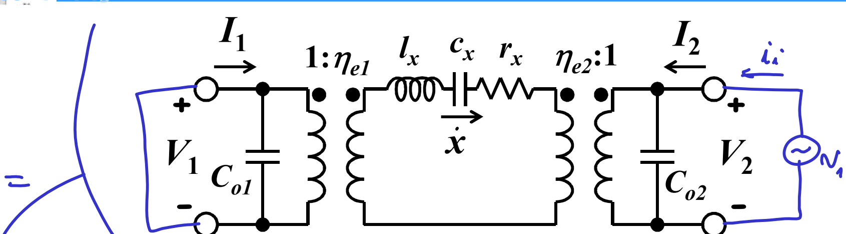
$$\frac{e_1}{f_1} = \frac{e_2}{\eta}\left(\frac{1}{-\eta f_2}\right) = -\frac{1}{\eta^2}\frac{e_2}{f_2} \longrightarrow \frac{v_i}{i_i} = z_i = -\frac{1}{\eta_{e1}^2}\frac{F_2}{(-\dot{x}_2)} = \frac{1}{\eta_{e1}^2} z_x$$

$$z_i = \frac{1}{\eta_{e1}^2}\left(j\omega l_x + \frac{1}{j\omega c_x} + r_x\right) = j\omega\underbrace{\left(\frac{l_x}{\eta_{e1}^2}\right)}_{L_{x1}} + \frac{1}{j\omega\underbrace{(\eta_{e1}^2 c_x)}_{C_{x1}}} + \underbrace{\frac{r_x}{\eta_{e1}^2}}_{R_{x1}}$$



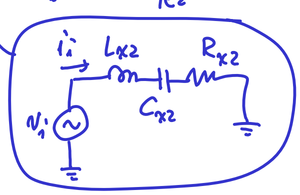
17

Input Impedance Into Port 2



- What is the impedance seen looking into port 2 with port 1 shorted to ground?

$$\frac{v_i}{i_i} = Z_i = \frac{1}{\eta_{e2}^2}\left(j\omega l_x + \frac{1}{j\omega c_x} + r_x\right) = j\omega\underbrace{\left(\frac{l_x}{\eta_{e2}^2}\right)}_{L_{x2}} + \frac{1}{j\omega\underbrace{(\eta_{e2}^2 c_x)}_{C_{x2}}} + \underbrace{\frac{r_x}{\eta_{e2}^2}}_{R_{x2}}$$

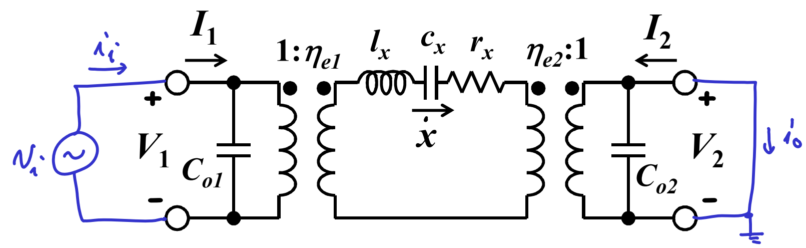


Note: These are not the same as L_{x1}, C_{x1}, & R_{x1}!

18

Port 1 to 2 TransG Across the Circuit

UC Berkeley



- What is the transconductance from port 1 to port 2 with port 2 shorted to ground? $\frac{i_o}{v_i}(j\omega)$

$\dot{x} = \frac{1}{\eta_{e1}} i_i$

$i_o = \eta_{e2}\dot{x}$

$$i_o = \frac{\eta_{e2}}{\eta_{e1}} i_i = \frac{\eta_{e2}}{\eta_{e1}}\left(\frac{v_i}{Z_i}\right) = \frac{\eta_{e2}}{\eta_{e1}} v_i \left[\eta_{e1}^2 \frac{1}{j\omega l_x + \frac{1}{j\omega c_x} + r_x}\right]$$

$$\therefore \frac{i_o}{v_i}(j\omega) = \frac{\eta_{e1}\eta_{e2}}{j\omega l_x + \frac{1}{j\omega c_x} + r_x} = \left[j\omega L_{x12} + \frac{1}{j\omega C_{x12}} + R_{x12}\right]^{-1} \quad \begin{cases} L_{x12} = \frac{l_x}{\eta_{e1}\eta_{e2}} \\ C_{x12} = \eta_{e1}\eta_{e2} c_x \\ R_{x12} = \frac{r_x}{\eta_{e1}\eta_{e2}} \end{cases}$$

Port 1 to 2 v_i-to-i_o Transfer Function

UC Berkeley

$$\frac{i_o}{v_i}(j\omega) = \frac{\eta_{e1}\eta_{e2}}{j\omega l_x + \frac{1}{j\omega c_x} + r_x} = \left[j\omega L_{x12} + \frac{1}{j\omega C_{x12}} + R_{x12}\right]^{-1} \quad \begin{cases} L_{x12} = \frac{l_x}{\eta_{e1}\eta_{e2}} \\ C_{x12} = \eta_{e1}\eta_{e2} c_x \\ R_{x12} = \frac{r_x}{\eta_{e1}\eta_{e2}} \end{cases}$$

Separate freq. response & magnitude:

$$\frac{i_o}{v_i}(s) = \frac{1}{sL_x + \frac{1}{sC_x} + R_x} = \frac{sC_x}{s^2L_xC_x + 1 + sC_xR_x} = \frac{s\left(\frac{1}{L_x}\right)}{s^2 + \frac{1}{L_xC_x} + s\left(\frac{R_x}{L_x}\right)}$$

$$\left[\frac{1}{L_xC_x} = \omega_o^2,\ Q = \frac{\omega_o L_x}{R_x} \rightarrow \frac{R_x}{L_x} = \frac{\omega_o}{Q}\right] \Rightarrow \boxed{\frac{i_o}{v_i}(s) = \underbrace{\frac{1}{R_x}}_{\text{Gain Term}} \underbrace{\frac{s(\omega_o/Q)}{s^2 + s(\omega_o/Q) + \omega_o^2}}_{\text{Bandpass Biquad}} = \frac{1}{R_x} H(s)}$$

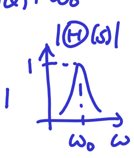
This will always be the same. Thus, could just work @ resonance & just multiply by $H(s)$.

$$H(s) = \frac{s(\omega_o/Q)}{s^2 + s(\omega_o/Q) + \omega_o^2}$$

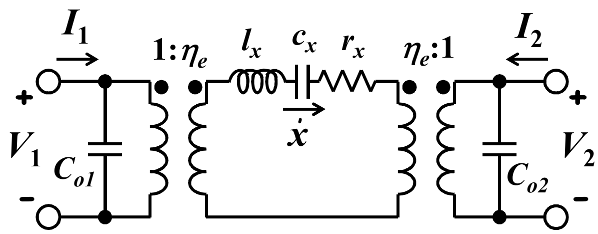
$s=0$: $H(0) = 0$

$s=j\omega_o$: $H(j\omega_o) = 1$

$s=\infty$: $H(\infty) = 0$

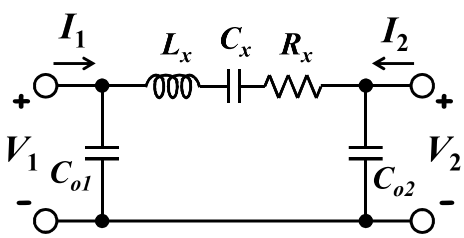


Condensed Equiv. Circuit (Symmetrical)



Holds for the symmetrical case, where port 1 and port 2 are identical

If $\eta_{e1} = \eta_{e2}$, then …



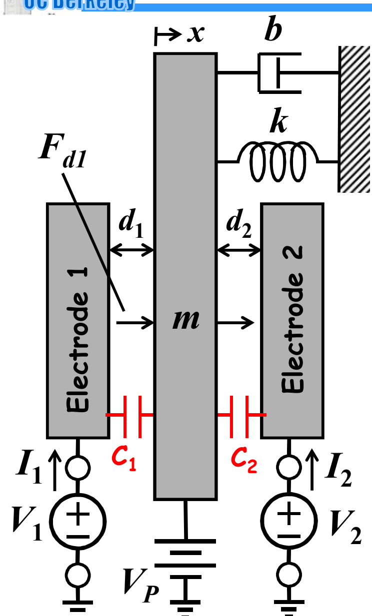
where

$$L_x = \frac{m}{\eta_e^2}, \quad C_x = \frac{\eta_e^2}{k}, \quad R_x = \frac{b}{\eta_e^2}$$

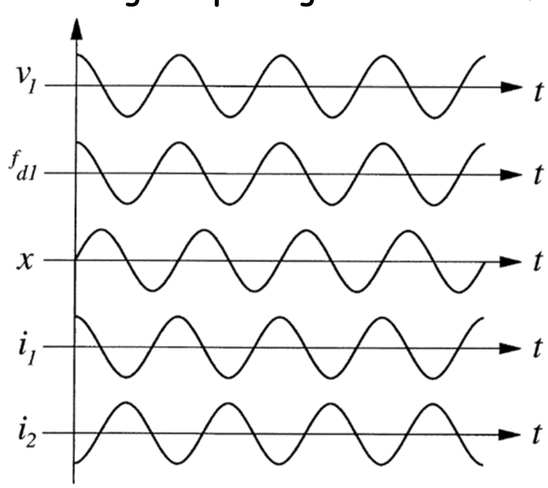
EE C245: Introduction to MEMS Design LecM 13 C. Nguyen 11/18/08 21

21

Phasings of Signals



- Below: plots of resonance electrical and mechanical signals vs. time, showing the phasings between them



EE C245: Introduction to MEMS Design LecM 13 C. Nguyen 11/18/08 22

22