

### Lecture Outline

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- Reading: Senturia Chpt. 3, Jaeger Chpt. 11, Handout: "Surface Micromachining for Microelectromechanical Systems"
- Lecture Topics:
  - ↳ Polysilicon surface micromachining
  - ↳ Stiction
  - ↳ Residual stress
  - ↳ Topography issues
  - ↳ Nickel metal surface micromachining
  - ↳ 3D "pop-up" MEMS
  - ↳ Foundry MEMS: the "MUMPS" process
  - ↳ The Sandia SUMMIT process

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### Microstructure Stiction

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Wetted Area  $A$   
Force Applied to Maintain Equilibrium  $F$   
Microstructures  
Contact Angle  $\theta_c$   
Liquid Layer Thickness  $g$

- Thin liquid layer between two solid plates  $\Rightarrow$  adhesive
- If the contact angle between liquid and solid  $\theta_c < 90^\circ$ :
  - ↳ Pressure inside the liquid is lower than outside
  - ↳ Net attractive force between the plates
- The pressure difference (i.e., force) is given by the Laplace equation

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### Microstructure Stiction Modeling

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Wetted Area  $A$   
Force Applied to Maintain Equilibrium  $F$   
Microstructures  
Contact Angle  $\theta_c$   
Liquid Layer Thickness  $g$

Laplace Equation: Surface Tension @ the Liq-Air Interface  $\gamma_{la}$   
 $\Delta p_{la} = \frac{\gamma_{la}}{r}$   $\leftarrow$  Radius of Curvature of the Meniscus (-) if concave  
 Pressure Difference @ the Liquid-Air Interface

$[r = -\frac{(g/2)}{\cos\theta_c}] \Rightarrow F = -\Delta p_{la} A = \frac{2A\gamma_{la}\cos\theta_c}{g}$

Force needed to keep the plates apart  $\Rightarrow$  (+) force means  $g$  (-) Laplace pressure

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### Avoiding Stiction

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- Reduce droplet area via mechanical design approaches

Standoff Bumps      Meniscus-Shaping Features

- Avoid liquid-vapor meniscus formation
  - ↳ Use solvents that sublime
  - ↳ Use vapor-phase sacrificial layer etch
- Modify surfaces to change the meniscus shape from concave (small contact angle) to convex (large contact angle)
  - ↳ Use teflon-like films
  - ↳ Use hydrophobic self-assembled monolayers (SAMs)

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### UC Berkeley Supercritical CO<sub>2</sub> Drying

- A method for stictionless drying of released microstructures by immersing them in CO<sub>2</sub> at its supercritical point
- Basic Strategy:** Eliminate surface tension-derived sticking by avoiding a liquid-vapor meniscus
- Procedure:**
  - Etch oxide in solution of HF
  - Rinse thoroughly in DI water, but do not dry
  - Transfer the wafer from water to methanol
  - Displace methanol w/ liquid CO<sub>2</sub>
  - Apply heat & pressure to take the CO<sub>2</sub> past its critical pt.
  - Vent to lower pressure and allow the supercritical CO<sub>2</sub> to revert to gas → liquid-to-gas Xsition in supercritical region means no capillary forces to cause stiction

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### UC Berkeley Hydrophilic Versus Hydrophobic

**contact angle**

Lotus Surface [Univ. Mainz]

- Hydrophilic:**
  - A surface that invites wetting by water
  - Get stiction
  - Occurs when the contact angle  $\theta_{\text{water}} < 90^\circ$
- Hydrophobic:**
  - A surface that repels wetting by water
  - Avoids stiction
  - Occurs when the contact angle  $\theta_{\text{water}} > 90^\circ$

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### UC Berkeley Tailoring Contact Angle Via SAM's

- Can reduce stiction by tailoring surfaces so that they induce a water contact angle  $> 90^\circ$

**Self-Assembled Monolayers (SAM's):**

- Monolayers of "stringy" molecules covalently bonded to the surface that then raise the contact angle
- Beneficial characteristics:**
  - Conformal, ultrathin
  - Low surface energy
  - Covalent bonding makes them wear resistant
  - Thermally stable (to a point)

OTS  
CH3(CH2)17SiCl3

	$\theta_{\text{water}}$
ODT SAM	$112 \pm 0.7^\circ$
SiO <sub>2</sub>	$< 10^\circ$

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### UC Berkeley Dry Release

- Another way to avoid stiction is to use a dry sacrificial layer etch
- For an oxide sacrificial layer use HF vapor phase etching
  - Additional advantage:** gas can more easily get into tiny gaps
  - Issue:** not always completely dry → moisture can still condense → stiction → **soln:** add alcohol
- For a polymer sacrificial layer
  - Use an O<sub>2</sub> plasma etch (isotropic, so it can undercut well)
  - Issues:**
    - Cannot be used when structural material requires high temperature for deposition
    - If all the polymer is not removed, polymer under the suspended structure can still promote stiction

Released via vapor phase HF [Kenny, et al., Stanford]

[Kobayashi]

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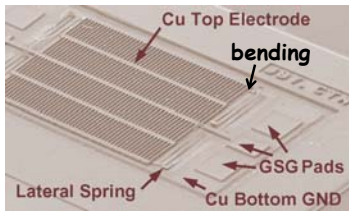
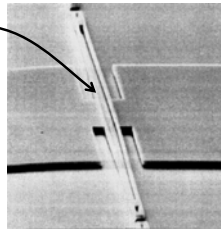
## Residual Stress

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## Residual Stress in Thin Films

- After release, poorly designed microstructures might buckle, bend, or warp → often caused by residual film stress
- Origins of residual stress,  $\sigma$ 
  - ↳ Growth processes
    - Non-equilibrium deposition
    - Grain morphology change
    - Gas entrapment
    - Doping
  - ↳ Thermal stresses
    - Thermal expansion mismatch of materials → introduce stress during cool-down after deposition
    - Annealing

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## Need to Control Film Stress

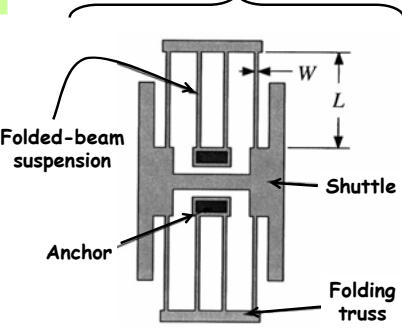
• Resonance frequency expression for a lateral resonator:

$$f_0 \approx \frac{1}{2\pi} \sqrt{\frac{4E_y t W^3}{ML^3} + \frac{24\sigma_r t W}{5ML}}$$

Since  $W \ll L$ , the stress term will dominate if  $\sigma_r \sim E_y$

Basic term:  $\frac{4E_y t W^3}{ML^3}$   
Stress term:  $\frac{24\sigma_r t W}{5ML}$

$E_y$  = Young's modulus  
 $\sigma_r$  = stress  
 $t$  = thickness  
 $W$  = beam width  
 $L$  = beam length  
 $M$  = mass


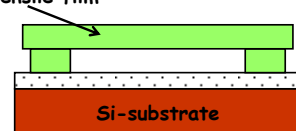
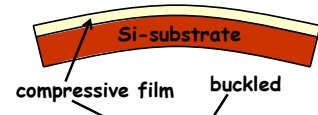
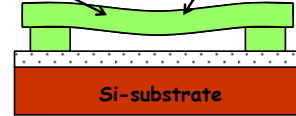


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## Tensile Versus Compressive Stress

- Under tensile stress, a film wants to shrink w/r to its substrate
  - ↳ Caused, e.g., by differences in film vs. substrate thermal expansion coefficients
  - ↳ If suspended above a substrate and anchored to it at two points, the film will be "stretched" by the substrate
- Under compressive stress, a film wants to expand w/r to its substrate
  - ↳ If suspended above a substrate and anchored to it at two points, the film will buckle over the substrate

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### Vertical Stress Gradients

- Variation of residual stress in the direction of film growth
- Can warp released structures in z-direction

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### Stress in Polysilicon Films

- Stress depends on crystal structure, which in turn depends upon the deposition temperature
- Temperature  $\leq 600^\circ\text{C}$ 
  - Films are initially amorphous, then crystallize
  - Get equiaxed crystals, largely isotropic
  - Crystals have higher density  $\rightarrow$  tensile stress
  - Small stress gradient
- Temperature  $\geq 600^\circ\text{C}$ 
  - Columnar crystals grow during deposition
  - As crystals grow vertically and in-plane they push on neighbors  $\rightarrow$  compressive stress
  - Positive stress gradient

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### Annealing Out Polysilicon Stress

- Control polySi stress by annealing at high temperatures
  - Typical anneal temperatures:  $900\text{--}1150^\circ\text{C}$
  - Grain boundaries move, relax
  - Can dope while annealing by sandwiching the polysilicon between similarly doped oxides (symmetric dopant drive-in), e.g. using 10-15 wt. % PSG

- Rapid thermal anneal (RTA) also effective (surprisingly)

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### Topography Issues

- Degradation of lithographic resolution
  - PR step coverage, streaking
  - Thickness differences pose problems for reduction steppers
- Stringers
  - Problematic when using anisotropic etching, e.g., RIE

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## Nickel Surface-Micromachining Process Flow

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## Electroplating: Metal MEMS

- Use electroplating to obtain metal structures
- When thick: call it "LIGA"
- Pros:** fast low temp deposition, very conductive
- Cons:** drift, low mech. Q but may be solvable?

RF Switch

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## Nickel Metal Surface-Micromachining

- Deposit isolation LTO:
  - Target = 2 $\mu$ m
  - 1 hr. 40 min. LPCVD @450°C
- Densify the LTO
  - Anneal @950°C for 30 min.
- Define metal interconnect via lift-off
  - Spin photoresist and pattern lithographically to open areas where interconnect will stay
  - Evaporate a Ti/Au layer
    - Target = 30nm Ti
    - Target = 270nm Au
  - Remove photoresist in PRS2000  $\rightarrow$  Ti/Au atop the photoresist also removed

*Handwritten notes:* "expand" with arrow pointing to the photoresist layer; "thin cross-section better for lift-off!" with arrow pointing to the Ti/Au layer.

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## Nickel Metal Surface-Micromachining

- Evaporate Al to serve as a sacrificial layer
  - Target = 1 $\mu$ m
- Lithography to define anchor openings
- Wet etch the aluminum to form anchor vias
  - Use solution of  $H_3PO_4/HNO_3/H_2O$
- Remove photoresist in PRS2000
  - Handwritten note: "corner" with arrow pointing to a corner of the photoresist.
- Electroplate nickel to fill the anchor vias
  - Use solution of nickel sulfamate @ 50°C
  - Time the electroplating to planarize the surface

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### Nickel Metal Surface-Micromachining

- Evaporate a thin film of nickel to serve as a seed layer for subsequent Ni electroplating
  - ↳ Target = 20nm
- Form a photoresist mold for subsequent electroplating
  - ↳ Spin 6  $\mu\text{m}$ -thick AZ 9260 photoresist
  - ↳ Lithographically pattern the photoresist to delineate areas where nickel structures are to be formed
- Electroplate nickel structural material through the PR mold
  - ↳ Use a solution of nickel sulfamate @ 50°C
  - ↳ Cathode-to-anode current density  $\sim 2.5 \text{ mA/cm}^2$

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### Nickel Metal Surface-Micromachining

- Strip the PR in PRS2000
- Remove the Ni seed layer in Ni wet etchant
- Release the structures
  - ↳ Use a  $\text{K}_4\text{Fe}(\text{CN})_6/\text{NaOH}$  etchant that attacks Al while leaving Ni and Au intact
  - ↳ Etch selectivity  $> 100:1$  for Al:Ni and Al:Au

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### Nickel Surface-Micromachining Example

• Below: Surface-micromachined in nickel using the described process flow

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### 3D "Pop-up" MEMS

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### Pop-Up MEMS

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5µm

plate

staple

pin

First MEMS hinge  
[K. Pister, et al., 1992]

Corner Cube Reflector  
[v. Hsu, 1999]

8011 20KV X6,000 1µm WD25

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### Pop-Up MEMS

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- Pictured: hinged Campanile made in SUMMiT process, assembled using probes [Elliot Hui, et al.]

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### 3D Direct-Assembled Tunable L

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[Ming Wu, UCLA]

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### Hinge Process Flow

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Deposit first sacrificial

Deposit and pattern first poly

Deposit and pattern second sacrificial

Pattern contacts

Deposit and pattern second poly

Etch sacrificial

Assemble part

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