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EE C245 - ME C218 Introduction to MEMS Design Fall 2010

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Lecture Module 3: Oxidation & Film Deposition

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Lecture Outline

- Reading: Senturia, Chpt. 3; Jaeger, Chpt. 2, 3, 6
 - ↳ Example MEMS fabrication processes
 - ↳ Oxidation
 - ↳ Film Deposition
 - Evaporation
 - Sputter deposition
 - Chemical vapor deposition (CVD)
 - Plasma enhanced chemical vapor deposition (PECVD)
 - Epitaxy
 - Atomic layer deposition (ALD)
 - Electroplating

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MEMS Fabrication

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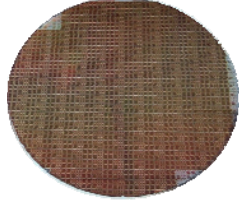
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Making Mechanical Devices

- How best does one make a mechanical product?
- Assembly line production?
 - ↳ Pick and place parts
 - ↳ Used for many macroscopic mechanical products
 - ↳ Robotic automation greatly reduces cost
- **Problem:** difficult to do this with MEMS-scale parts (but not impossible, as we'll soon see ...)
- **Solution:** borrow from integrated circuit (IC) transistor technology
 - ↳ Use monolithic wafer-level fabrication methods
 - ↳ Harness IC's batch methods, where multiple devices are achieved all at once



Automobile Assembly Line



CMOS Integrated Circuit Wafer

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Polysilicon Surface-Micromachining

- Uses IC fabrication instrumentation exclusively
- *Variations*: sacrificial layer thickness, fine- vs. large-grained polysilicon, *in situ* vs. POCL₃-doping

300 kHz Folded-Beam Micromechanical Resonator

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Electroplating: Metal MEMS

- Use electroplating to obtain metal structures
- When thick: call it "LIGA"
- *Pros*: fast low temp deposition, very conductive
- *Cons*: drift, low mech. Q but may be solvable?

RF Switch

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Bulk Micromachining and Bonding

- Use the wafer itself as the structural material
- *Adv*: very large aspect ratios, thick structures
- *Example*: deep etching and wafer bonding

Micromechanical Vibrating Ring Gyroscope [Najafi, Michigan]

Microrotor (for a microengine) [Pisano, UC Berkeley]

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Oxidation

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Thermal Oxidation of Silicon

- Achieved by heating the silicon wafer to a high temperature (~900°C to 1200°C) in an atmosphere containing pure oxygen or water vapor
- Enabling reactions:
 - For dry oxygen: $\text{Si} + \text{O}_2 \rightarrow \text{SiO}_2$
 - For water vapor: $\text{Si} + 2\text{H}_2\text{O} \rightarrow \text{SiO}_2 + 2\text{H}_2$

Schematically:

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Oxidation Modeling

(1) Initially: (no oxide @ surface)

(2) As oxide builds up:

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Oxidation Modeling (cont.)

$N_0 =$ reactant conc. at oxide surface [in cm^{-2}]
 $N_i =$ reactant conc. at Si-SiO₂ interface
 $J =$ reactant flux = $-D \frac{\partial N(x,t)}{\partial x}$ [Fick's 1st Law of Diffusion]
 Diffusion coeff. [in $\mu\text{m/hr}$ or m/s]

In the SiO₂: $J = D \frac{(N_0 - N_i)}{X_{ox}} = \text{constant}$ (1)
 [in # particles/(cm²·s)] Assumption that the reactant does not accumulate in the oxide.

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Oxidation Modeling (cont.)

At the Si-SiO₂ interface:
 Oxidation rate $\propto N_i \therefore J \propto N_i \Rightarrow J = k_s N_i$ (2)
 Reaction rate constant @ Si-SiO₂ interface

Combining (1) and (2):

$$\left[N_i = \frac{J}{k_s} \right] \Rightarrow J = D \left(\frac{N_0 - J/k_s}{X_{ox}} \right)$$

$$J X_{ox} = D N_0 - \frac{D J}{k_s} \rightarrow J \left(X_{ox} + \frac{D}{k_s} \right) = D N_0$$

$\therefore J = \frac{D N_0}{X_{ox} + \frac{D}{k_s}} = \text{Flux of reactants}$

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Oxidation Modeling (cont.)

Find an expression for $X_{OX}(t)$:

oxidizing flux

$$\left. \begin{array}{l} \text{Rate of change of oxide} \\ \text{layer thickness w/time} \end{array} \right\} = \frac{dX_{OX}}{dt} = \frac{J}{M} = \frac{DN_{O_2}/M}{X_{OX} + D/k_s} \quad (3)$$

of molecules of oxidizing species incorporated into a unit volume of oxide

$$\left. \begin{array}{l} = 2.2 \times 10^{22} \text{ cm}^{-3} \text{ for } O_2 \\ = 4.4 \times 10^{22} \text{ cm}^{-3} \text{ for } H_2O \end{array} \right\}$$

Solve (3) for $X_{OX}(t)$: [Initial condition $X_{OX}(t=0) = X_i$]

$$\frac{dX_{OX}}{dt} = \frac{DN_{O_2}/M}{X_{OX} + D/k_s} \Rightarrow \int_{X_i}^{X_{OX}} \left(X_{OX} + \frac{D}{k_s} \right) dX_{OX} = \int_0^t \frac{DN_{O_2}}{M} dt$$

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Oxide Thickness Versus Time

Result:

additional time required (to go from $X_i \rightarrow X_{OX}$) time required to grow X_i [X_i = initial oxide thickness]

$$X_{OX}(t) = \frac{A}{2} \left\{ \left[1 + \frac{4B}{A^2} (t + \tau) \right]^{1/2} - 1 \right\}$$

where $A = \frac{2D}{k_s}$ $\tau = \frac{X_i^2}{B} + \frac{X_i}{(B/A)}$

$$B = \frac{2DN_{O_2}}{M} \quad D = D_0 \exp\left(-\frac{E_A}{kT}\right)$$

[i.e., D governed by an Arrhenius relationship \rightarrow temperature dependent]

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Oxidation Modeling (cont.)

For shorter times:

$$\left[(t + \tau) \ll \frac{A^2}{4B} \right] \Rightarrow X_{OX}(t) = \left(\frac{B}{A} \right) (t + \tau) \Rightarrow$$

oxide growth limited by reaction at the Si-SiO₂ interface

Taylor expansion (first term after 1's cancel) linear growth rate constant

For long oxidation times: oxide growth diffusion-limited

$$\left[(t + \tau) \gg \frac{A^2}{4B} \right] \Rightarrow X_{OX}(t) = \sqrt{B(t + \tau)} \approx \sqrt{Bt}$$

$t \gg \tau$ Parabolic rate constant

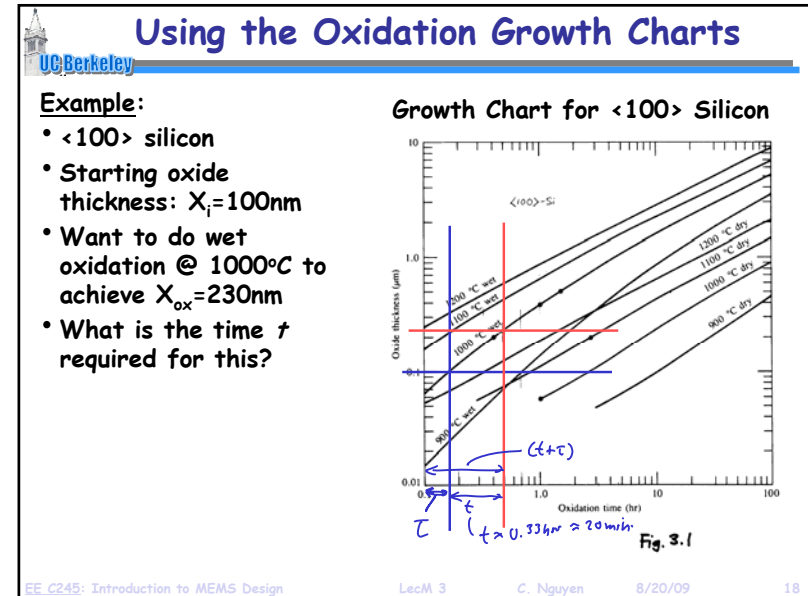
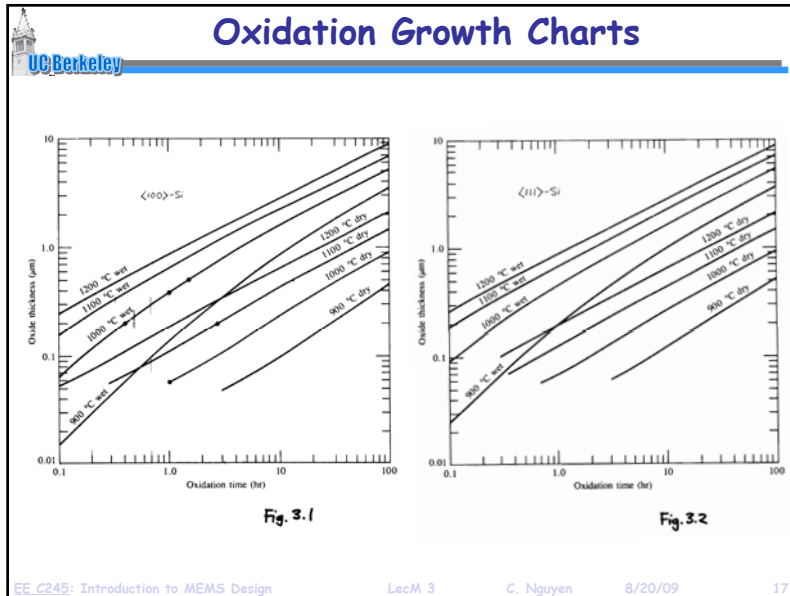
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Oxidation Rate Constants

Ambient	B	B/A
Dry O ₂	$C_1 = 7.72 \times 10^2 \mu\text{m}^2 \text{hr}^{-1}$	$C_2 = 6.23 \times 10^6 \mu\text{m hr}^{-1}$
	$E_1 = 1.23 \text{ eV}$	$E_2 = 2.0 \text{ eV}$
Wet O ₂	$C_1 = 2.14 \times 10^2 \mu\text{m}^2 \text{hr}^{-1}$	$C_2 = 8.95 \times 10^7 \mu\text{m hr}^{-1}$
	$E_1 = 0.71 \text{ eV}$	$E_2 = 2.05 \text{ eV}$
H ₂ O	$C_1 = 3.86 \times 10^2 \mu\text{m}^2 \text{hr}^{-1}$	$C_2 = 1.63 \times 10^8 \mu\text{m hr}^{-1}$
	$E_1 = 0.78 \text{ eV}$	$E_2 = 2.05 \text{ eV}$

• Above theory is great ... but usually, the equations are not used in practice, since measured data is available
 ↳ Rather, oxidation growth charts are used

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Factors Affecting Oxidation

- In summary, oxide thickness is dependent upon:
 1. Time of oxidation
 2. Temperature of oxidation
 3. Partial pressure of oxidizing species ($\propto N_o$)
- Also dependent on:
 4. Reactant type:
 - Dry O_2
 - Water vapor \Rightarrow faster oxidation, since water has a higher solubility (i.e., D) in SiO_2 than O_2
 5. Crystal orientation:
 - <111> \leftarrow faster, because there are more bonds available at the Si-surface
 - <100> \leftarrow fewer interface traps; smaller # of unsatisfied Si-bonds at the Si- SiO_2 interface

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Factors Affecting Oxidation

6. Impurity doping:
 - P: increases linear rate const.
no affect on parabolic rate constant
faster initial growth \rightarrow surface reaction rate limited
 - B: no effect on linear rate const.
increases parabolic rate const.
faster growth over an initial oxide \rightarrow diffusion faster

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Thin Film Deposition

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Thin Film Deposition

- Methods for film deposition:
 - ↳ Evaporation
 - ↳ Sputter deposition
 - ↳ Chemical vapor deposition (CVD)
 - ↳ Plasma enhanced chemical vapor deposition (PECVD)
 - ↳ Epitaxy
 - ↳ Electroplating
 - ↳ Atomic layer deposition (ALD)

Evaporation:

- Heat a metal (Al, Au) to the point of vaporization
- Evaporate to form a thin film covering the surface of the Si wafer
- Done under vacuum for better control of film composition

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Evaporation

Filament Evaporation System:

1. Pump down to vacuum → reduces film contamination and allows better thickness control
2. Heat W filament → melt Al, wet filament
3. Raise temperature → evaporate Al

$$\text{mean free path} = \lambda = \frac{kT}{\sqrt{2\pi} Pd^2}$$

k = Boltzmann Constant
 T = temperature
 P = pressure
 d = diameter of gas molecule

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Evaporation (cont.)

- λ can be ~60m for a 4Å particle at 10^{-4} Pa ($-0.75 \mu\text{Torr}$)
 - ↳ thus, at 0.75 μTorr , get straight line path from Al staple filament to wafer

Problem: Shadowing & Step Coverage

Problem: line of sight deposition

Solns:

- i. Rotate wafer during evaporation
- ii. Etch more gradual sidewalls

Better Solution: forget evaporation → sputter deposit the film!

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Sputter Deposition

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- Use an energetic plasma to dislodge atoms from a material target, allowing the atoms to settle on the wafer surface

Not as low a vacuum as evaporation (~100 Pa) (750 mTorr)

Vacuum Pump

Target (Al, SiO₂, Si₂N₄, ZnO, Ti, ...)

plasma

Ar+

Ar+

wafer

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Sputter Deposition Process

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- Step-by-step procedure:**
 - Pump down to vacuum
 $(\sim 100 \text{ Pa}) \rightarrow 1 \text{ Pa} = 9.8 \times 10^{-6} \text{ atm} \left(\frac{760 \text{ Torr}}{\text{atm}} \right) = 0.0075012 \text{ Torr}$
 \swarrow
 7.5 mTorr
 - Flow gas (e.g., Ar)
 - Fire up plasma (create Ar⁺ ions) → apply dc-bias (or RF for non-conductive targets)
 - Ar⁺ ions bombard target (dislodge atoms)
 - Atoms make their way to the wafer in a more random fashion, since at this higher pressure, $\lambda \sim 60 \mu\text{m}$ for a 4 Å particle; plus, the target is much bigger
- Result:** better step coverage!

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Problems With Sputtering

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- Get some Ar in the film
- Substrate can heat up
 - ↪ up to ~350°C, causing nonuniformity across the wafer
 - ↪ but it still is more uniform than evaporation!
- Stress can be controlled by changing parameters (e.g., flow rate, plasma power) from pass to pass, but repeatability is an issue

• **Solution:** use Chemical Vapor Deposition (CVD)

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Chemical Vapor Deposition (CVD)

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- Even better conformity than sputtering
- Form thin films on the surface of the substrate by thermal decomposition and/or reaction of gaseous compounds
 - ↪ Desired material is deposited directly from the gas phase onto the surface of the substrate
 - ↪ Can be performed at pressures for which λ (i.e., the mean free path) for gas molecules is small
 - ↪ This, combined with relatively high temperature leads to

Excellent Conformal Step Coverage!

- ↪ **Types of films:** polysilicon, SiO₂, silicon nitride, SiGe, Tungsten (W), Molybdenum (M), Tantalum (Ta), Titanium (Ti), ...

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