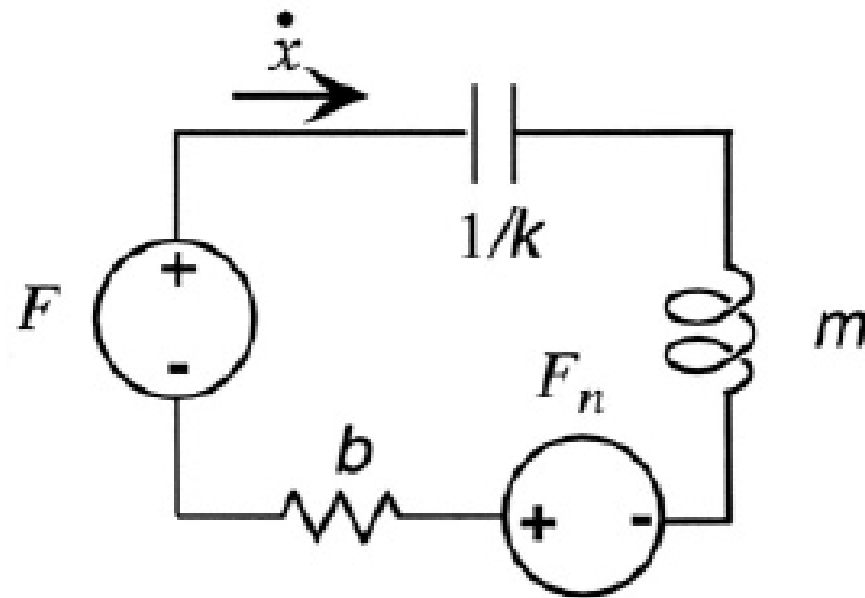


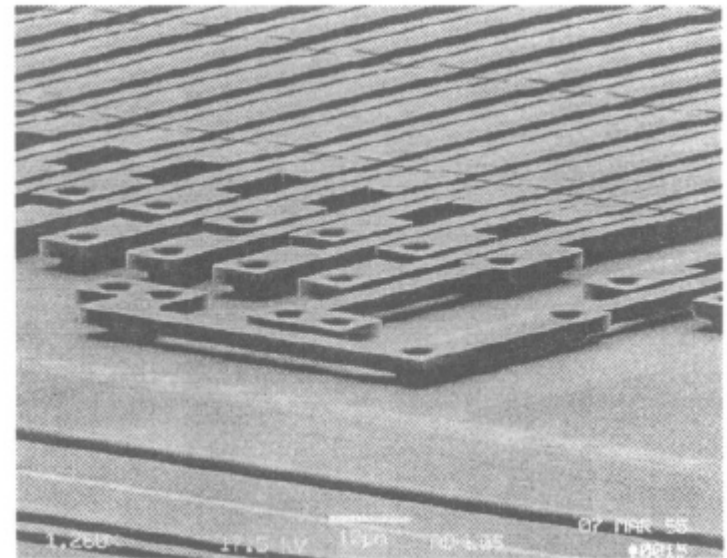
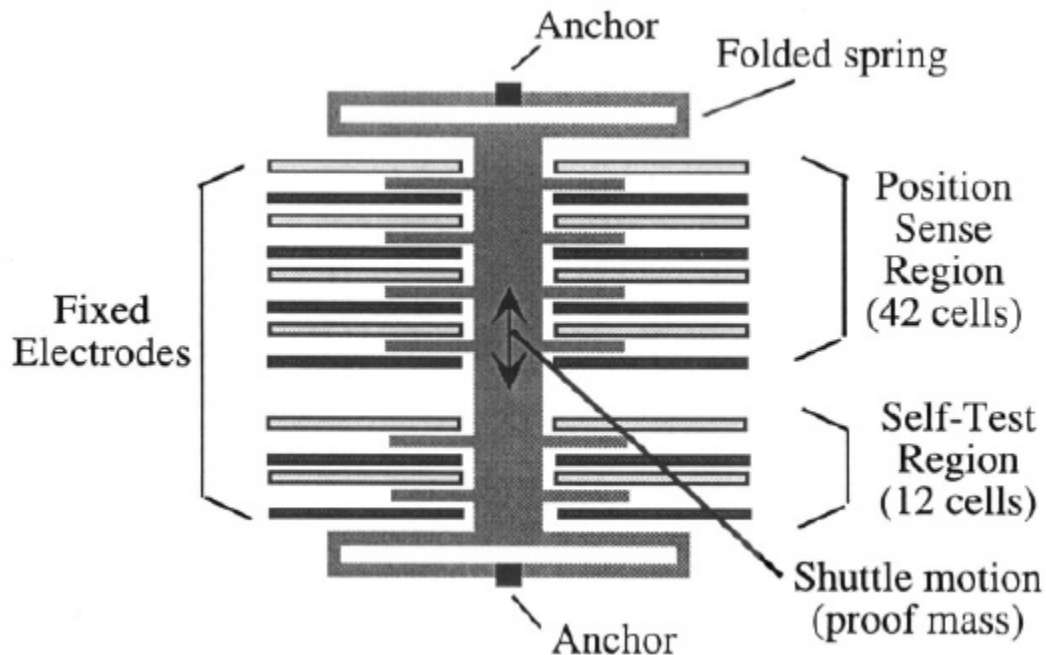
# EE 245 Discussion Section 9/12/2011

- Unless otherwise noted, all material taken from Senturia *Microsystems Design*:  
<http://www.springerlink.com/content/978-0-7923-7246-2/>

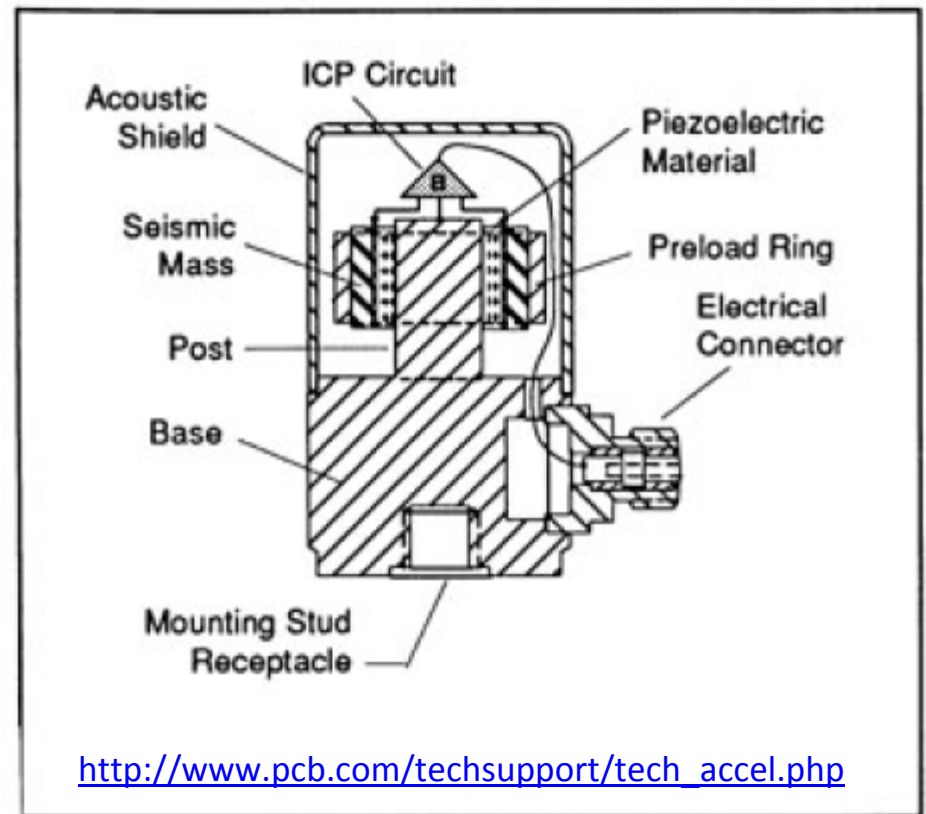
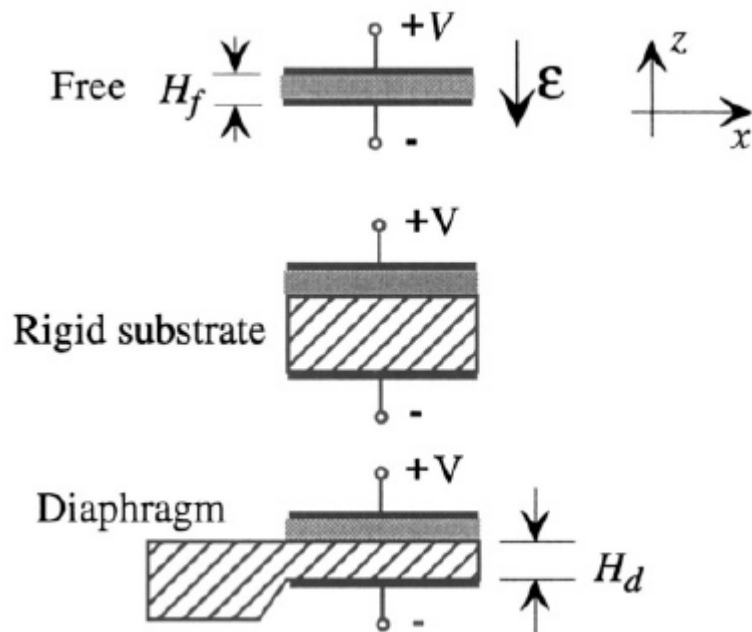
# Accelerometers: $F = ma$



# Capacitive Sensing



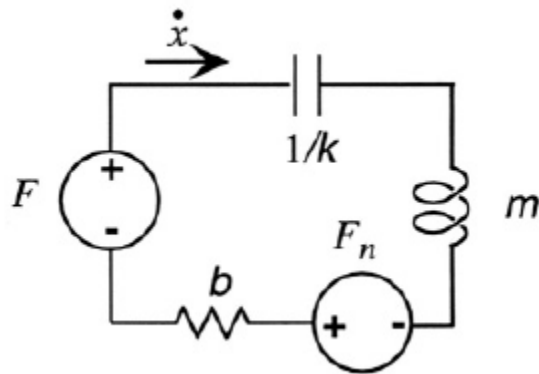
# Piezoelectric Sensing



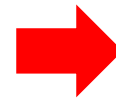
## Shear Mode

Shear mode designs bond, or "sandwich," the sensing crystals between a center post and seismic mass. A compression ring or stud applies a preload force required to create a rigid linear structure. Under acceleration, the mass causes a shear stress to be applied to the sensing crystals.

This system has an undamped resonant frequency  $\omega_o$  equal to  $\sqrt{k/m}$  and a quality factor  $Q$  equal to  $m\omega_o/b$ .



$$\dot{x} = sx = \frac{F + F_n}{ms + b + k/s}$$



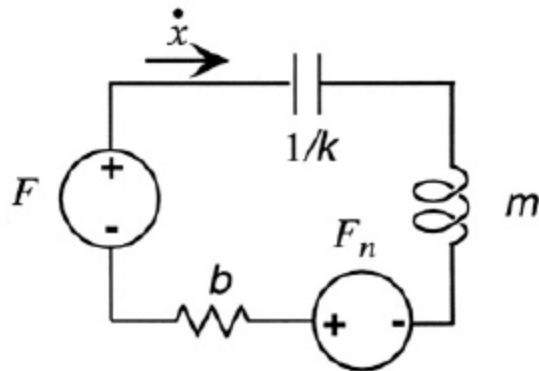
$$x = \frac{F + F_n}{\cancel{ms^2} + \cancel{bs} + k}$$

$\omega_o$  equal to  $\sqrt{k/m}$



$$x = \frac{F + F_n}{k}$$

We examine, first, the signal term, then the noise term. The inertial force  $F$  equals the proofmass  $m$  times the acceleration to be measured, denoted here by  $a$ . This, together with the definition of  $\omega_o$ , leads to a fundamental characteristic of quasi-static accelerometers. The displacement and acceleration are scaled by the square of the resonance frequency:

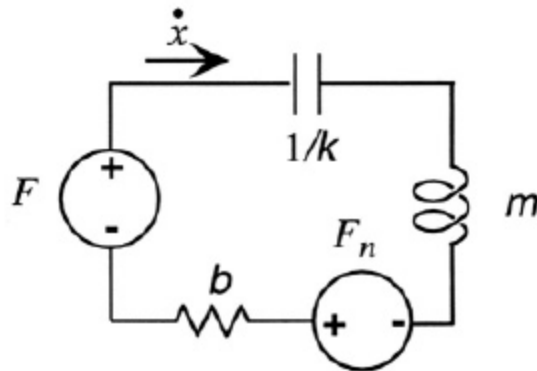


$$x = \frac{F + \cancel{F_n}}{k}$$



$$x = \frac{a}{\omega_o^2}$$

We now consider the intrinsic noise due to damping. The spectral density function of the force noise is  $4k_B T b$ , just like Johnson noise in a resistor. This noise typically arises from fluid damping. It is called *Brownian motion noise*, although in fact, the form of the force-noise spectral density function does not depend on the specific mechanism producing the damping.



$$x = \frac{F + F_n}{k}$$

$$\omega_o \text{ equal to } \sqrt{k/m}$$

$$Q \text{ equal to } m\omega_o/b$$



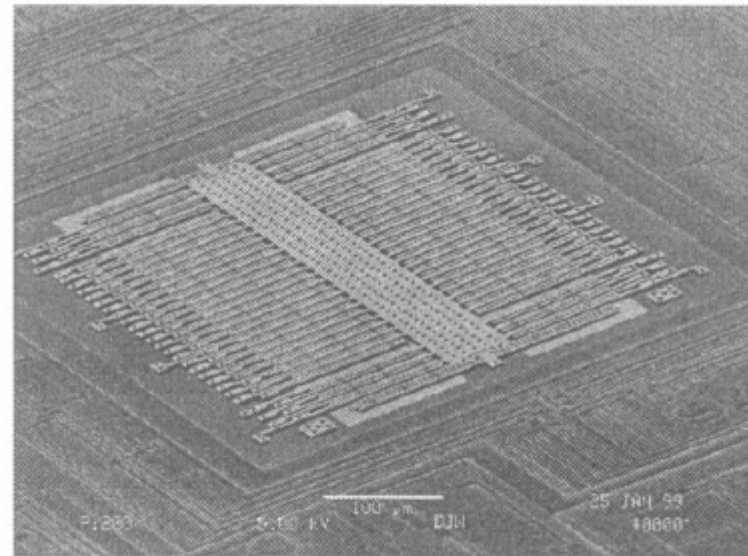
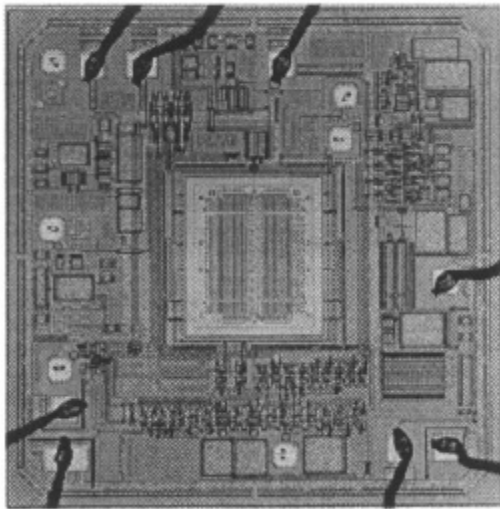
$$a_{n,\text{rms}} = \sqrt{\frac{4k_B T \omega_o}{mQ}}$$



$$\text{ADX326} = 320 \mu\text{g}/\sqrt{\text{Hz}}$$

$$\text{PCB} = 0.4 \mu\text{g}/\sqrt{\text{Hz}}$$

In practice, the signal-to-noise ratio, and, hence, the achievable accelerometer sensitivity, is dominated by other effects: the noise contributed by the position-measuring circuit, especially its first stage of amplification, the need to build additional stiffness into the structure (raising its resonant frequency) to prevent either sticking of parts during fabrication or excess fragility; or residual calibration errors and drift problems. We now consider position measurement methods.



- Other important factors to consider are voltage supply (sensitivity and range) and application (power)