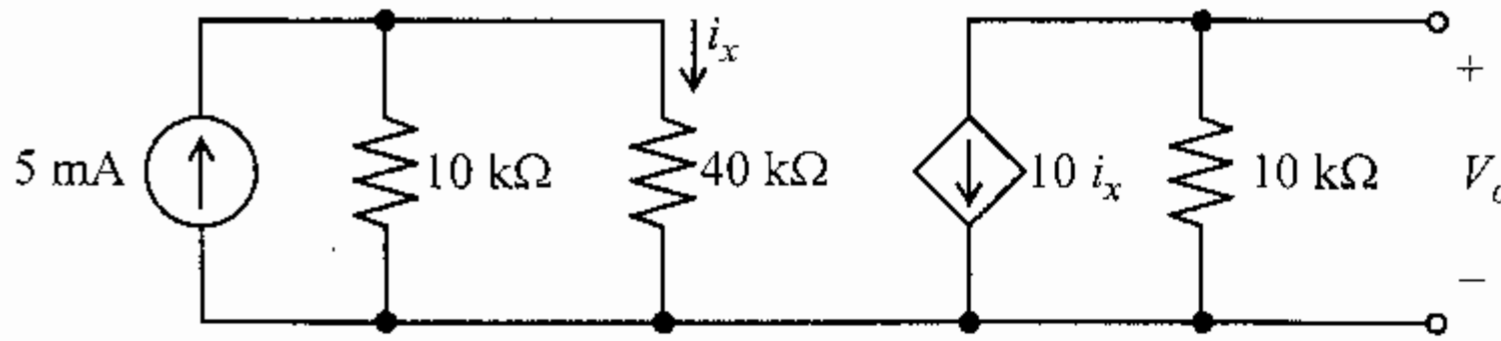


Problem 1 Circuits with Dependent Sources [20 points]a) Find V_o . [4 pts]

Current divider formula: $i_x = \frac{10 \text{ k}\Omega}{10 \text{ k}\Omega + 40 \text{ k}\Omega} (5 \text{ mA})$
 $= 1 \text{ mA}$

$$V_o = -100 \text{ V}$$

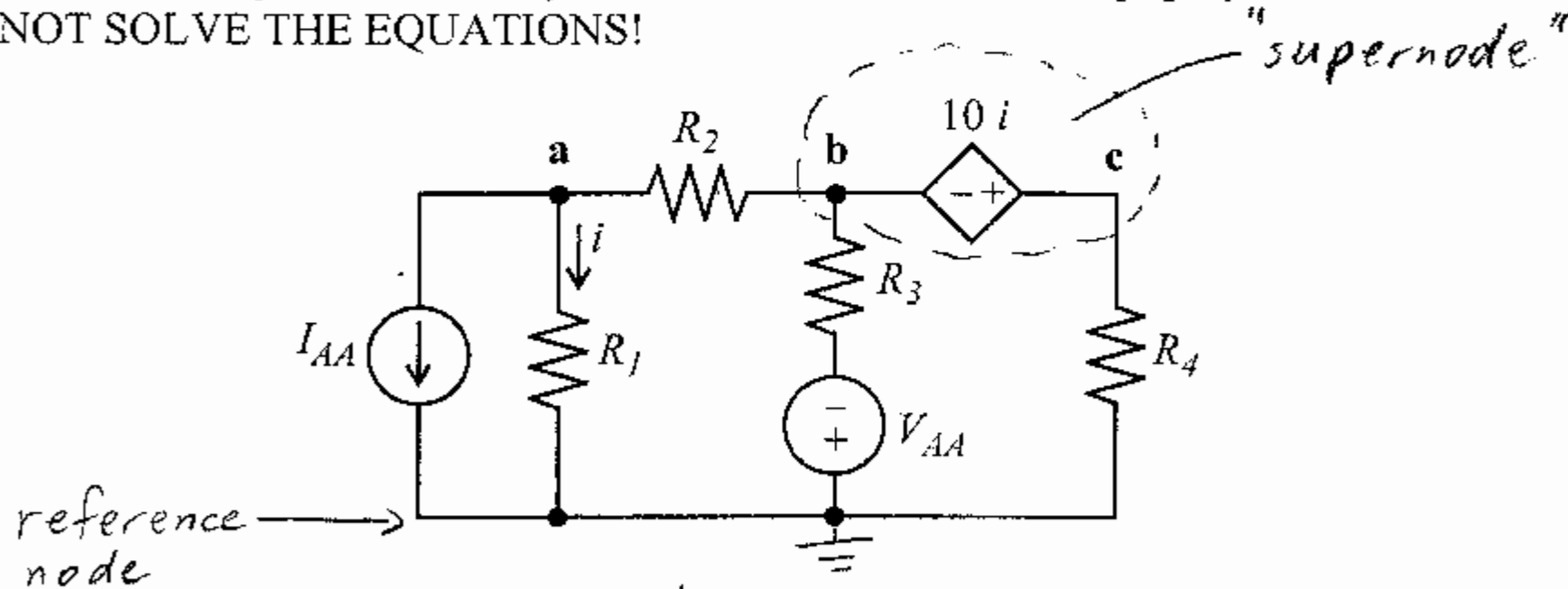
$$V_o = (-10 i_x)(10 \text{ k}\Omega) = (-10 \times 1 \text{ mA})(10 \text{ k}\Omega) = -100 \text{ V}$$

b) In the circuit below, the independent source values and resistances are known.

Use the **nodal analysis technique** to write 3 equations sufficient to solve for V_a , V_b , and V_c .

To receive credit, you must write your answer in the box below. [6 pts]

DO NOT SOLVE THE EQUATIONS!



$$i = \frac{V_a}{R_1}$$

$$\Rightarrow \text{Value of dependent voltage source} = 10i = 10 \left(\frac{V_a}{R_1} \right)$$

Write the nodal equations here:

Note that the only unknowns in these equations

are V_a, V_b, V_c .

$$\text{node a: } I_{AA} + \frac{V_a}{R_1} + \frac{V_a - V_b}{R_2} = 0$$

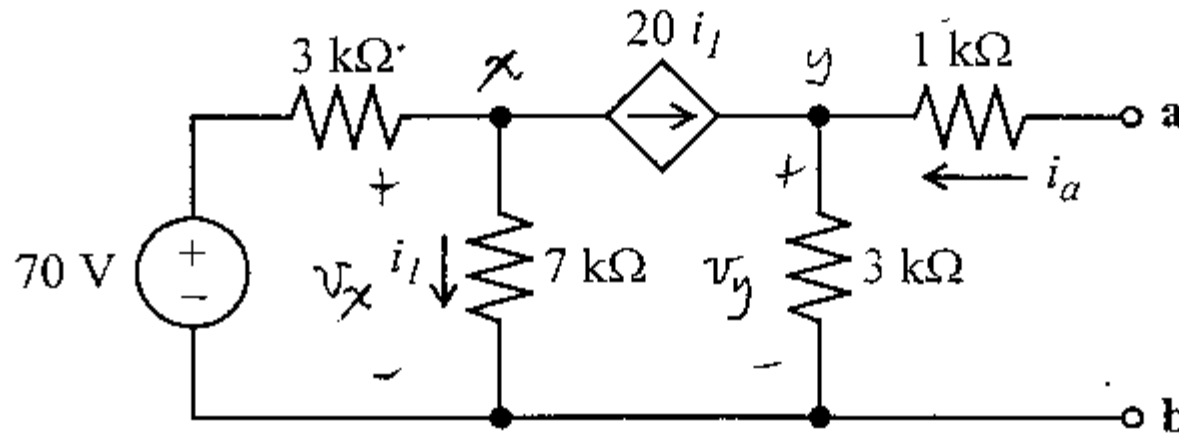
$$\text{supernode: } \frac{V_b - V_a}{R_2} + \frac{V_b + V_{AA}}{R_3} + \frac{V_c}{R_4} = 0$$

$$\text{relationship due to dependent source: } V_c - V_b = 10 \frac{V_a}{R_1}$$

KCL applied

Problem 1 (continued)

c) Consider the following circuit:



i) Find the voltage V_{ab} . [5 pts]

$$i_1 = \frac{v_x}{7k\Omega}$$

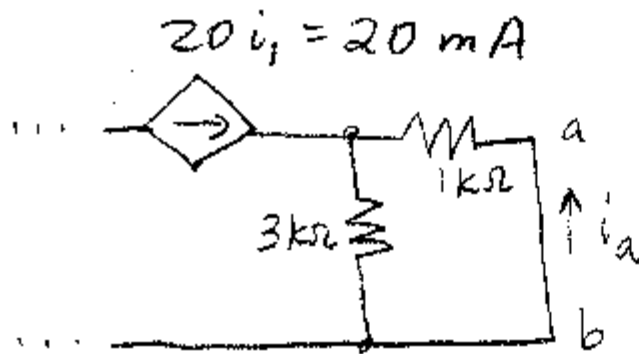
$$V_{ab} = \underline{60} \text{ V}$$

Applying KCL to node x: $\frac{70 - v_x}{3k\Omega} = i_1 + 20i_1 = 21i_1 = 21 \left(\frac{v_x}{7k\Omega} \right)$

$$70 - v_x = 9v_x \Rightarrow v_x = 7V$$

$$i_1 = \frac{7V}{7k\Omega} = 1mA ; i_a = 0 \Rightarrow V_{ab} = v_y = 20i_1 (3k\Omega) = 60V$$

ii) What is the current i_a when the terminals a and b are shorted together? [3 pts]



$$i_a = \underline{-15} \text{ mA}$$

Current divider formula:

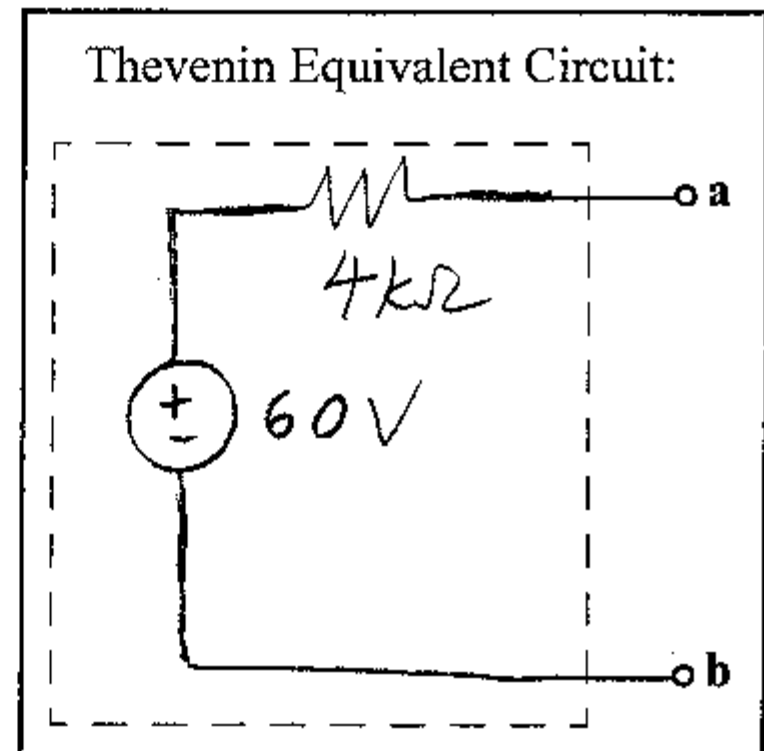
$$i_a = \frac{3k\Omega}{3k\Omega + 1k\Omega} (-20mA) = -15mA$$

iii) Draw the Thevenin Equivalent Circuit. [2 pts]

$$V_{Th} = V_{oc} = V_{ab} \text{ from part (i)}$$

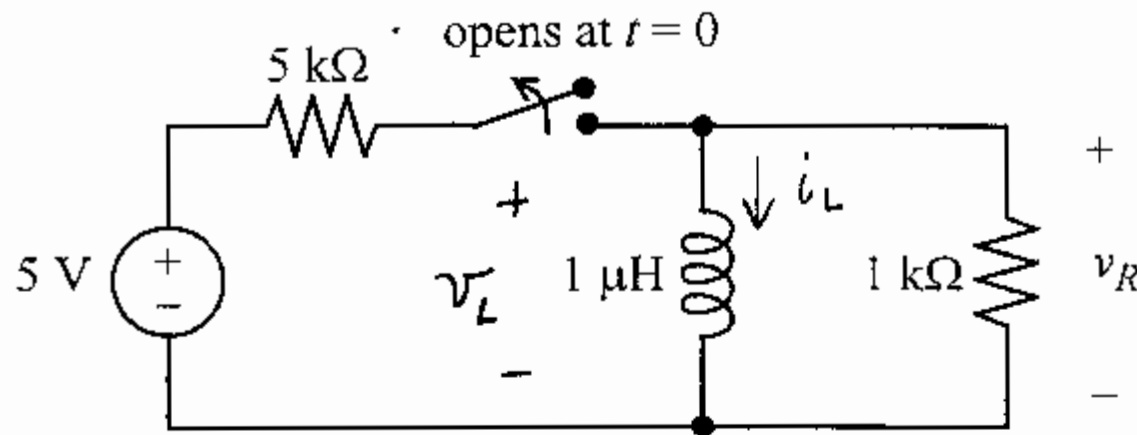
$$R_{Th} = -\frac{V_{oc}}{I_{sc}} = \frac{V_{ab} \text{ from part (i)}}{i_a \text{ from part (ii)}}$$

$$= -\frac{60V}{-15mA} = 4k\Omega$$



Problem 2: Transient Response [30 points]

a) In the circuit below, the switch has been in the closed position for a long time.



i) Find the value of v_R just after the switch opens ($t = 0^+$). [3 pts]

Before the switch is opened, the voltage across the inductor is zero ($v_L = L \frac{di_L}{dt} = 0$), i.e. the $1\text{ k}\Omega$ resistor is "shorted out" by the inductor.

$$v_R(0^+) = (-i_L(0^+))(1\text{ k}\Omega) = (-1\text{ mA})(1\text{ k}\Omega) = -1\text{ V}$$

$$v_R(0^+) = \underline{-1} \text{ V}$$

\Rightarrow The current flowing through the inductor $i_L(0^-) = 5\text{ V} / 5\text{ k}\Omega = 1\text{ mA}$

$i_L(0^+) = i_L(0^-) = 1\text{ mA}$, since inductor current cannot change instantaneously.

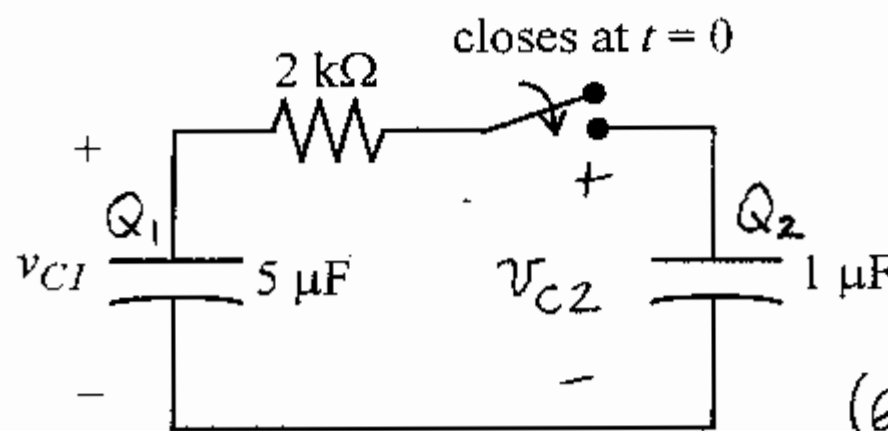
ii) How much energy is dissipated in the $1\text{ k}\Omega$ resistor after the switch is opened? [2 pts]

All of the energy which was stored in the inductor at $t=0$ is dissipated in the $1\text{ k}\Omega$ resistor after the switch is closed.

$$\text{Energy dissipated} = \underline{0.5} \text{ pJ}$$

$$\frac{1}{2} L [i(0)]^2 = \frac{1}{2} (10^{-6} \text{ H}) (10^{-3} \text{ A})^2 = \frac{1}{2} \times 10^{-12} \text{ J}$$

b) In the circuit below, the $5\text{ }\mu\text{F}$ capacitor is initially charged to 5 V ($v_{C1}(0^-) = 5\text{ V}$). (The $1\text{ }\mu\text{F}$ capacitor is initially uncharged.) The switch is then closed at time $t = 0$. What is the final value of v_{C1} ? [5 pts]



Charge stored on a capacitor is $Q = CV$

$$(6\text{ }\mu\text{F}) v_{C1\text{ final}} = (5\text{ }\mu\text{F})(5\text{ V})$$

$$v_{C1\text{ final}} = \frac{5}{6} (5\text{ V}) = 4.17\text{ V}$$

Conservation of charge

$$\Rightarrow Q_{1\text{ final}} + Q_{2\text{ final}} = Q_{1\text{ initial}}$$

$$(5\text{ }\mu\text{F}) v_{C1\text{ final}} + (1\text{ }\mu\text{F}) v_{C2\text{ final}} = (5\text{ }\mu\text{F}) v_{C1\text{ initial}}$$

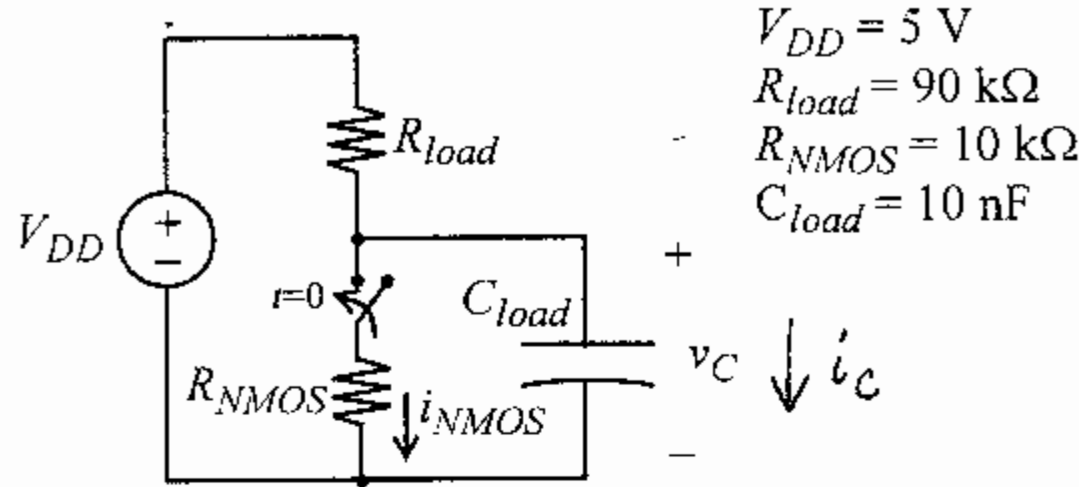
$$\text{Final value of } v_{C1} = \underline{4.2} \text{ V}$$

In the final state ($t = \infty$), the voltages across the capacitors are equal, i.e. $v_{C1\text{ final}} = v_{C2\text{ final}}$

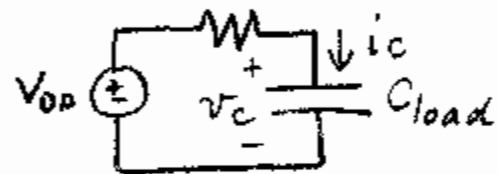
Problem 2 (continued)

c) The following is a circuit model for an NMOS inverter, in which the transistor is turned on at time $t = 0$:

NMOS is off
for $t < 0$
 $\Rightarrow i_{NMOS} = 0$
for $t \leq 0^-$



i) What is the value of v_C at $t = 0^-$? [3 pts]



In steady state (before the switch closes), $i_C = 0$
 $\Rightarrow v_C = V_{DD}$

$v_C(0^-) = 5 \text{ V}$

ii) What is the value of i_{NMOS} at $t = 0^+$? [3 pts]

$v_C(0^+) = v_C(0^-)$, since capacitor voltage cannot change instantaneously
 $i_{NMOS}(0^+) = v_C(0^+) / R_{NMOS} = 5V / 10 \text{ k}\Omega$

$i_{NMOS}(0^+) = 0.5 \text{ mA}$

iii) What is the final value of v_C ? [3 pts]

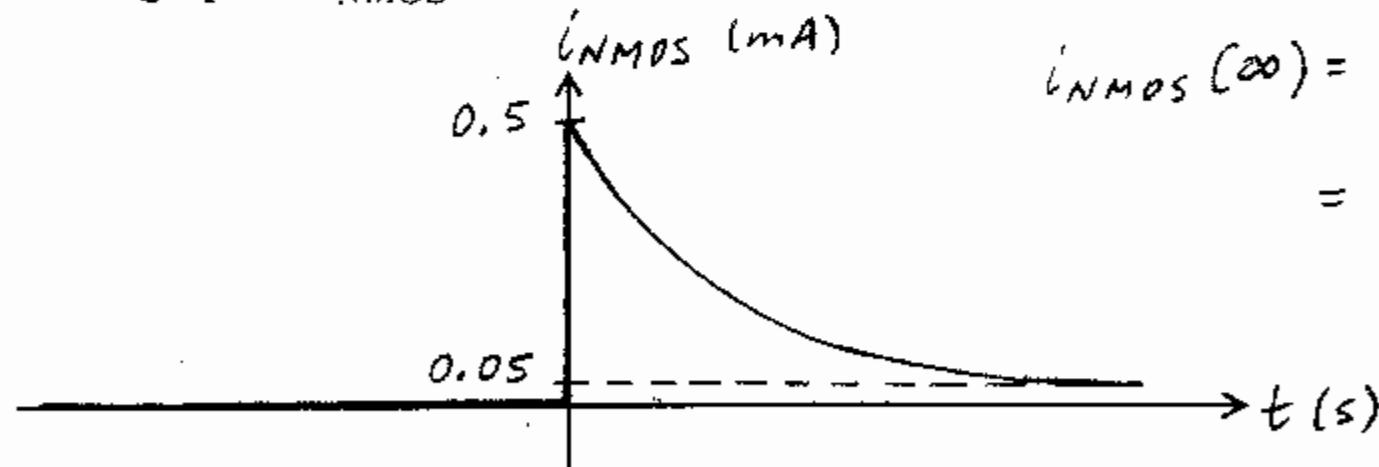
In steady state, $i_C = 0$

Therefore, we have a simple voltage divider:
 $v_C(\infty) = [R_{NMOS} / (R_{NMOS} + R_{load})] V_{DD}$

final value of $v_C = 0.5 \text{ V}$

$v_C(\infty) = \frac{10}{10+90} (5V) = 0.5 \text{ V}$

iv) Neatly sketch the graph of i_{NMOS} for all t , labelling the axes. [5 pts]



$i_{NMOS}(\infty) = \frac{v_C(\infty)}{R_{NMOS}} = \frac{0.5V}{10 \text{ k}\Omega} = 0.05 \text{ mA}$

v) Write an equation for i_{NMOS} as a function of time, for $t > 0$. [6 pts]

$i_{NMOS} = i_{NMOS \text{ final}} + [i_{NMOS}(0^+) - i_{NMOS \text{ final}}] e^{-t/Req C}$

Req is equivalent resistance seen by the capacitor: $Req = R_{load} \parallel R_{NMOS}$

Equation for i_{NMOS} : $0.05 + 0.45 e^{-t/9 \times 10^{-5}} \text{ mA}$

$Req = \frac{(90)(10)}{90+10} = 9 \text{ k}\Omega$; $Req C = (9 \text{ k}\Omega)(10 \text{ nF}) = 9 \times 10^{-5} \text{ s}$

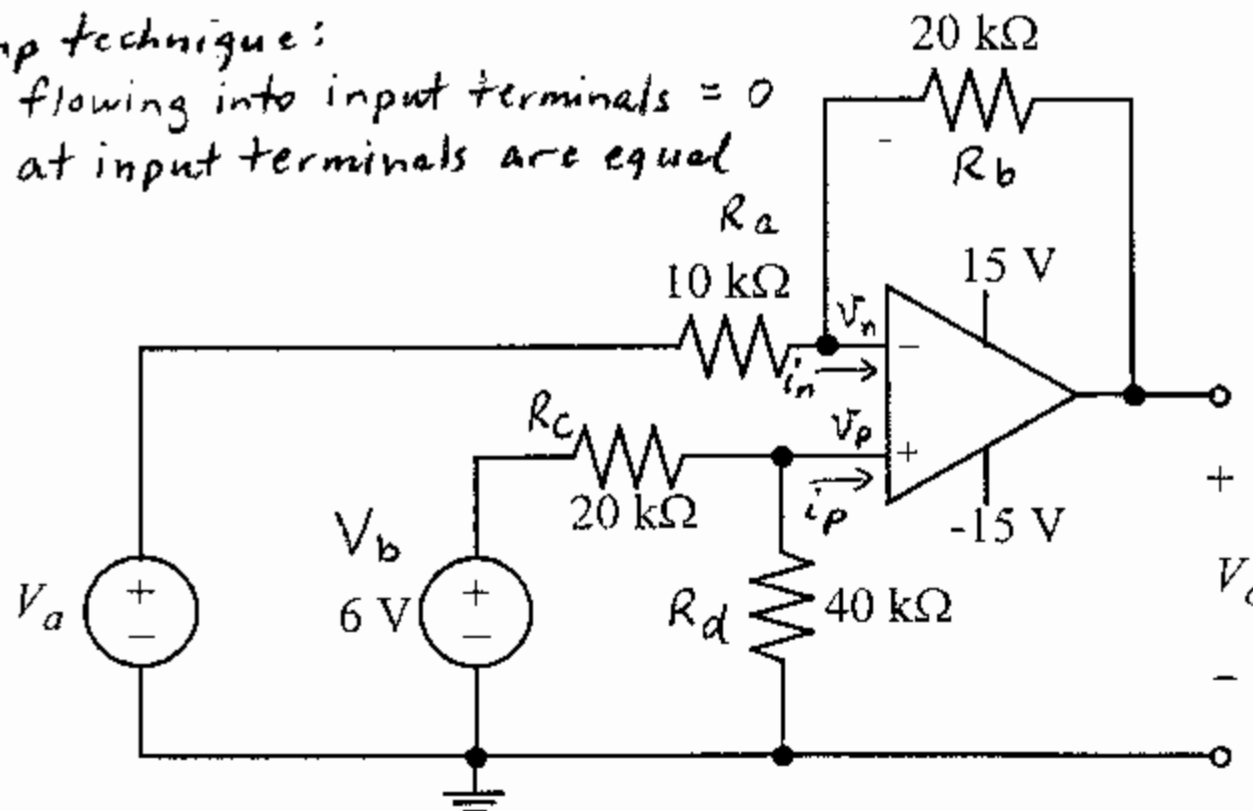
Problem 3: Op-Amp Circuits [25 points]

Assume the op-amps in this problem are ideal.

a) Consider the following circuit:

ideal op-amp technique:

- currents flowing into input terminals = 0
- voltages at input terminals are equal



Apply KCL at (-) node:

$$\frac{V_a - v_n}{R_a} + \frac{V_o - v_n}{R_b} = 0$$

$$\Rightarrow V_o = -\frac{R_b}{R_a} (V_a - v_n) + v_n$$

Since $i_p = 0$, we can use the voltage-divider formula:

$$v_p = \frac{R_d}{R_c + R_d} V_b = v_n$$

$$\Rightarrow V_o = -\frac{R_b}{R_a} \left[V_a - \frac{R_d}{R_c + R_d} V_b \right] + \frac{R_d}{R_c + R_d} V_b$$

i) Find an expression for V_o as a function of V_a . [6 pts]

This is a difference-amplifier circuit (which you've studied in the lab)

with $\frac{R_a}{R_b} = \frac{R_c}{R_d} = \frac{1}{2}$

$$V_o = \frac{R_b}{R_a} (6 - V_a) = 2(6 - V_a)$$

Expression for V_o : 12 - 2 V_a

ii) Find V_o for $V_a = 2$ V. [3 pts]

$$V_o = 12 - 2(2) = 8 \text{ V}$$

$V_o =$ 8 V

iii) For what values of V_a will the op-amp be saturated? [6 pts]

$$V_o = 12 - 2V_a \Rightarrow V_a = \frac{12 - V_o}{2}$$

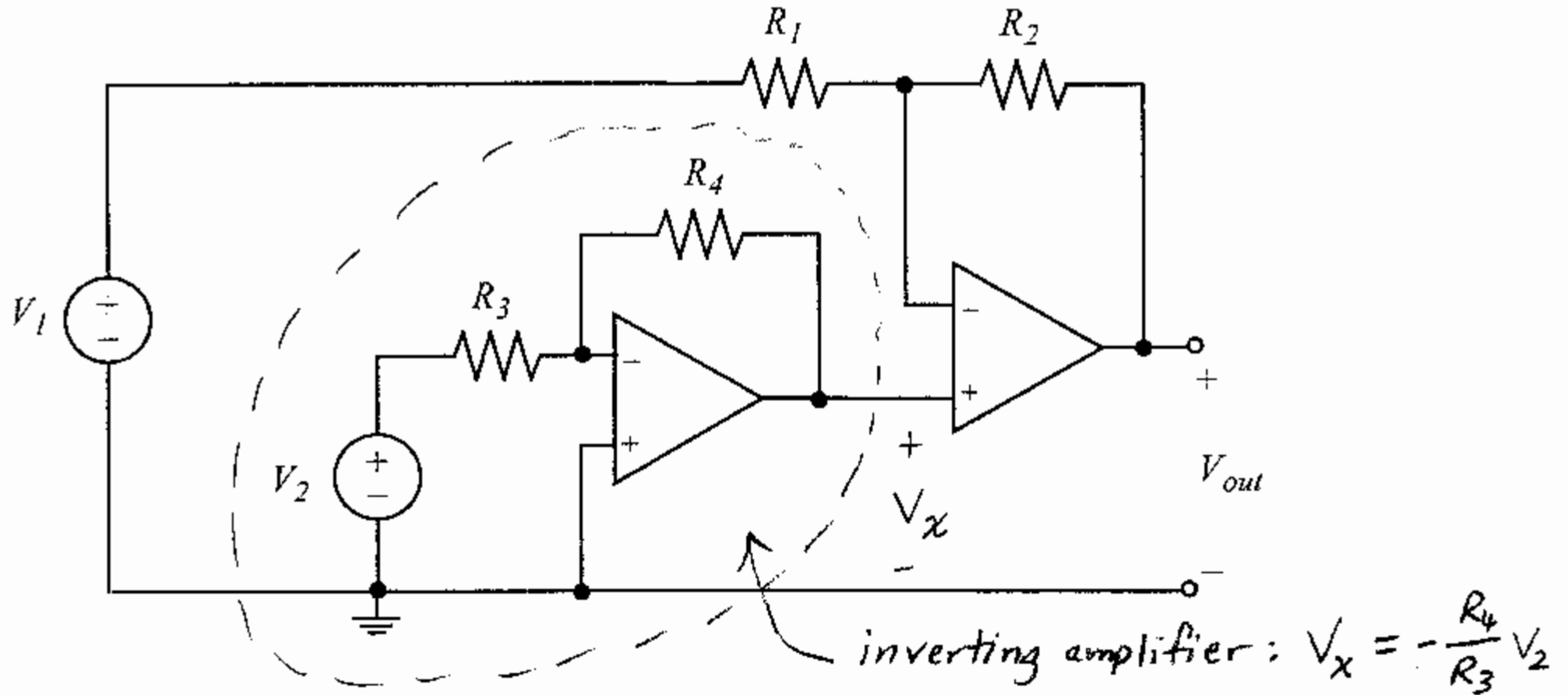
$$V_o \text{ saturated at } 15 \text{ V} : V_a \leq \frac{12 - 15}{2} = -\frac{3}{2} \text{ V}$$

$$V_o \text{ saturated at } -15 \text{ V} : V_a \geq \frac{12 - (-15)}{2} = \frac{27}{2} \text{ V}$$

Values of V_a for which the op-amp will be saturated: $V_a \leq -1.5 \text{ V} ; V_a \geq 13.5 \text{ V}$

Problem 3 (continued)

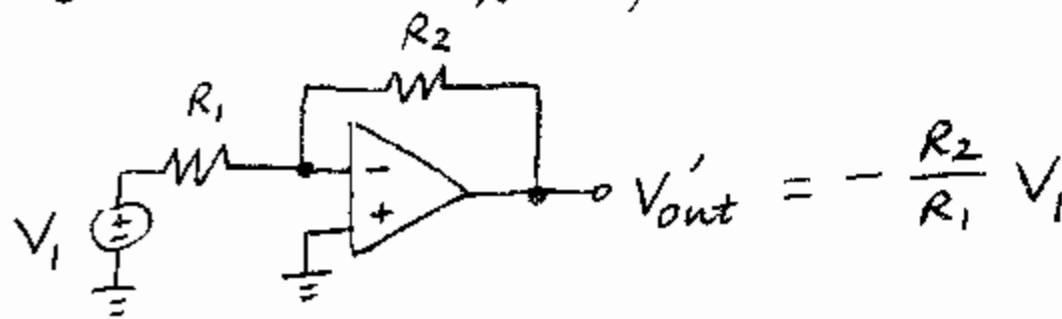
b) In the following circuit, the op-amps are operating linearly.



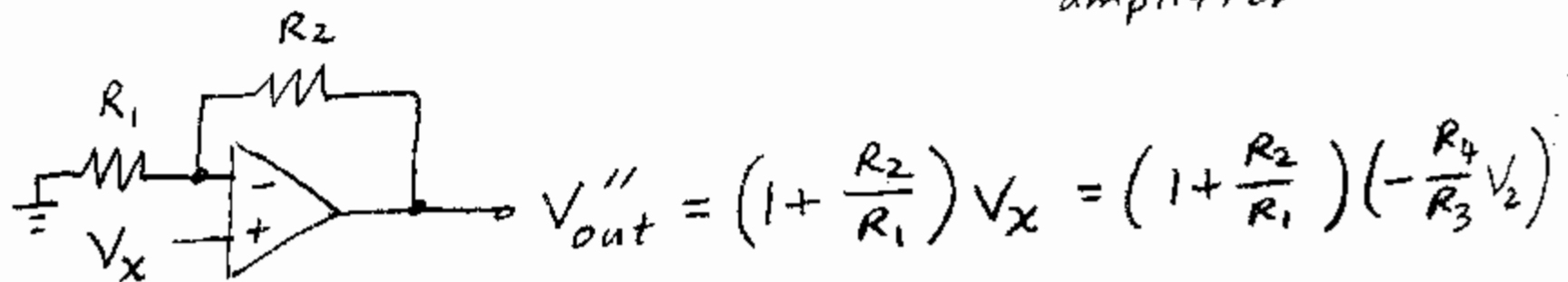
Find V_{out} in terms of $V_1, V_2, R_1, R_2, R_3, R_4$. [10 pts]
 (Hint: The superposition method might be helpful here.)

Find the individual contributions of each voltage source:

i) Set V_2 to 0V: $V_x = 0$, so the circuit simplifies to a simple inverting amplifier



ii) Set V_1 to 0V: Circuit simplifies to simple non-inverting amplifier



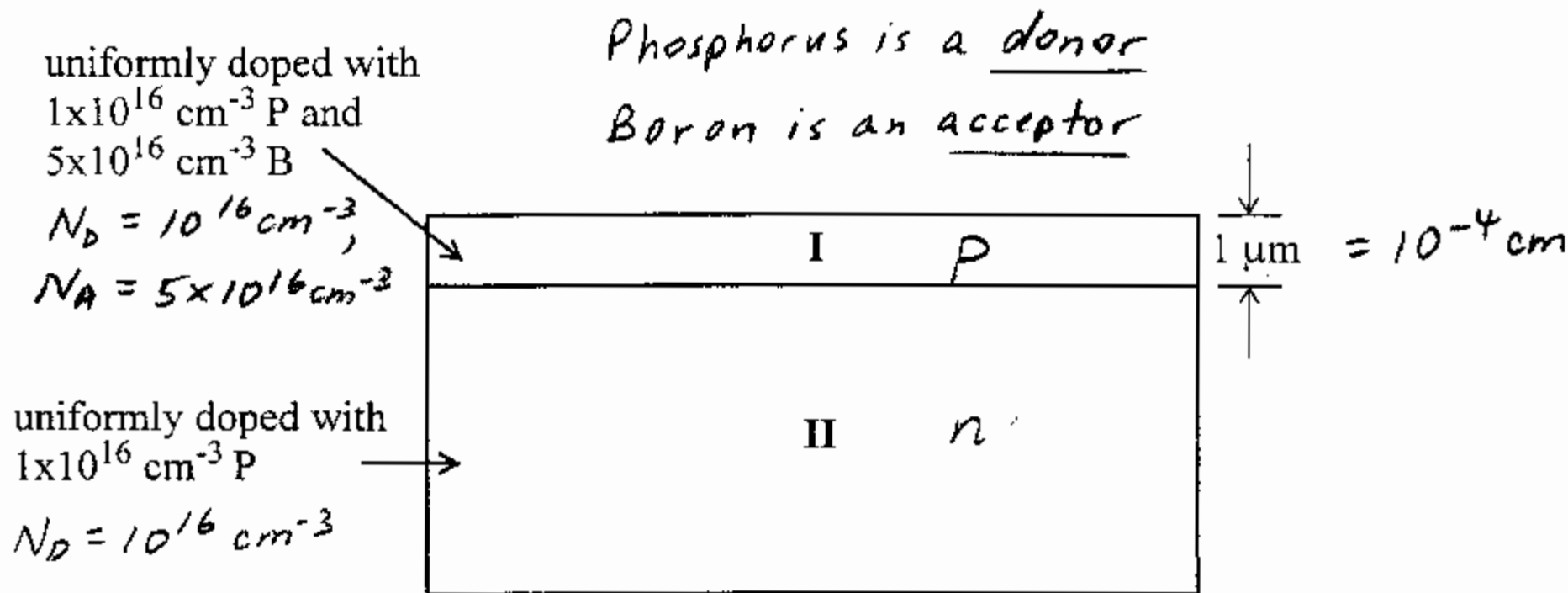
Add the contributions of each source together:

$$V_{out} = V_{out}' + V_{out}'' = -\frac{R_2}{R_1} V_1 - \frac{R_4}{R_3} \left(1 + \frac{R_2}{R_1}\right) V_2$$

$$V_{out} = -\frac{R_2}{R_1} V_1 - \frac{R_4}{R_3} \left(1 + \frac{R_2}{R_1}\right) V_2$$

Problem 4: Semiconductor properties; p-n diodes [25 points]

a) Consider a silicon sample maintained at 300K under equilibrium conditions, uniformly doped with $1 \times 10^{16} \text{ cm}^{-3}$ phosphorus atoms. The surface region of the sample is **additionally** doped uniformly with $5 \times 10^{16} \text{ cm}^{-3}$ boron atoms, to a depth of $1 \mu\text{m}$, as shown in the figure below.



Schematic cross-sectional view of silicon sample

i) In the figure above, indicate the type of the regions (I and II) by labelling them as “n” or “p” type. [2 pts]

ii) What are the electron and hole concentrations in Region I? [5 pts]

$N_A > N_D$, and $N_A \gg n_i$ so

$\rho = N_A - N_D = 5 \times 10^{16} - 1 \times 10^{16} = 4 \times 10^{16}$

$pn = n_i^2 \Rightarrow n = \frac{n_i^2}{p} = \frac{(1.45 \times 10^{10})^2}{4 \times 10^{16}} = 5256$

$n =$	<u>5256</u>	cm^{-3}
$p =$	<u>4×10^{16}</u>	cm^{-3}

iii) What is the sheet resistance of Region I? [5 pts]

$R = \frac{1}{q\mu_n n + q\mu_p p} \approx \frac{1}{q\mu_p p}$

$R_s =$	<u>4458</u>	Ω/square
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From plot on Page 2, $\mu_p \approx 350 \text{ cm}^2/\text{V}\cdot\text{s}$ for $N_A + N_D = 6 \times 10^{16} \text{ cm}^{-3}$

$R_s = \frac{R}{t} = \frac{1}{q\mu_p p t} = [(1.602 \times 10^{-19})(350)(4 \times 10^{16})(10^{-4})]^{-1} = 4458 \Omega/\square$

iv) Suppose any voltage between 0 V and 5 V can be applied to Region I. What fixed voltage (“bias”) would you apply to Region II, to guarantee that no current would ever flow between Region I and Region II? Briefly explain your answer. [3 pts]

To prevent current from flowing, we need to ensure that the p-n junction will never be forward biased. Thus, the n-type region must be biased at 5V or higher.

Region II bias voltage =	<u>5</u>	V
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Problem 4 (continued)

b) If a diode is operated only within a small range of forward-bias voltages, its behavior can be accurately modelled by a resistor, whose value is dependent on the bias voltage. Derive an expression for the diode "small-signal" resistance:

$$R_{diode} = \left(\frac{\partial I}{\partial V} \right)^{-1}$$

in terms of the saturation current I_s , the bias voltage V , and the absolute temperature T . [5 pts]

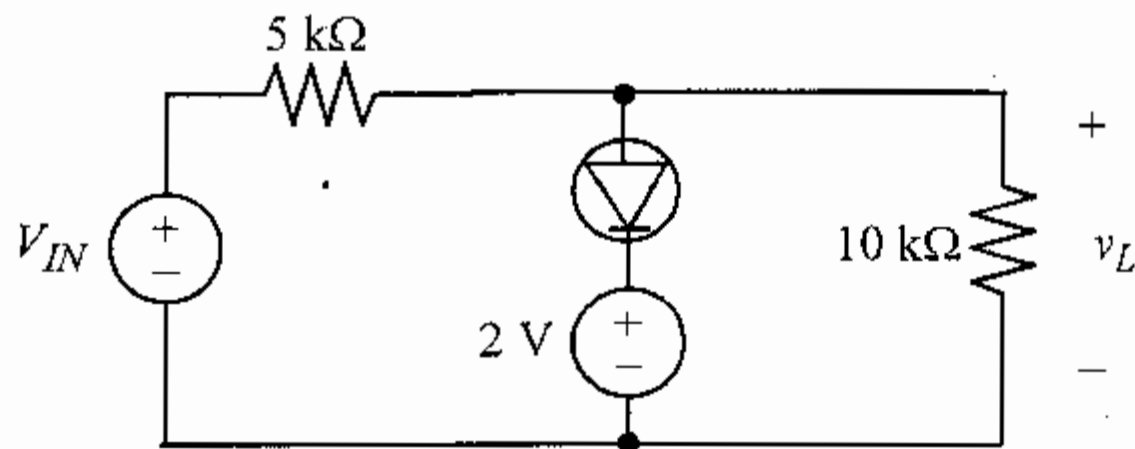
$$I = I_s (e^{qV/kT} - 1)$$

$$\frac{\partial I}{\partial V} = I_s \left(\frac{q}{kT} \right) e^{qV/kT}$$

$$R_{diode} = \frac{kT}{qI_s} e^{-qV/kT}$$

$$R_{diode} = \left(\frac{kT}{qI_s} \right) e^{-qV/kT}$$

c) Plot v_L vs. V_{IN} for $-10 \text{ V} < V_{IN} < 10 \text{ V}$ on the axes provided, for the circuit below. Note that the diode is a perfect rectifier. Label the axes. [5 pts]



When the diode is off, we have a simple voltage-divider circuit

$$v_L = \frac{10}{5+10} V_{IN} = \frac{2}{3} V_{IN}$$

Diode turns on when v_L reaches 2V, i.e. when $\frac{2}{3} V_{IN} = 2V$, or $V_{IN} = 3V$

