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**EE40**  
**Lecture 11**  
**Josh Hug**

7/19/2010

# Logistical Things

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- Lab 4 tomorrow
- Lab 5 (active filter lab) on Wednesday
  - Prototype for future lab for EE40
  - Prelab is very short, sorry.
  - Please give us our feedback
  - Google docs for labs and general class comments now available (link shared via email)
  - Bring a music player if you have one (if not, you can use the signal generator in the lab)
- HW5 due tomorrow at 2PM
- HW6 due Friday at 5PM (also short)
- Midterm next Wednesday 7/28
  - Focus is heavily on HW4, 5, 6, and Labs P1, 4, 5
  - Will reuse concepts from HW 1,2,3

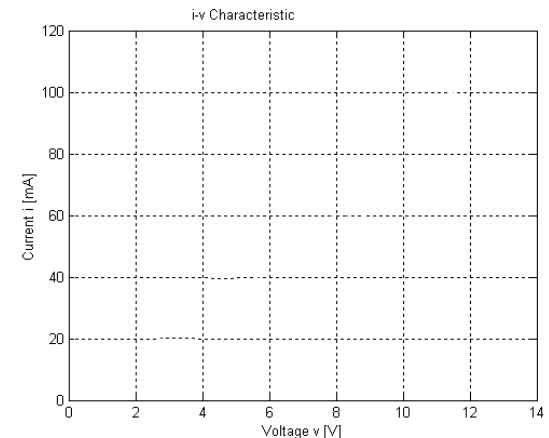
# Logistics

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- No lunch today
- Slightly shorter lecture today
- Midterm regrade requests due today
- Office hours Cory 240 2:30-4PM or so

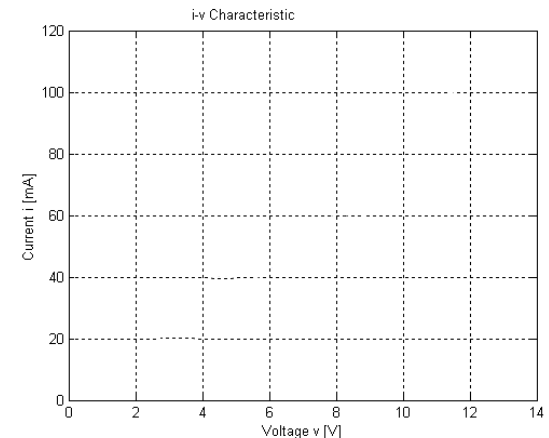
# iClicker Question #1

- Consider a capacitor with a capacitance of  $1nF$ . Total resistance of circuit is small  $\sim 1\Omega$ .
- If we **compile an I-V table in lab** with a voltage source and multimeter by:
  - Applying a set of test voltages
  - Measuring current through the capacitor for each source
- What I-V characteristic will we get?
  - A. Horizontal line at  $I=0$
  - B. Vertical line at  $I=0$
  - C. Line of slope  $1/RC$
  - D. Horizontal line at  $I=V/1\Omega$
  - E. Something else



## iClicker Question #2

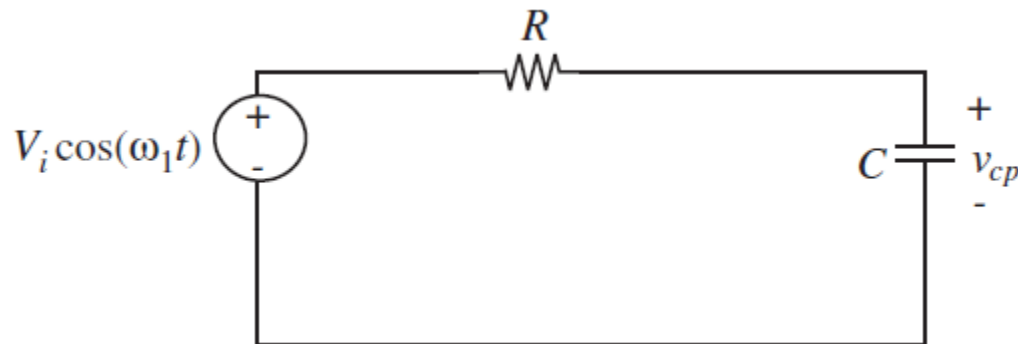
- Consider an inductor with an inductance of  $1\mu\text{H}$ . Total resistance of circuit is small  $\sim 1\Omega$ .
- If we **compile an I-V table in lab** with a voltage source and multimeter by:
  - Applying a set of test voltages
  - Measuring current through the inductor for each source
- What I-V characteristic will we get?
  - A. Horizontal line at  $I=0$
  - B. Vertical line at  $I=0$
  - C. Line of slope  $R/L$
  - D. Line at  $I=V/1\Omega$
  - E. Something else



# Easy Method for AC Circuits

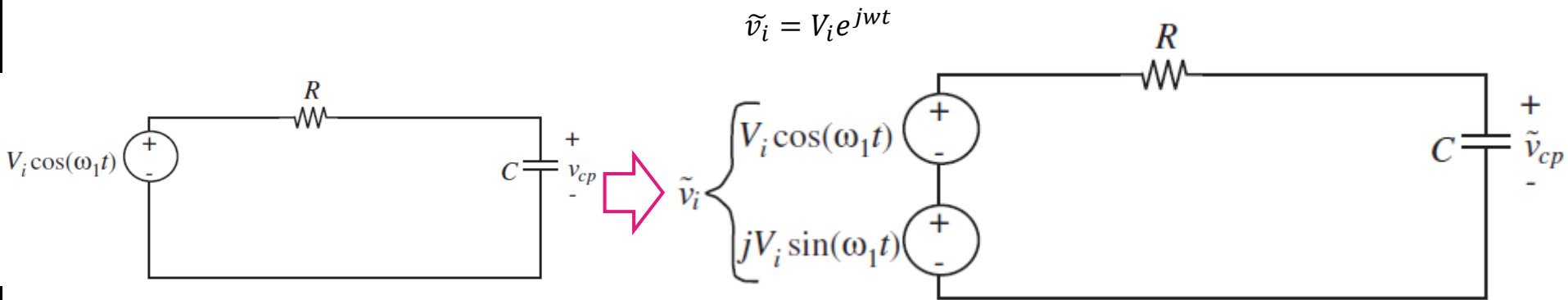
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- We want to find the voltage across the capacitor for the following circuit



- Homogenous solution is easy, since source is irrelevant
- Finding particular solution the usual way (plugging in a guess, finding coefficients that cancel) is painful

# Easy Method for AC Circuits



Guess  $v_{cp} = A \cos(\omega_1 t + \phi)$

Plug into ODE



Solve for A and  $\phi$  (hard)



$$v_{cp} = A \cos(\omega_1 t + \phi)$$

Guess  $\tilde{V}_{cp} = k_1 e^{j\omega t}$



Plug into ODE



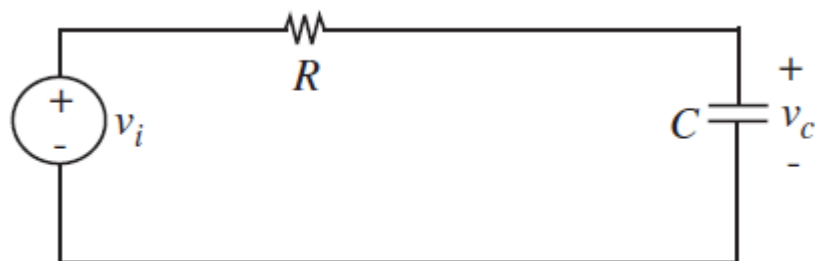
Divide by  $e^{j\omega t}$ . Now  $t$  is gone

Solve for  $k_1$  (easy)



$$v_{cp} = \text{Real}[k_1 e^{j\omega t}]$$

# Memory Circuits with Exponential Source



$$v_I = V_i e^{j\omega t} \quad t > 0$$

$$V'_O = -\frac{V_O}{RC} + V_i \frac{e^{j\omega t}}{RC}$$

- Homogeneous solution is just  $Ae^{-t/RC}$
- Pick particular solution  $V_{O,P} = k_1 e^{j\omega t}$ , plug in:

$$k_1 j\omega e^{j\omega t} = -k_1 \frac{e^{j\omega t}}{RC} + V_i \frac{e^{j\omega t}}{RC}$$

- Divide by  $e^{j\omega t}$ , and solve for  $k_1$

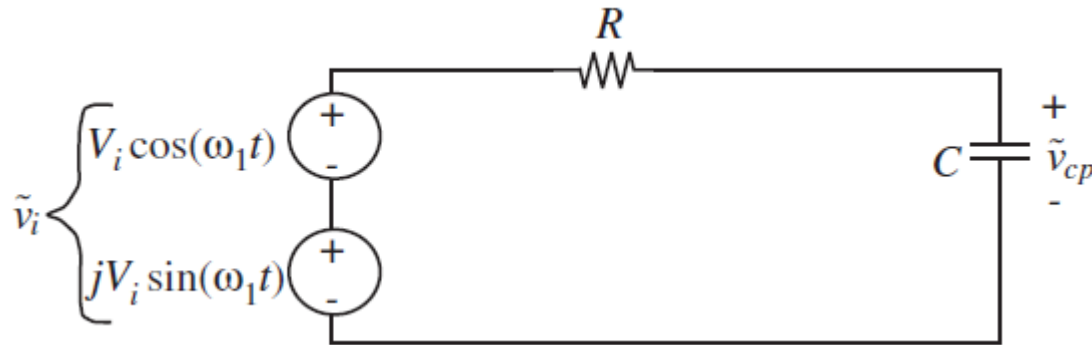
$$k_1 = V_i \frac{1}{1 + j\omega RC}$$

$$V_{O,P}(t) = V_i \frac{1}{1 + j\omega RC} e^{j\omega t}$$

Real part of  $V_{O,P}$  gives solution for cosine source



# Inverse Superposition



- Superposition tells us that our output  $V_{O,P}(t)$  will just be the sum of the effect of these two sources

$$V_{O,P}(t) = V_i \frac{1}{1 + j\omega RC} e^{j\omega t}$$

- Luckily for us, all complex numbers are the sum of their real and imaginary parts  $x = a + jb$
- Just find real part and we're done!

# Real Part of Expression

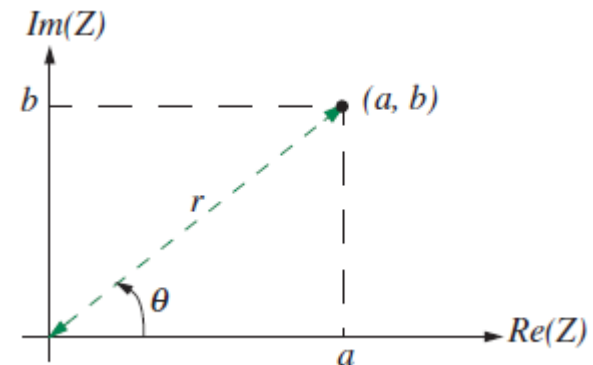
- Finding the real part of the expression is easy, it just involves some old school math that you've probably forgotten (HW5 has complex number exercises)

$$V_{O,P}(t) = \frac{1}{1 + j\omega RC} V_i e^{j\omega t}$$

- Key thing to remember is that complex numbers have two representations
  - Rectangular form:  $a + jb$
  - Polar form:  $r e^{j\theta}$

$$r = \sqrt{a^2 + b^2}$$

$$\theta = \arctan\left(\frac{b}{a}\right)$$



# Real Part of Expression

- What we have is basically the product of two complex numbers
- Let's convert the left one to polar form

$$V_{O,P}(t) = \frac{1}{1 + j\omega RC} V_i e^{j\omega t}$$

– Rectangular form:  $a + jb$

– Polar form:  $r e^{j\theta}$

$$r = \sqrt{a^2 + b^2}$$
$$\theta = \arctan\left(\frac{b}{a}\right)$$

$$V_{O,P}(t) = \frac{1}{R e^{j\phi}} V_i e^{j\omega t} = V_i \frac{1}{\sqrt{1 + (\omega RC)^2}} e^{j\phi} e^{j\omega t}$$

$$\phi = \arctan(\omega RC)$$

# Real Part of Expression

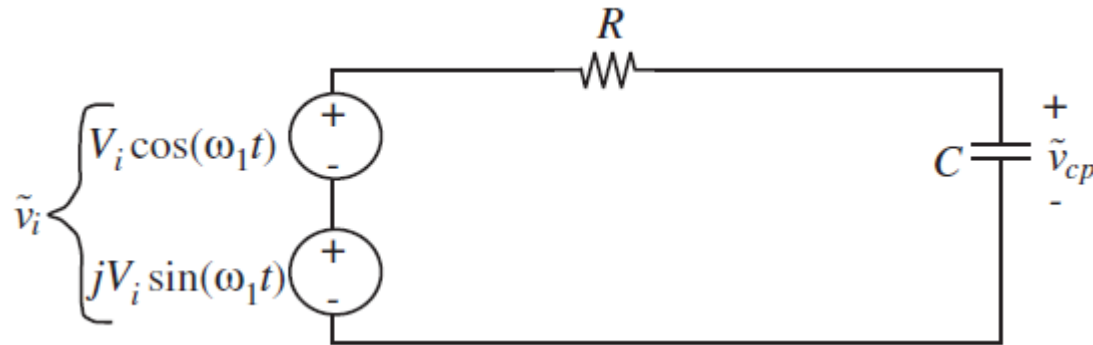
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$$V_i \frac{1}{\sqrt{1 + (\omega RC)^2}} e^{j\phi} e^{j\omega t}$$

$$V_i \frac{1}{\sqrt{1 + (\omega RC)^2}} e^{j(\phi + \omega t)}$$

$$V_i \frac{1}{\sqrt{1 + (\omega RC)^2}} (\cos(\omega t + \phi) + j\sin(\omega t + \phi))$$

# Real Part of Expression



- Superposition tells us that our output  $V_{O,P}(t)$  will just be the sum of the effect of these two sources

$$V_{O,P}(t) = \frac{V_i}{\sqrt{1 + (\omega RC)^2}} (\cos(\omega t + \phi) + j \sin(\omega t + \phi))$$

- Thus, particular solution (forced response) of original cosine source is just the real part

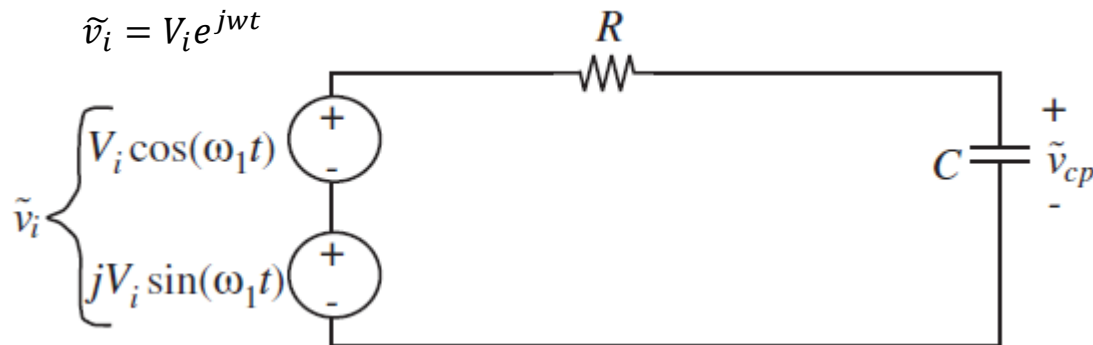
$$V_{O,P}(t) = \frac{V_i}{(1 + \omega RC)^2} \cos(\omega t + \phi) \quad \phi = \arctan(\omega RC)$$

# Easy Method for AC Circuits

Just as actually writing the ODE isn't necessary for DC sources, we can avoid the ODE again in AC circuits:

## Impedance Analysis

$$\tilde{v}_i = V_i e^{j\omega t}$$



Write ODE



$$\text{Guess } \tilde{V}_{cp} = k_1 e^{j\omega t}$$



Plug into ODE

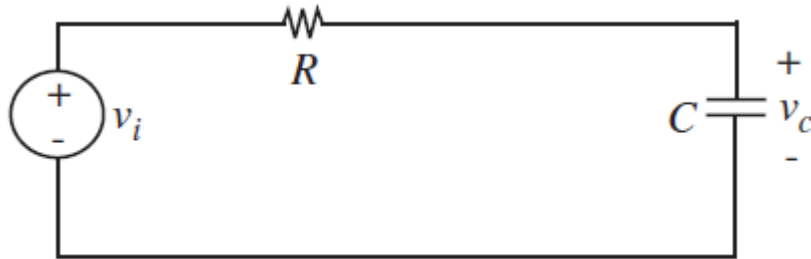


Divide by  $e^{j\omega t}$ . Now  $t$  is gone  
Solve for  $k_1$  (easy)



$$v_{cp} = \text{Real}[k_1 e^{j\omega t}]$$

# Impedance



$$v_I = V_i e^{j\omega t} \quad t > 0$$

For a complex exponential source:

$$V_{C,P}(t) = \frac{1}{1 + j\omega RC} v_I(t)$$

Rewrite as:

$$V_{C,P}(t) = \frac{1/j\omega C}{1/j\omega C + R} v_I(t)$$

Let  $Z_c = 1/j\omega C$

$$V_{C,P}(t) = \frac{Z_c}{Z_c + R} v_I(t)$$

Looks a lot like...  
voltage divider

Real part gives solution for  $v_I = V_i \cos(\omega t)$

## Method of Impedance Analysis (without Phasors)

- Replace passive components with equivalent impedance,  $Z_C = \frac{1}{j\omega C}$ ,  $Z_L = j\omega L$ ,  $Z_R = R$
- Replace all sources with complex exponentials
  - e.g.  $v(t) = A \cos(\omega t + \theta) \Rightarrow \tilde{v}(t) = Ae^{j(\omega t + \theta)}$
- Solve using Ohm's Law of Impedances for complex exponential sources
  - $\tilde{v}(t) = \tilde{i}(t)Z$
  - Just like normal node voltage, but with complex numbers
  - Real part of node voltage  $\tilde{V}_a(t)$  gives true output  $V_a(t)$

Lugging these complex exponential functions is algebraically annoying



# Phasors (not in the book!)

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- Definition: A phasor is a complex number which represents a sinusoid
- $f(t) = A\cos(\omega t + \theta)$
- Three parameters
  - A: Magnitude
  - $\omega$ : Frequency
  - $\theta$ : Phase
- The phasor representation of the sinusoid above is  $Ae^{j\theta}$
- In shorthand we write phasor as  $A\angle\theta$

# Phasors

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- If we have a voltage  $V(t) = A\cos(\omega t + \theta)$
- The phasor version of the voltage is  $\hat{V} = A\angle\theta$
- If we have a phasor  $\hat{I} = \alpha\angle\phi$ , the time function this phasor represents is  $i(t) = \alpha\cos(\omega t + \phi)$

# Why are phasors useful?

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- Sources that look like  $Ae^{t(j\omega+\theta)}$  result in lots of  $Ae^{t(j\omega+\theta)}$  terms in our algebra
- When you apply a sinusoidal source to a circuit, the amplitude and phase will vary across components, but it will always still be  $\alpha e^{t(j\omega+\phi)}$ 
  - Important:  $\omega$  doesn't change!
    - Otherwise we'd need REALLY complex numbers
- Thus, we'll just replace our sources with a complex number  $A\angle\phi$  and just keep in mind that this number represents a function throughout

# Why are phasors useful?

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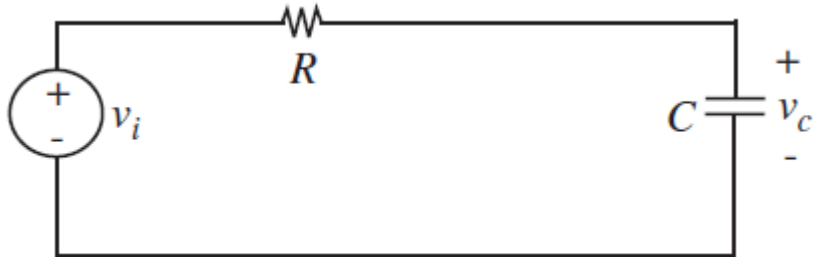
- We know that for complex exponential sources, we have that:
  - $\tilde{v}(t) = \tilde{i}(t)Z$
  - $real[\tilde{v}(t)] = real[\tilde{i}(t)Z]$
- Phasors are complex numbers  $\hat{V}$  and  $\hat{I}$  which represent cosine functions  $v(t)$  and  $i(t)$
- Cosine functions are just the real parts of complex exponentials
- Thus, in the world of phasors, we can just rewrite Ohm's Law of Impedances as:
  - $\hat{V} = \hat{I}Z$

## Method of Impedance Analysis (with Phasors)

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- Replace passive components with equivalent impedance,  $Z_C = \frac{1}{j\omega C}$ ,  $Z_L = j\omega L$ ,  $Z_R = R$
- Replace all sources with phasor representation:  
e.g.  $v(t) = A \cos(\omega t + \theta) \Rightarrow \hat{V}(t) = A \angle \theta$
- Solve using Ohm's Law of Impedances:
  - $\hat{v} = \hat{i}Z$
  - Just like normal node voltage, but with complex numbers, attaining voltage phasors  $\hat{V}_a, \hat{V}_b, \dots$
  - Output  $V_a(t)$  is just  $|\hat{V}_a| \cos(\omega t + \angle \hat{V}_a)$
- Original sources are implicitly represented by phasors
  - Time is gone completely from our problem

# Example



$$v_I = V_i \cos(\omega t), \quad t > 0$$

$$R = 10,000\Omega$$

$$C = 1\mu F$$

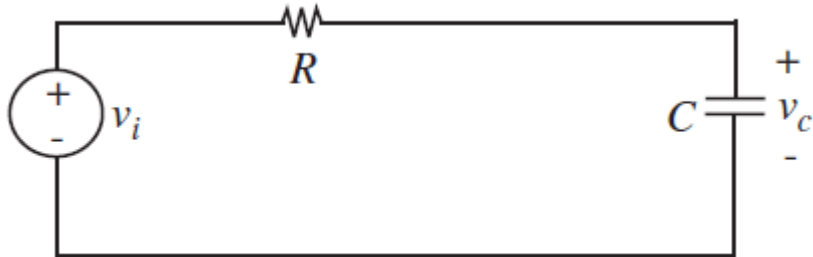
$$V_i = 5V$$

$$\omega = 100$$

Find  $i(t)$  in steady state

- $Z_R = 10000, Z_C = \frac{1}{j\omega C} = -10000j$
- $\hat{V} = V_i \angle 0 = 5 \angle 0$
- $Z_{eq} = 10000 - 10000j$
- $\hat{I} = \frac{5 \angle 0}{10000 - 10000j}$

# Example



$$v_I = V_i \cos(\omega t), \quad t > 0$$

$$R = 10,000\Omega$$

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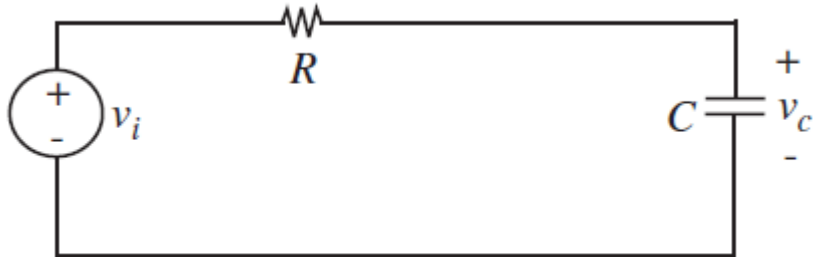
$$V_i = 5V$$

$$\omega = 100$$

Find  $i(t)$  in steady state

- $\hat{I} = \frac{5\angle 0}{10000 - 10000j}$
- Polar divided by non polar, so convert bottom to polar
- $10000 - 10000j = 10000\sqrt{2}\angle \frac{-\pi}{4}$

# Example



$$v_I = V_i \cos(\omega t), \quad t > 0$$

$$R = 10,000\Omega$$

$$C = 1\mu F$$

$$V_i = 5V$$

$$\omega = 100$$

Find  $i(t)$  in steady state

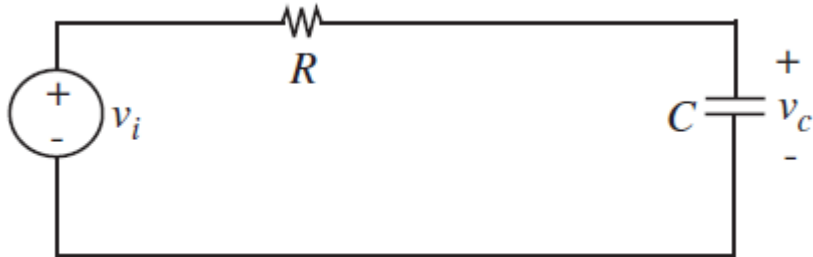
$$\bullet \hat{I} = \frac{5\angle 0}{10000 - 10000j}$$

$$\bullet 10000 - 10000j = 10000\sqrt{2}\angle \frac{-\pi}{4}$$

$$\bullet \text{So } \hat{I} = \frac{5\angle 0}{10000\sqrt{2}\angle \frac{-\pi}{4}} = \frac{1}{2000\sqrt{2}}\angle \frac{\pi}{4}$$



# Example



$$v_I = V_i \cos(\omega t), \quad t > 0$$

$$R = 10,000\Omega$$

$$C = 1\mu F$$

$$V_i = 5V$$

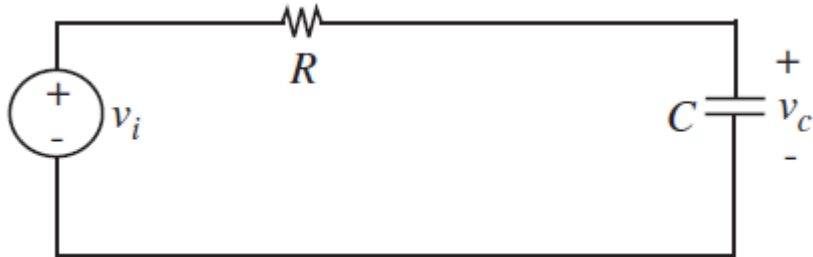
$$\omega = 100$$

Find  $i(t)$  in steady state

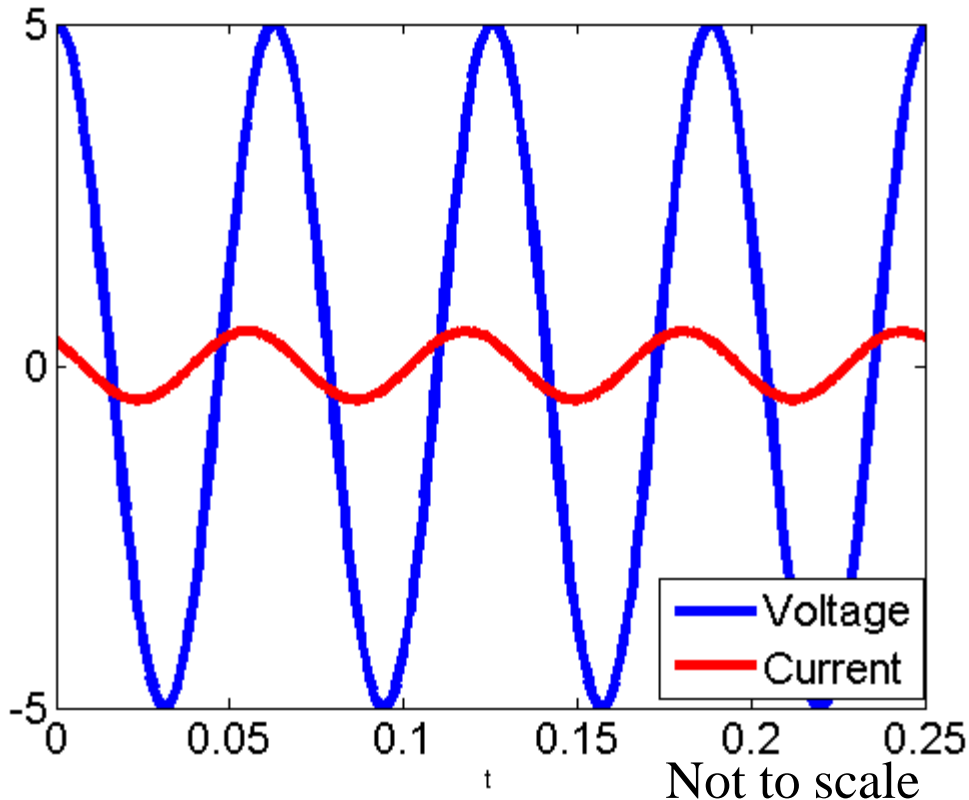
- $\hat{I} = \frac{1}{2000\sqrt{2}} \angle \frac{\pi}{4}$
- $i(t) = \frac{1}{2000\sqrt{2}} \cos(100t + \frac{\pi}{4})$  [in steady state]

# Example

$$v_I = V_i \cos(\omega t), \quad t > 0$$



$$i(t) = \frac{1}{2000\sqrt{2}} \cos(100t + \frac{\pi}{4})$$



- Current has same shape as voltage
- Current is  $10000\sqrt{2}$  times smaller than source voltage
- Current leads source voltage by  $\frac{\pi}{4}$  radians or  $\frac{\pi}{400}$  seconds

# Harder Example

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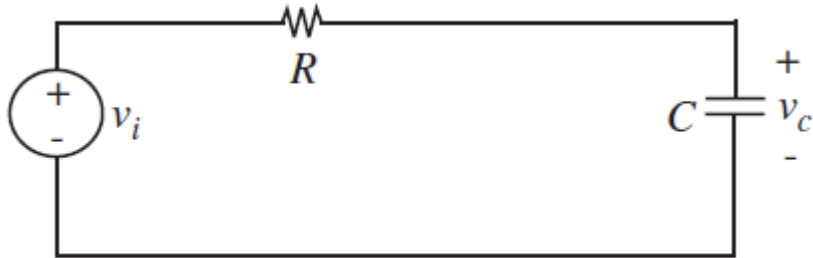
- On board

# Filters

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- Often, we'll want to build circuits which react differently based on different signal frequencies, e.g.
  - Splitting audio signals into low and high portions (for delivery to tweeter and subwoofer)
  - Removing noise of a particular frequency (e.g. 60 Hz noise or vuvuzela sound)
  - Removing signals except those at a certain frequency

# Example Filter



$$v_I = V_i \cos(\omega t), \quad t > 0$$

$$R = 10,000\Omega$$

$$C = 1\mu F$$

$$V_i = 5V$$

Find  $v_c(t)$  in steady state

$$\bullet \hat{V}_C = \frac{Z_C}{Z_C + Z_R} \hat{V}_I$$

$$Z_C = -10^6 j / \omega$$

$$Z_R = 10^5$$

$$\bullet \hat{V}_C = \frac{-10^6 j / \omega}{-10^6 j / \omega + 10^5} \hat{V}_I$$

$$\bullet \hat{V}_C = \frac{1}{1 + 0.1j\omega} \hat{V}_I$$

$\underbrace{\hspace{10em}}_{\text{Transfer Function } H(j\omega)}$

# Transfer Functions

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- $\hat{V}_C = \frac{1}{1+0.1j\omega} \hat{V}_I = H(j\omega) \hat{V}_I$
- Maps system input signal to system output signal
  - Plug an input voltage  $A \cos(\omega t + \phi)$  into  $\hat{V}_I$
  - Get an output voltage  $A |H(j\omega)| \cos(\omega t + \phi + \angle H(j\omega))$ 
    - Output is scaled and shifted in time
      - Scaling and shifting depend on frequency
    - Frequency is unchanged (linear system)
- Tells you how system will respond to any frequency, a.k.a. frequency response

# Using a Transfer Function

- $\hat{V}_C = \frac{1}{1+0.1j\omega} \hat{V}_I = H(j\omega) \hat{V}_I$
- Suppose  $v_i(t)$  is  $3\cos(50t + \frac{\pi}{4})$ 
  - $\hat{V}_I = 3\angle\frac{\pi}{4}$
  - $H(j50) = \frac{1}{1+5j}$
  - $|H(j50)| = 1/\sqrt{26}$
  - $\angle H(j50) = -\text{ArcTan}[5/1] = -1.37$
- Output phasor  $\hat{V}_C$  is just  $\hat{V}_I \times H(j50)$ 
  - $\hat{V}_C = \frac{3}{\sqrt{26}}\angle(\frac{\pi}{4} - 1.37)$
  - $v_c(t) = \frac{3}{\sqrt{26}}\cos(50t + \frac{\pi}{4} - 1.37)$

# Using a Transfer Function (general)

- $\hat{V}_C = \frac{1}{1+0.1j\omega} \hat{V}_I = H(j\omega) \hat{V}_I$
- Suppose  $v_i(t)$  is  $3\cos(\omega t + \frac{\pi}{4})$ 
  - $\hat{V}_I = 3 \angle \frac{\pi}{4}$
  - $H(j\omega) = \frac{1}{1+0.1j\omega}$
  - $|H(j\omega)| = 1/\sqrt{1+0.01\omega^2}$
  - $\angle H(j\omega) = -\text{ArcTan}[0.1\omega/1]$
- Output phasor  $\hat{V}_C$  is just  $\hat{V}_I \times H(j50)$ 
  - $\hat{V}_C = \frac{3}{\sqrt{1+0.01\omega^2}} \angle \left( \frac{\pi}{4} - \text{ArcTan} \left[ \frac{0.1\omega}{1} \right] \right)$
  - $v_c(t) = \frac{3}{\sqrt{1+0.01\omega^2}} \cos(50t + \frac{\pi}{4} - \text{ArcTan} \left[ \frac{0.1\omega}{1} \right])$

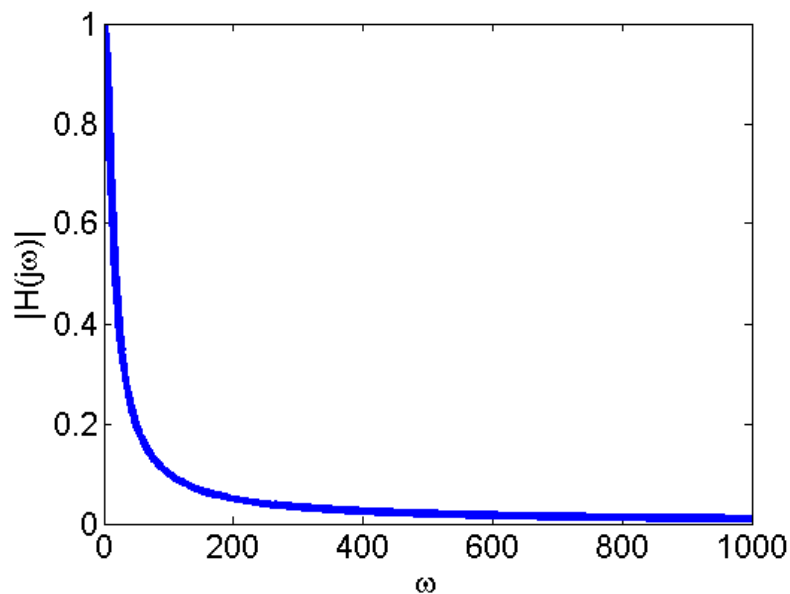


# Bode Magnitude Plot

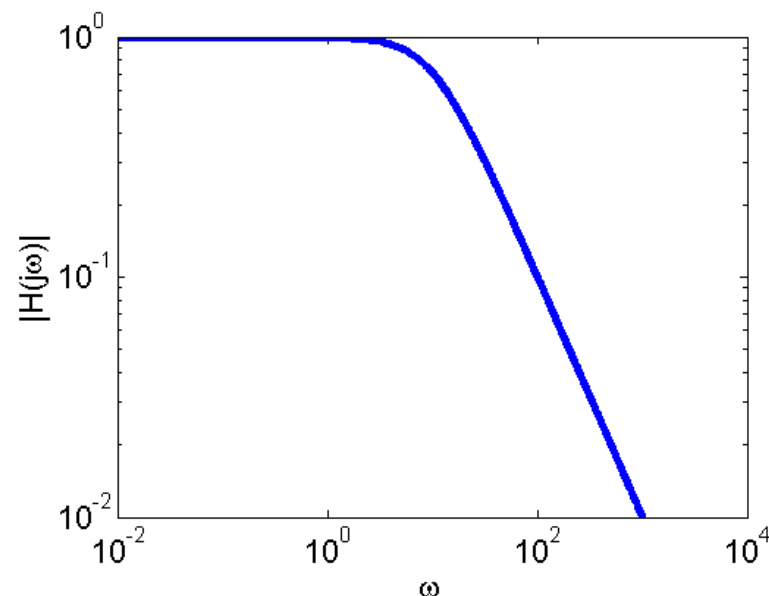
- $\hat{V}_C = \frac{1}{1+0.1j\omega} \hat{V}_I = H(j\omega) \hat{V}_I$

$$|H(j\omega)| = 1/\sqrt{1 + 0.01\omega^2}$$

- Magnitude plot is just a plot of  $|H(j\omega)|$  as a function of  $\omega$

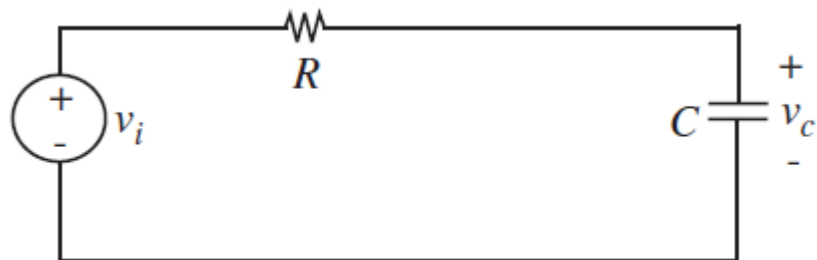


Linear Scale



Log Scale

# Bode Magnitude Plot in Context of Circuit



$$v_I = V_i \cos(\omega t), \quad t > 0$$

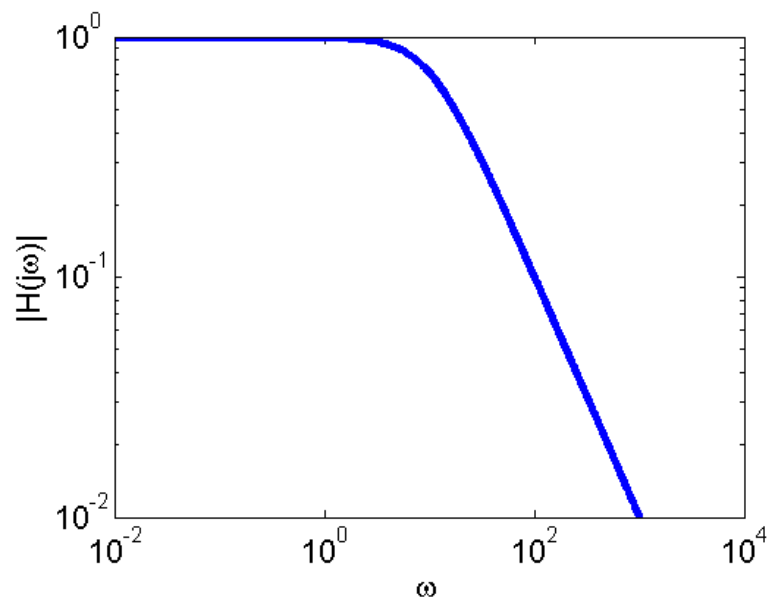
$$R = 10,000\Omega$$

$$C = 1\mu F$$

$$V_i = 5V$$

$$\hat{V}_C = \frac{1}{1 + 0.1j\omega} \hat{V}_I = H(j\omega) \hat{V}_I$$

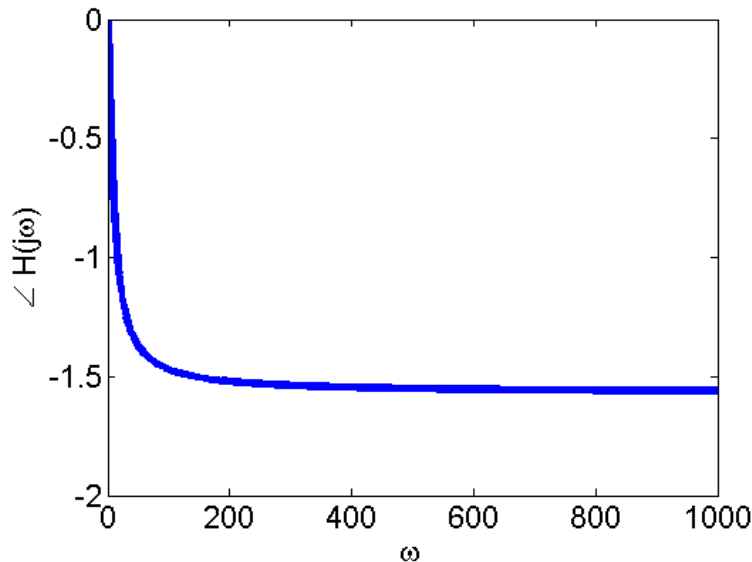
$$|H(j\omega)| = 1/\sqrt{1 + 0.01\omega^2}$$



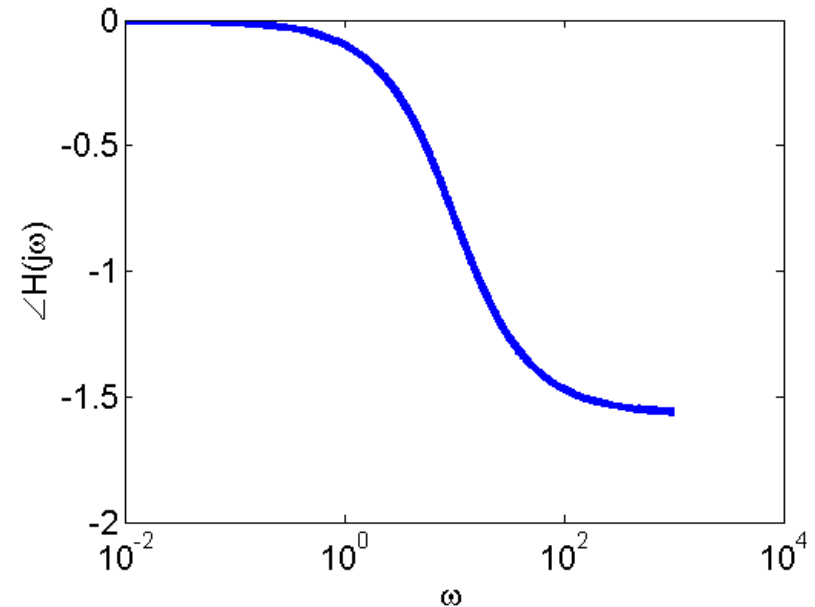
All frequencies below  $\omega_c = 10$  get through pretty well. Above, that increasingly attenuated

# Bode Phase Plot

- $\hat{V}_C = \frac{1}{1+0.1j\omega} \hat{V}_I = H(j\omega) \hat{V}_I$   
 $\angle H(j\omega) = -\text{ArcTan}[0.1\omega/1]$
- Phase plot is just a plot of  $\angle H(j\omega)$  as a function of  $\omega$

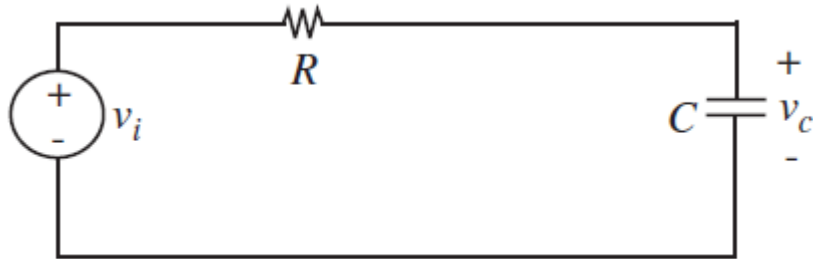


Linear Scale



Semilog Scale

# Bode Phase Plot in Context of Circuit

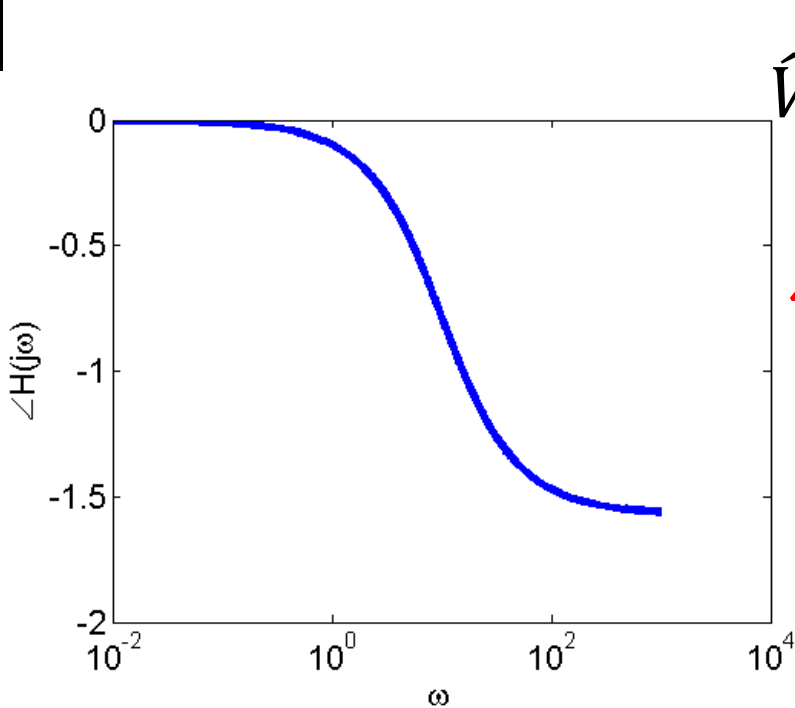


$$v_I = V_i \cos(\omega t), \quad t > 0$$

$$R = 10,000\Omega$$

$$C = 1\mu F$$

$$V_i = 5V$$



$$\hat{V}_C = \frac{1}{1 + 0.1j\omega} \hat{V}_I = H(j\omega) \hat{V}_I$$

$$\angle H(j\omega) = -\text{ArcTan}[0.1\omega/1]$$

All frequencies below  $\omega_c = 10$  move in time with the source, above that,  $v_c$  gets out of phase

# Frequency vs. Time Domain

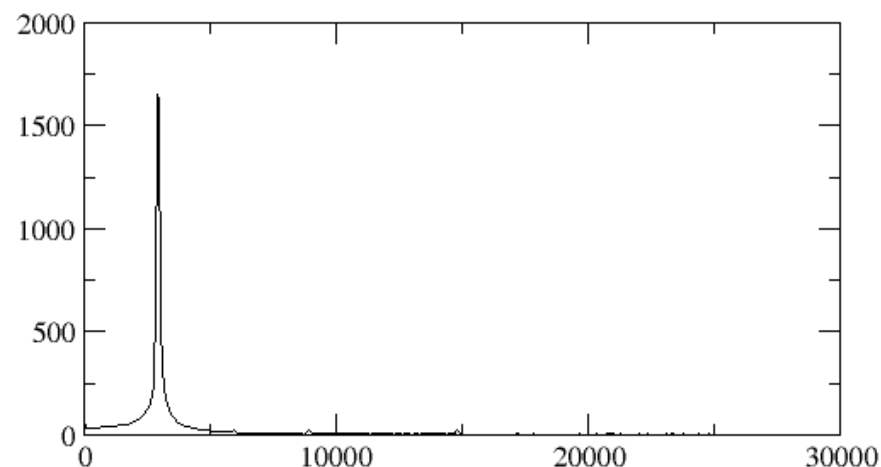
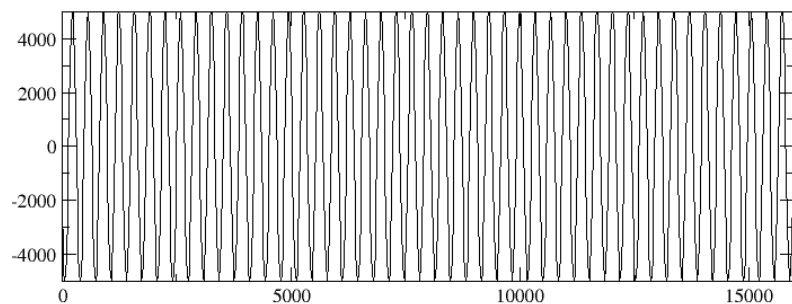
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- Almost always, our signals consist of multiple frequencies
- Examples:
  - Sound made when you press a buttons on a phone is two pure sine waves added together (DTMF)
  - Antennas on radio theoretically pick up ALL frequencies of ALL transmissions
- Using a technique known as the Fourier Transform, we can convert any signal into a sum of sinusoids
  - See EE20 for more details

# Fourier Transform Example

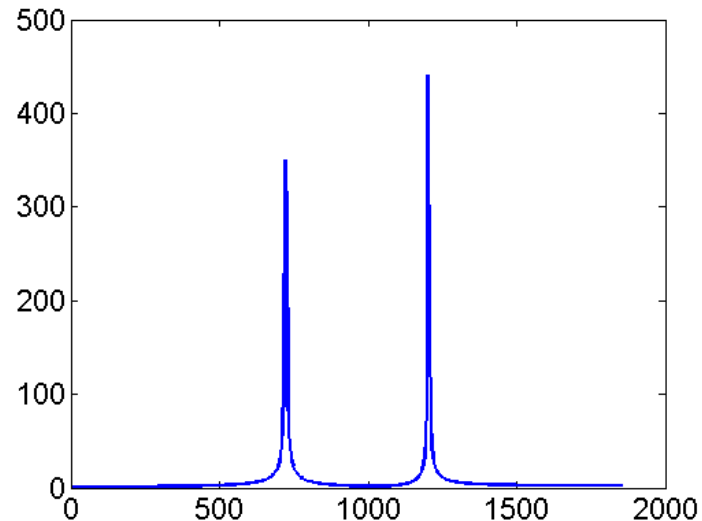
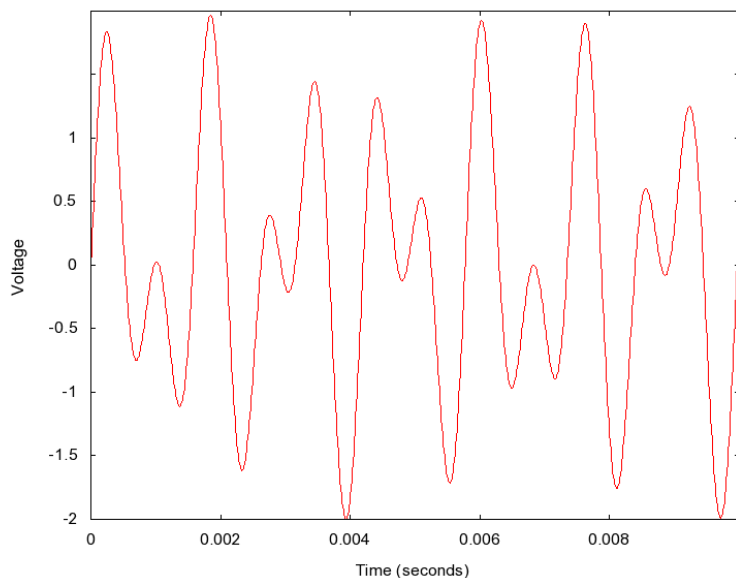
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- If someone whistles a signal that is approximately  $\sin(3000t)$ , and we apply the Fourier Transform, then:



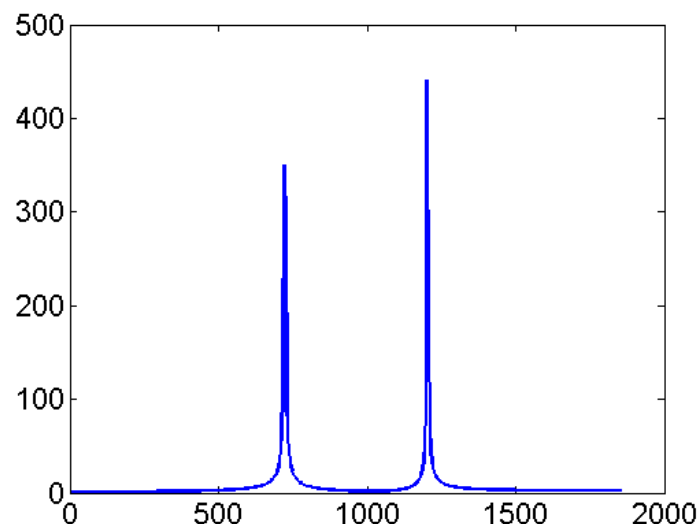
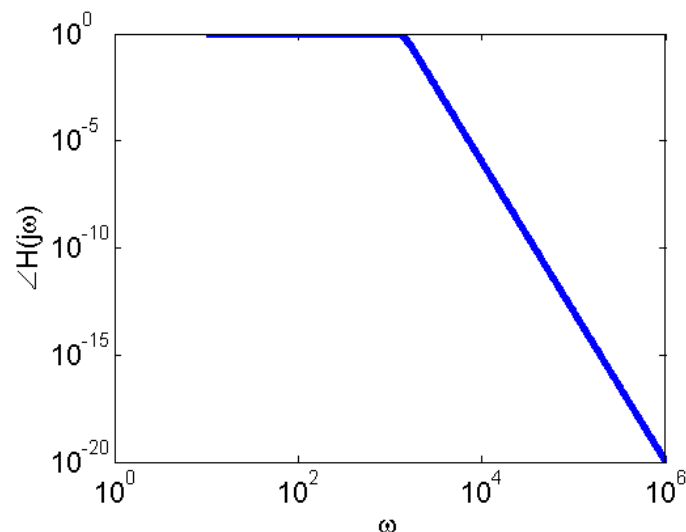
# Fourier Transform Example

- The 1 button on a phone is just  $v(t) = \sin\left(\frac{697}{2\pi} t\right) + \sin\left(\frac{1209}{2\pi} t\right)$

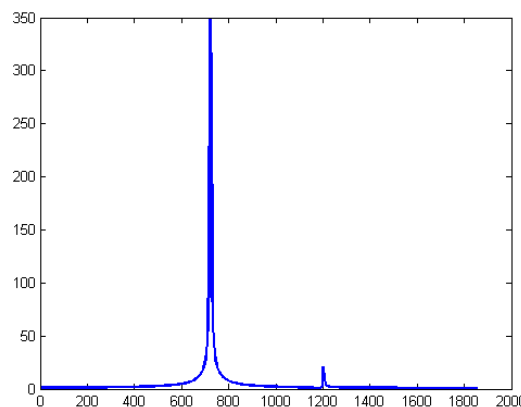


# Fourier Transform Example

- If we apply a filter with the frequency response on the left to the signal on the right



Then we'll get:





# Types of Filters

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- **Passive Filters**
  - Filters with no sources (i.e. just R, L, and C)
  - Don't require power source
  - Scale to larger signals (no op-amp saturation)
  - Cheap
- **Active Filters**
  - Filters with active elements, e.g. op-amps
  - More complex transfer function
    - No need for inductors (can be large and expensive, hard to make in integrated circuits)
    - More easily tunable
  - Response more independent of load (buffering)

# Filter Examples

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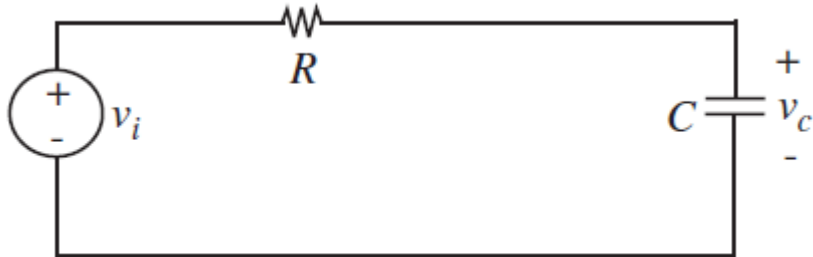
- On board

# Manually Plotting

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- In this day and age, it is rarely necessary to make our Bode plots manually
- However, learning how to do this will build your intuition for what a transfer function means
- Manual plotting of bode plots is essentially a set of tricks for manually plotting curves on a loglog axis
- We will only teach a subset of the full method (see EE20 for a more thorough treatment)

# Example Filter



$$v_I = V_i \cos(\omega t), \quad t > 0$$

$$R = 10,000\Omega$$

$$C = 1\mu F$$

$$V_i = 5V$$

Find  $v_c(t)$  in steady state

- $\hat{V}_C = \frac{1}{1+0.1j\omega} \hat{V}_I$
- $\hat{V}_C = \frac{1}{\sqrt{1+0.01\omega^2} \angle \text{ArcTan}[0.1\omega]} \hat{V}_I$
- $\hat{V}_C = \frac{1}{\sqrt{1+0.01\omega^2}} \angle -\text{ArcTan}[0.1\omega] \hat{V}_I$
- Intuitive plot on board
- More thorough algorithm next time

# Extra Slides

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# Why do equivalent Impedances work?

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- Components with memory just integrate or take the derivative of  $e^{q_1 t}$ , giving scaled versions of the same function
  - This is unlike forcing functions like  $t^3$  or  $\cos(\omega t)$
  - This allows us to divide by the source, eliminating  $t$  from the problem completely
  - Left with an algebra problem
  - [For those of you who have done integral transforms, this whole process can be thought of as just using Laplace/Fourier transforms]