

Lecture 8

- * Solving systems of diff. eqns with Phasors
 - * i.e. transforming systems of diff. eqns into sys. of lin. eqns.
-

$$(1) \quad \frac{d}{dt} \vec{x}(t) = A \vec{x}(t) + \vec{u}(t)$$

Let's consider the inputs of the form $\sim e^{st}$ and assert that the solutions are $\sim e^{st}$, valid for $s \neq \lambda$, $\text{Re}(\lambda) = \lambda_r < 0$ in steady-state.

$$\vec{u}(t) = \vec{\hat{u}} e^{st}, \quad \vec{\hat{u}} \text{ vector of constants}$$

Assert: $\vec{x}(t) = \vec{\hat{x}} e^{st}$, $\vec{\hat{x}}$ vector of constants

$$\frac{d}{dt} \vec{x}(t) = \frac{d}{dt} (\vec{\hat{x}} e^{st}) = \vec{\hat{x}} \frac{d}{dt} e^{st} = s \vec{\hat{x}} e^{st}$$

From (1) $s \vec{\hat{x}} e^{st} = A \vec{\hat{x}} e^{st} + \vec{\hat{u}} e^{st}$

$$s \vec{\hat{x}} = A \vec{\hat{x}} + \vec{\hat{u}}$$

$$(2) \quad (sI - A) \vec{\hat{x}} = \vec{\hat{u}}$$

System of lin. equations.

$$\vec{\hat{x}} = (sI - A)^{-1} \cdot \vec{\hat{u}}$$

Remember $s \neq \lambda$
 $sI - A$ has no nullspace & is therefore

$$\vec{x}(t) = \vec{\hat{x}} \cdot e^{st}$$

invertible

$$\vec{x}(t) = (sI - A)^{-1} \vec{u} \cdot e^{st}$$

solution
to (1) for
 $\vec{u}(t) = \vec{u} e^{st}$

Can we use this for cbs directly?

$$C \begin{cases} \downarrow I(t) \\ + \\ \uparrow V(t) \\ - \end{cases}$$

$$I(t) = C \frac{d}{dt} V(t)$$

$$I(t) = \hat{I} e^{st}$$

$$V(t) = \hat{V} e^{st}$$

$$\left. \begin{array}{l} V(t) = \hat{V} \\ I(t) = \hat{I} \end{array} \right\}$$

$$I(t) = \hat{I} e^{st} = C \frac{d}{dt} (\hat{V} e^{st}) = C \hat{V} \frac{d}{dt} (e^{st})$$

$$\hat{I} e^{st} = s C \hat{V} e^{st}$$

$$= s C \hat{V} e^{st}$$

$$\frac{\hat{V}}{\hat{I}} = \frac{1}{sC}$$

(capacitor
s-impedance)

$$R \begin{cases} \downarrow I(t) \\ + \\ \uparrow V(t) \\ - \end{cases}$$

$$V(t) = \hat{V} e^{st}$$

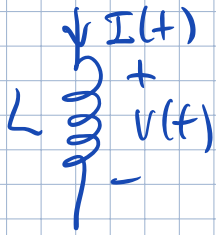
$$I(t) = \hat{I} e^{st}$$

$$V(t) = R \cdot I(t)$$

$$\hat{V} e^{st} = R \hat{I} e^{st}$$

$$\frac{\hat{V}}{\hat{I}} = R$$

(resistor
s-impedance)



$$v(t) = L \frac{d}{dt} i(t)$$

$$v(t) = \hat{v} e^{st}$$

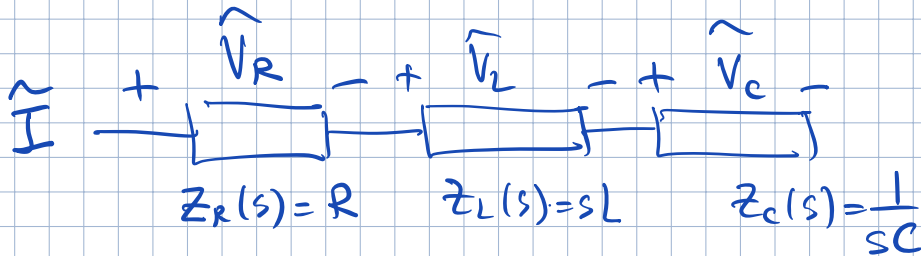
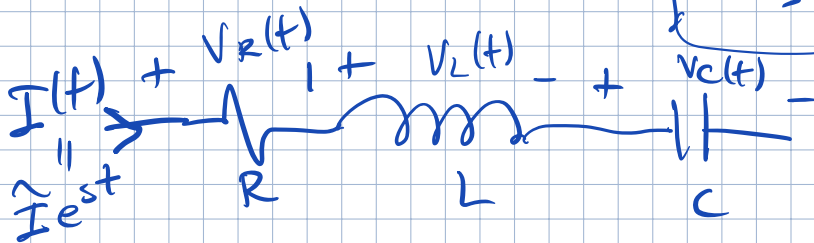
$$i(t) = \hat{i} e^{st}$$

$$\hat{v} e^{st} = L \frac{d}{dt} (\hat{i} e^{st}) = L \hat{i} \frac{d}{dt} (e^{st})$$

$$\hat{v} e^{st} = sL \hat{i} e^{st}$$

$$\hat{v} = sL \hat{i} \Rightarrow \frac{\hat{v}}{\hat{i}} = sL$$

inductor
s-impedance



$$\hat{V}_R = \hat{I} \cdot Z_R, \quad \hat{V}_L = \hat{I} \cdot Z_L, \quad \hat{V}_C = \hat{I} \cdot Z_C$$

$$v_R(t) = \hat{V}_R e^{st}, \quad \dots$$

For sinusoidal inputs :

$$u(t) = U \cos(\omega t + \phi) = U \frac{e^{j(\omega t + \phi)} + e^{-j(\omega t + \phi)}}{2}$$

$$u(t) = \frac{U \cdot e^{j\phi}}{2} \cdot e^{j\omega t} + \frac{U e^{-j\phi}}{2} \cdot e^{-j\omega t}$$

$$\underbrace{\frac{U \cdot e^{j\phi}}{2}}_{\hat{u}} \cdot \underbrace{e^{j\omega t}}_{e^{s_1 t}} + \underbrace{\frac{U e^{-j\phi}}{2}}_{\bar{u}} \cdot \underbrace{e^{-j\omega t}}_{e^{s_2 t}}$$

$s_1 = j\omega$ $s_2 = -j\omega$
always complex conjugates
b/c $u(t)$ is real

$$u(t) = \hat{u} e^{j\omega t} + \bar{u} e^{-j\omega t}$$

Use superposition to solve for the first & second component.

For $s_1 = j\omega$: $M = s_1 I - A = j\omega I - A$

$$M \vec{x} = \vec{u}$$

$$\vec{x} = M^{-1} \vec{u}$$

element voltages & currents $\rightarrow \begin{bmatrix} \vec{i} \\ \vec{v} \end{bmatrix} = M^{-1} \vec{u} \leftarrow \text{independent sources}$
 \uparrow
circuit topology

For $s_2 = -j\omega$ $\bar{M} = s_2 I - A = -j\omega I - A$

$$\bar{M} \begin{bmatrix} \overrightarrow{V} \\ \overrightarrow{I} \end{bmatrix} = \overrightarrow{u} \quad \overline{M \vec{x}} = \bar{M} \vec{x}$$

$$\begin{bmatrix} \overrightarrow{V} \\ \overrightarrow{I} \end{bmatrix} = \begin{bmatrix} \overrightarrow{V} \\ \overrightarrow{I} \end{bmatrix} = \bar{M}^{-1} \cdot \overrightarrow{u} = \overline{M^{-1} \vec{x}}$$

$$\begin{bmatrix} \overrightarrow{V} \\ \overrightarrow{I} \end{bmatrix} = M^{-1} \overrightarrow{u}$$

all solutions:

$$\overrightarrow{V}(t) = \overrightarrow{V} e^{j\omega t} + \overrightarrow{V} e^{j\omega t}$$

$$\overrightarrow{I}(t) = \overrightarrow{I} e^{j\omega t} + \overrightarrow{I} e^{j\omega t}$$

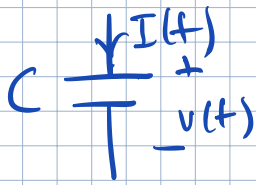
so only need to find one (i.e. $\overrightarrow{V}, \overrightarrow{I}$)
to compute $\overrightarrow{V}(t)$ & $\overrightarrow{I}(t)$

For sinusoidal inputs:

\overrightarrow{V} and \overrightarrow{I} are phasors (functions of $s = j\omega$)

s -impedances are called impedances

Phasors turn 16B problems into 16A problems!



$$v(t) = V_0 \cos(\omega t + \phi)$$

$$v(t) = \underbrace{\frac{V_0}{2} e^{j\phi}}_{\hat{v}} e^{j\omega t} + \underbrace{\frac{V_0}{2} e^{-j\phi}}_{\hat{\bar{v}}} e^{-j\omega t}$$

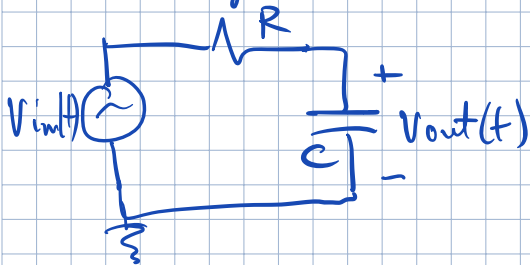
$$I(t) = C \frac{d}{dt} v(t) = C \frac{d}{dt} (\hat{v} e^{j\omega t} + \hat{\bar{v}} e^{-j\omega t})$$

$$= \underbrace{j\omega C \hat{v} e^{j\omega t}}_{\hat{I}} + \underbrace{(-j\omega) C \hat{\bar{v}} e^{-j\omega t}}_{\hat{\bar{I}}}$$

$$I(t) = \hat{I} e^{j\omega t} + \hat{\bar{I}} e^{-j\omega t}$$

$$\hat{I} = j\omega C \hat{v} \Rightarrow \boxed{Z_C(s=j\omega) = \frac{1}{j\omega C}}$$

Example 1: RC circuit



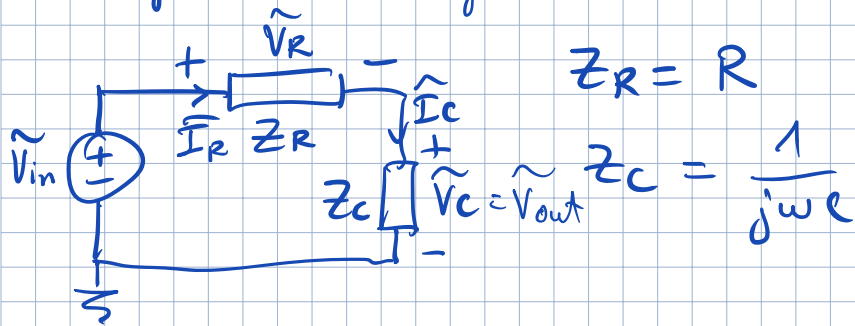
$$v_{in}(t) = V_{in} \cos(\omega t + \phi)$$

$$v_{out}(t) = ?$$

step 1: Write the sources as exponentials

$$v_{in}(t) = \underbrace{\frac{V_{in}}{2} e^{j\phi}}_{\hat{v}_{in}} e^{j\omega t} + \underbrace{\frac{V_{in}}{2} e^{-j\phi}}_{\hat{\bar{v}}_{in}} e^{-j\omega t}$$

step 2: Transform the circuit to phasor domain



step 3: Write down the circuit equations

$$\hat{V}_R = Z_R \hat{I}_R, \quad \hat{V}_C = \hat{I}_C \cdot Z_C$$

KCL: $\hat{I}_R = \hat{I}_C$

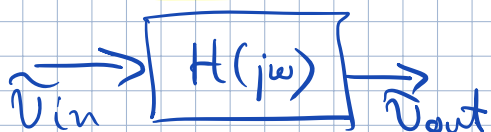
step 4: Solve the circuit

$$\hat{V}_C = \frac{Z_C}{Z_C + Z_R} \cdot \hat{V}_{in} = \frac{j\omega C}{\frac{1}{j\omega C} + R} \hat{V}_{in}$$

$$\hat{V}_C = \hat{V}_{out} = \frac{1}{1 + j\omega RC} \hat{V}_{in}$$

Note

$$\hat{V}_{out}(j\omega) = \frac{1}{1 + j\omega RC} \hat{V}_{in}(j\omega)$$



$$H(j\omega) = \frac{\hat{V}_{out}(j\omega)}{\hat{V}_{in}(j\omega)}$$

For our LP example: transfer function

$$H_{LP}(j\omega) = \frac{1}{1+j\omega RC} = \frac{1-j\omega RC}{1+(\omega RC)^2}$$

$$|H(j\omega)| = \frac{1}{|1+j\omega RC|} = \frac{1}{\sqrt{1+(\omega RC)^2}}$$

$$\Rightarrow H(j\omega) = -\text{atan2}(\omega RC, 1)$$

$$\hat{V}_{out} = H(j\omega) \cdot \hat{V}_{in}$$

$$\hat{V}_{in} = |\hat{V}_{in}| e^{j\hat{\varphi}_{in}}$$

$$\hat{V}_{out} = |\hat{V}_{out}| e^{j\hat{\varphi}_{out}}$$

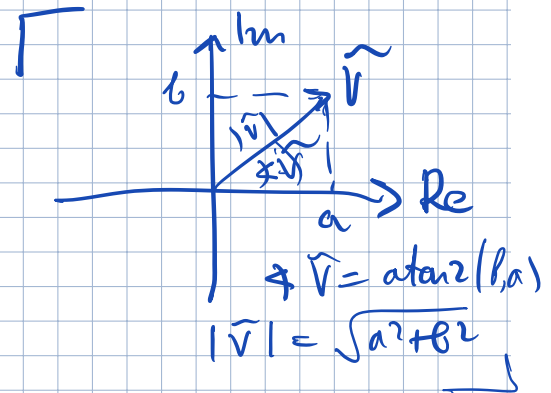
$$H(j\omega) = |H(j\omega)| e^{j\hat{\varphi}_{H(j\omega)}}$$

$$\hat{V}_{out} = |\hat{V}_{out}| e^{j\hat{\varphi}_{out}} = |\hat{V}_{in}| e^{j\hat{\varphi}_{in}} \cdot |H(j\omega)| e^{j\hat{\varphi}_{H(j\omega)}}$$

$$|\hat{V}_{out}| e^{j\hat{\varphi}_{out}} = |\hat{V}_{in}| \cdot |H(j\omega)| \cdot e^{j(\hat{\varphi}_{in} + \hat{\varphi}_{H(j\omega)})}$$

$$|\hat{V}_{out}| = |H(j\omega)| |\hat{V}_{in}|$$

$$\hat{\varphi}_{out} = \hat{\varphi}_{H(j\omega)} + \hat{\varphi}_{in}$$



$$|H_{LP}(j\omega)| = \frac{1}{\sqrt{1+(\omega RC)^2}} \rightarrow 1 \text{ as } \omega \rightarrow 0$$

i.e. a low-pass filter

$\rightarrow 0$ as $\omega \rightarrow \infty$

i.e. $\omega \ll \frac{1}{RC}$

$\omega \gg \frac{1}{RC}$

step 5: Convert to time domain,

$$V_{out}(t) = \widehat{V}_{out} e^{j\omega t} + \overline{\widehat{V}_{out}} e^{-j\omega t}$$

$$= |\widehat{V}_{out}| e^{j\phi_{\widehat{V}_{out}}} e^{j\omega t} + |\widehat{V}_{out}| e^{-j\phi_{\widehat{V}_{out}}} e^{-j\omega t}$$

$$= |\widehat{V}_{out}| e^{j(\omega t + \phi_{\widehat{V}_{out}})} + |\widehat{V}_{out}| e^{-j(\omega t + \phi_{\widehat{V}_{out}})}$$

$$= 2 |\widehat{V}_{out}| \cos(\omega t + \phi_{\widehat{V}_{out}})$$

similarly: $V_{in}(t) = 2 |\widehat{V}_{in}| \cos(\omega t + \phi_{\widehat{V}_{in}})$

$\underbrace{\quad}_{V_{in}} \quad \underbrace{\quad}_{\phi}$

$$V_{out}(t) = 2 \cdot |H_{LP}(j\omega)| \cdot |\widehat{V}_{in}| \cdot \cos(\omega t + \phi_{H_{LP}(j\omega)} + \phi_{\widehat{V}_{in}})$$

$$= \frac{1}{\sqrt{1+(\omega RC)^2}} \cdot V_{in} \cos(\omega t + \underbrace{\phi_{H_{LP}(j\omega)}}_{-\arctan(\omega RC)} + \underbrace{\phi_{\widehat{V}_{in}}}_{\phi})$$

┌ what is the phase?

$$\omega \cdot t_d = \angle H(j\omega), \quad t_d = \frac{\angle H(j\omega)}{\omega}$$

↑ delay