

Ideal: $\frac{V_o}{V_i} = \frac{-1}{s\tau}$

finite A:

$$\frac{V_i}{R} - \frac{V_x}{R} + V_o sC - V_x sC = 0 \quad V_x = \frac{-V_o}{A}$$

$$V_i \left(\frac{1}{R} \right) = -V_o \left(\frac{1}{AR} + sC + \frac{sC}{A} \right)$$

$$\frac{V_o}{V_i} = - \frac{1}{\frac{1}{A} + sRC \left(1 + \frac{1}{A} \right)}$$

$$= - \frac{1}{\tau} \frac{1}{s \left(1 + \frac{1}{A} \right) + \frac{1}{\tau A}}$$

$$\Rightarrow s \rightarrow \underbrace{s \left(1 + \frac{1}{A} \right)}_B + \frac{1}{\tau A}$$

$$s \rightarrow sB + \frac{1}{\tau A}$$

Filter: $H \left(sB + \frac{1}{\tau A} \right) \Big|_{s = \text{pachal}} \rightarrow \infty$

$$P_{ideal} = -\alpha_i \pm j\beta_i$$

$$P_{actual} = -\alpha_a \pm j\beta_a$$

$$P_{ideal} = B \cdot P_{actual} + \frac{1}{TA}$$

$$\Rightarrow \alpha_i = B\alpha_a + \frac{1}{TA}$$

$$\beta_i = B\beta_a$$

$$\Rightarrow \alpha_a = \frac{\alpha_i - \frac{1}{TA}}{B} \quad \parallel \quad B = 1 + \frac{1}{A}$$

$$\beta_a = \frac{\beta_i}{B}$$

$$\tau = RC$$

$$A \equiv A_{vo}$$

effect on Q:

$$Q_a \approx \frac{1}{2} \frac{\beta_a}{\alpha_a} = \frac{1}{2} \frac{\beta_i}{\alpha_i - \frac{1}{TA}} = Q_i \left(\frac{1}{1 + \frac{1}{\tau \alpha_i A_{vo}}} \right)$$

with: $\alpha_i = \frac{\omega_0}{2Q_i}$ and $\tau \approx \frac{1}{\omega_0}$

$$\Rightarrow Q_a = Q_i \frac{1}{1 + \frac{2Q}{A}} \approx \boxed{Q_i \left(1 - \frac{2Q}{A} \right)}$$

e.g.: $Q_i = 10, A_{vo} = 100$

$$\Rightarrow Q_a \approx 10 \left(1 - \frac{20}{100} \right) = \underline{\underline{8}}$$

$$\frac{\Delta Q}{Q} = \underline{\underline{-20\%}}$$

effect on ω_0 :

$$\omega_{oa} = \sqrt{\alpha_a^2 + \beta_a^2}$$

$$\omega_{oa}^2 = \frac{1}{B^2} \left[\left(\alpha_i + \frac{1}{TA} \right)^2 + \beta_i^2 \right]$$

$$= \frac{1}{B^2} \left[\alpha_i^2 + \beta_i^2 + 2\alpha_i \frac{1}{TA} + \left(\frac{1}{TA} \right)^2 \right]$$

say $T \cong \frac{1}{\omega_0}$; $\alpha_i = \frac{\omega_{oi}}{2Q_i}$

$$= \frac{1}{\left(1 + \frac{1}{A}\right)^2} \left[\omega_{oi}^2 + \frac{\omega_{oi}^2}{AQ_i} + \frac{\omega_{oi}^2}{A^2} \right]$$

$$\cong \omega_{oi}^2 \left(1 - \frac{2}{A} \right) \left(1 + \frac{1}{AQ_i} + \frac{1}{A^2} \right)$$

$A^2 \gg AQ_i \gg \frac{A}{2}$ usually

$$\omega_{oa} \cong \omega_{oi} \sqrt{1 - \frac{2}{A}}$$

e.g.: $A = 100$

$$\Rightarrow \frac{\omega_{oa}}{\omega_{oi}} = \sqrt{1 - \frac{2}{100}} = \underline{\underline{0.99}}$$

$$\frac{\Delta \omega_0}{\omega_0} \cong \underline{\underline{-1\%}} \quad (\text{only})$$

② a) I decided to use the following design flow:

Synthesize w/ Matlab in
z-domain

Break up into Biquads
using "tf2sos"

estimate Biquad Q s,
use inverse bilin.
transform

$$s_p = \frac{z}{T} \left(\frac{z_p - 1}{z_p + 1} \right)$$

$$\Rightarrow \left. \begin{array}{l} Q_1 = 0.61 \\ Q_2 = 0.16 \\ Q_3 = 6.3 \end{array} \right\} \begin{array}{l} \text{"Low Q"} \\ \text{"Hi Q"} \end{array} \quad (>3)$$

Implement using H_i - and
 L_o Q circuits as given in
Gregorian & Temes pp. 280.

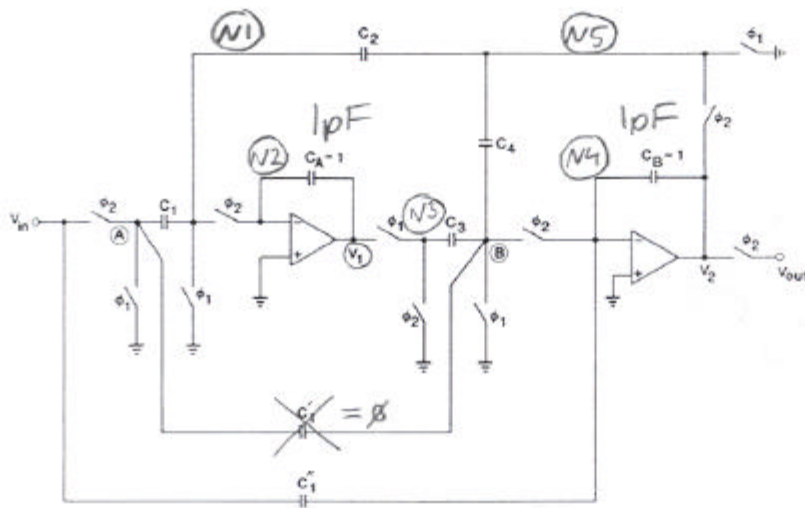
→ see attached schematics
with design equations

$$F_{\text{pass}} = 2 \cdot \frac{1 \text{ MHz}}{10 \text{ MHz}} = 0.2$$

$$F_{\text{slop}} = 2 \cdot \frac{1.5 \text{ MHz}}{10 \text{ MHz}} = 0.3$$

$$\Rightarrow \text{ellipord}(\dots) = \boxed{6}$$

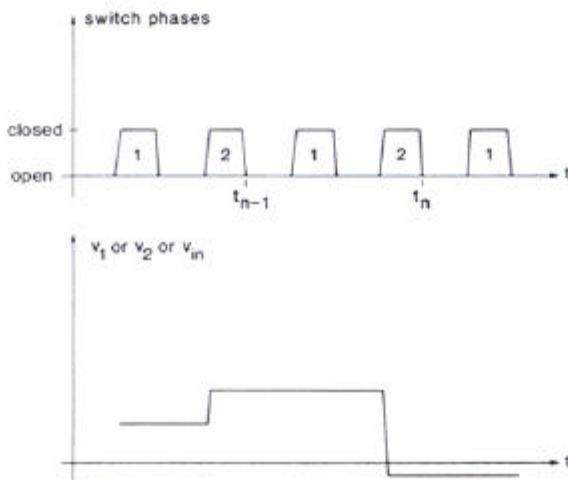
(filter order)



(c)

LoQ

$$H(z) = \frac{a_2 z^2 + a_1 z + a_0}{b_2 z^2 + b_1 z + b_0}$$



(d)

FIGURE 5.10. continued.

$$C_1'' = a_0$$

$$C_1' = a_2 - a_0$$

$$C_1 = \frac{a_0 + a_1 + a_2}{C_3}$$

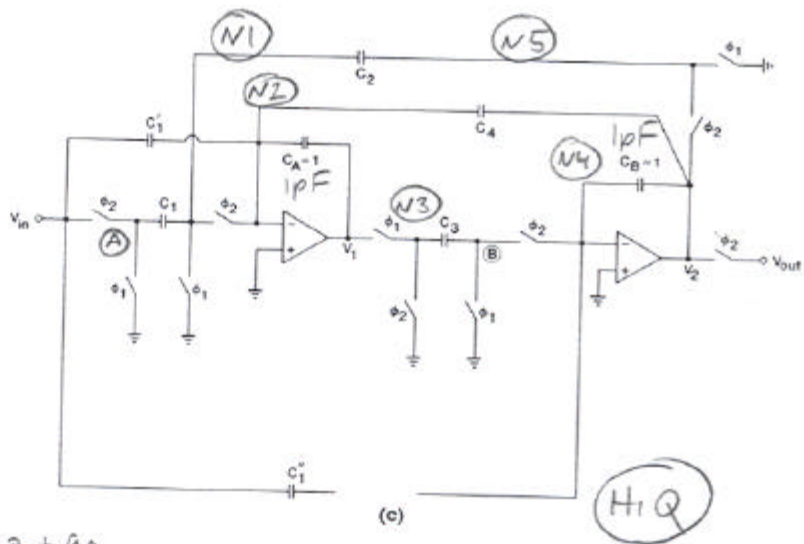
$$C_4 = b_2 - 1$$

$$C_2 C_3 = b_1 + b_2 + 1$$

ut

zation:

.10a.
le its
y an
on is
e the
input
rents
smitt-
d by
 f_{in}
value



$$H(z) = \frac{a_2 z^2 + a_1 z + a_0}{b_2 z^2 + b_1 z + b_0}$$

$$C_1^{II} = \frac{a_2}{b_2}$$

$$C_1^I = \frac{a_2 - a_0}{b_2 C_3}$$

$$C_1 = \frac{a_0 + a_1 + a_2}{b_2 C_3}$$

$$C_4 = \frac{1 - 1/b_2}{C_3}$$

$$C_2 C_3 = \frac{1 + b_1 + b_2}{b_2}$$

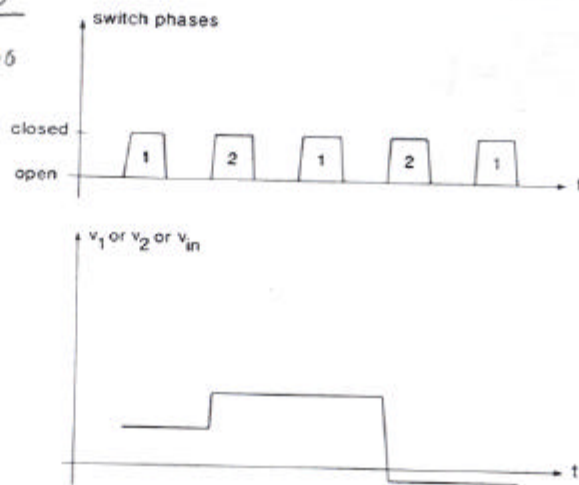


FIGURE 5.13. continued.

2) b) Poles and Zeros

Biquad 1:

Z1 =
-4.959483412658553e-001 +8.683520270003670e-001i
-4.959483412658553e-001 -8.683520270003670e-001i
P1 =
7.127856685302593e-001 +1.653876720637911e-001i
7.127856685302593e-001 -1.653876720637911e-001i

Biquad 2:

Z2 =
3.825418155817085e-001 +9.239381793883470e-001i
3.825418155817085e-001 -9.239381793883470e-001i
P2 =
7.246789558726074e-001 +4.320114746276476e-001i
7.246789558726074e-001 -4.320114746276476e-001i

Biquad 3:

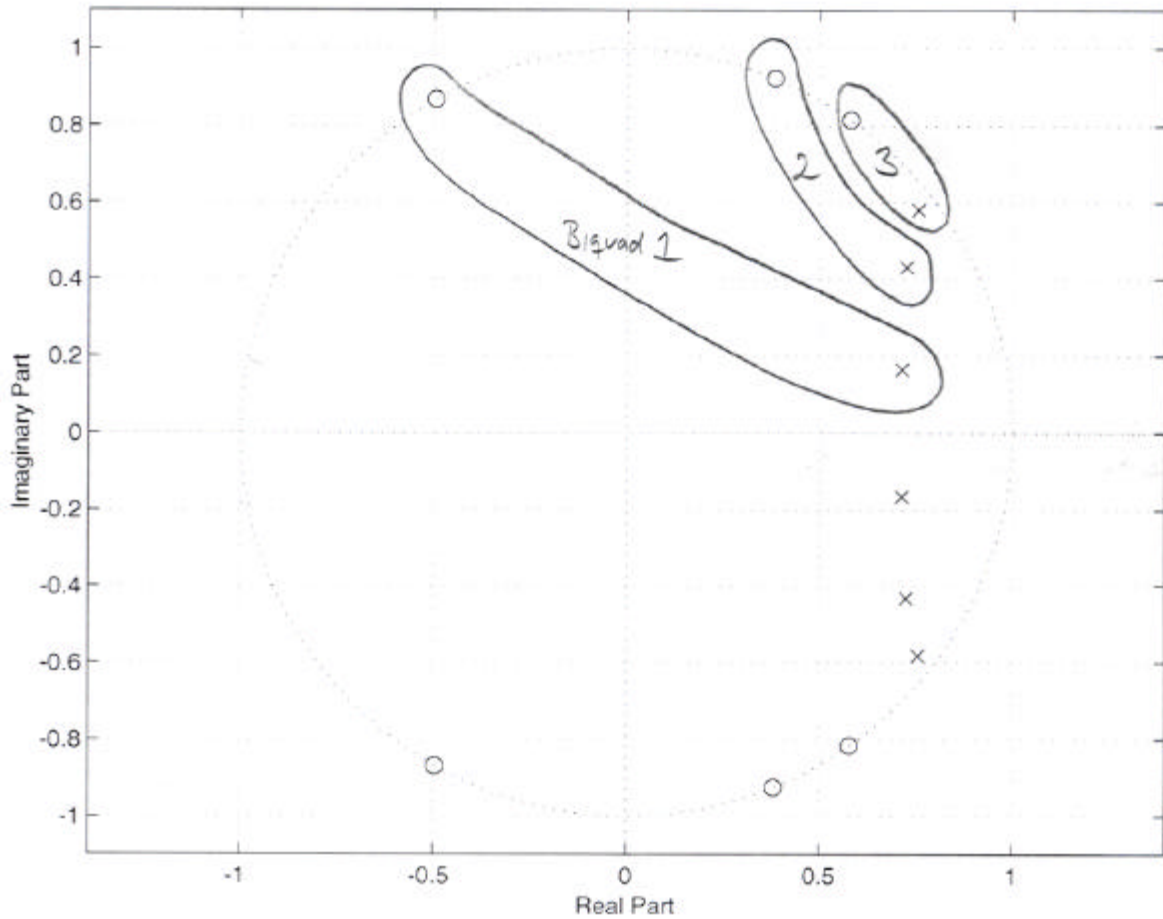
Z3 =
5.785179590177820e-001 +8.156696458088302e-001i
5.785179590177820e-001 -8.156696458088302e-001i
P3 =
7.553705109318878e-001 +5.808504547226241e-001i
7.553705109318878e-001 -5.808504547226241e-001i

(Grouping done by Matlab "tf2sos"
→ see next page)

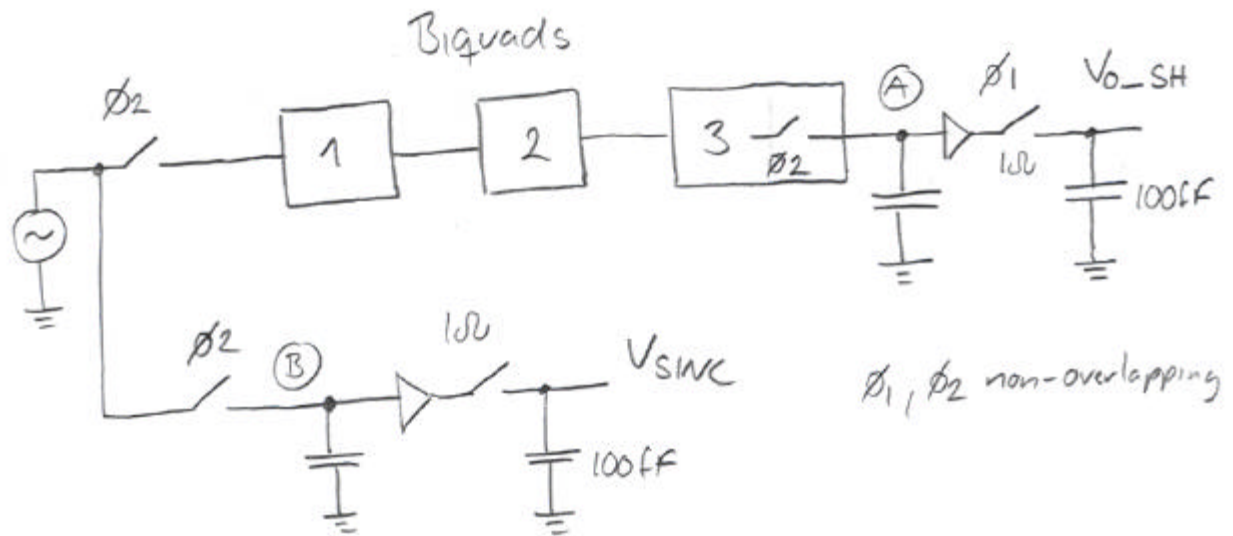
(2) b)

p/z grouping by Matlab:

(ⁿMinimum sensitivity to coefficient tolerances,
see e.g. Oppenheim & Schaffer)



② ③ Top Schematic:



→ ①, ② are "track and hold nodes", the held value is transferred with ϕ_1 to form an "ideal" staircase voltage \equiv Dirac sampling with falling edge of ϕ_2

→ V_{SINC} will be used in the post processor to eliminate sinc distortion.

$$V_{O_SH} [dB] - V_{SINC} [dB] \Rightarrow \text{actual discrete time response}$$

→ Biquads scaled in Matlab using:

$$\frac{\sum a}{\sum b} \stackrel{!}{=} 1 \quad \text{in} \quad \frac{a_2 z^2 + a_1 z + a_0}{b_2 z^2 + b_1 z + b_0} \quad z \rightarrow 1 \text{ @ DC}$$

(see Matlab script)

→ Good agreement w/ Spectre simulation, see Plots 1, 2

(2) d)

found: $A_{\min} \approx \underline{1200}$ for $R_p = 0.12 \text{ dB}$,
assuming f_{corner} is allowed to shift
 $\approx \frac{8 \text{ kHz}}{1 \text{ MHz}} = 0.8 \%$

→ Stopband attenuation appears to be
insensitive to low gain / gain variations.

→ See plots 3, 4

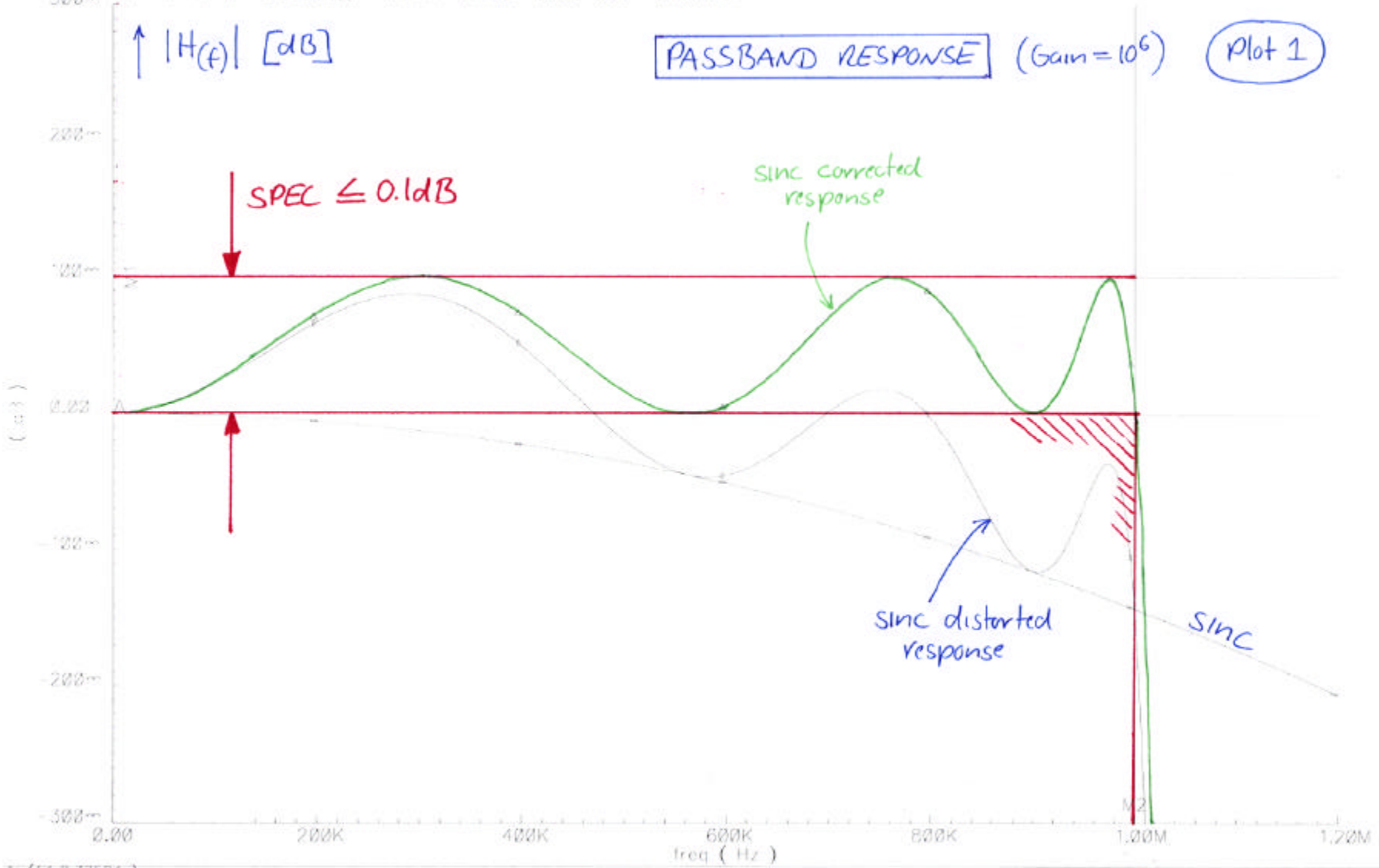
```
Δ: (wavew12s1i1() - wavew12s1i2())
```

```
=: harmonic="0";dB20((v "vsinc" ?result "pac2-pac" ?resultsD)
```

```
∴ harmonic="0";dB20((v "vo_sfr" ?result "pac2-pac" ?resultsD)
```

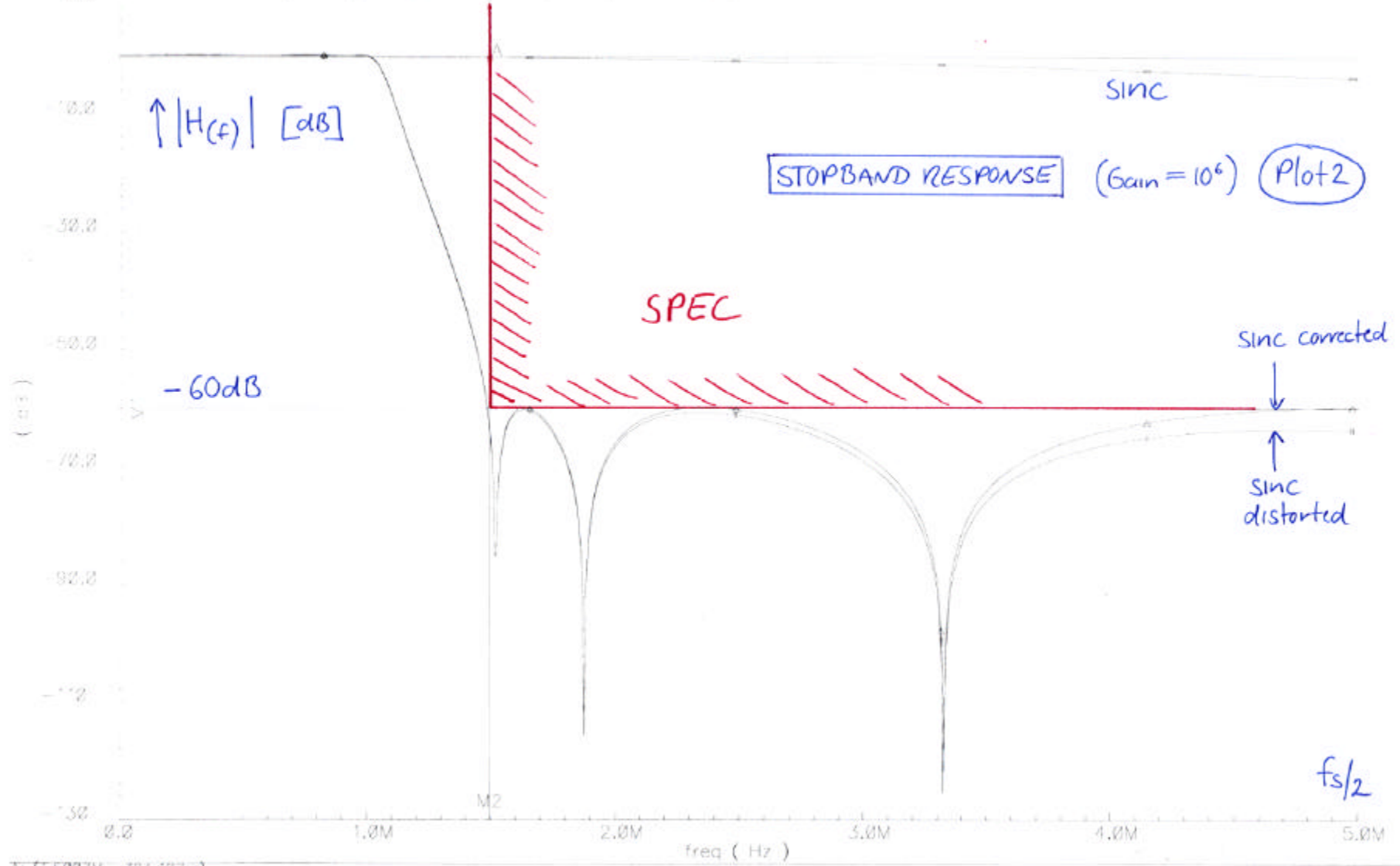
↑ $|H(f)|$ [dB]

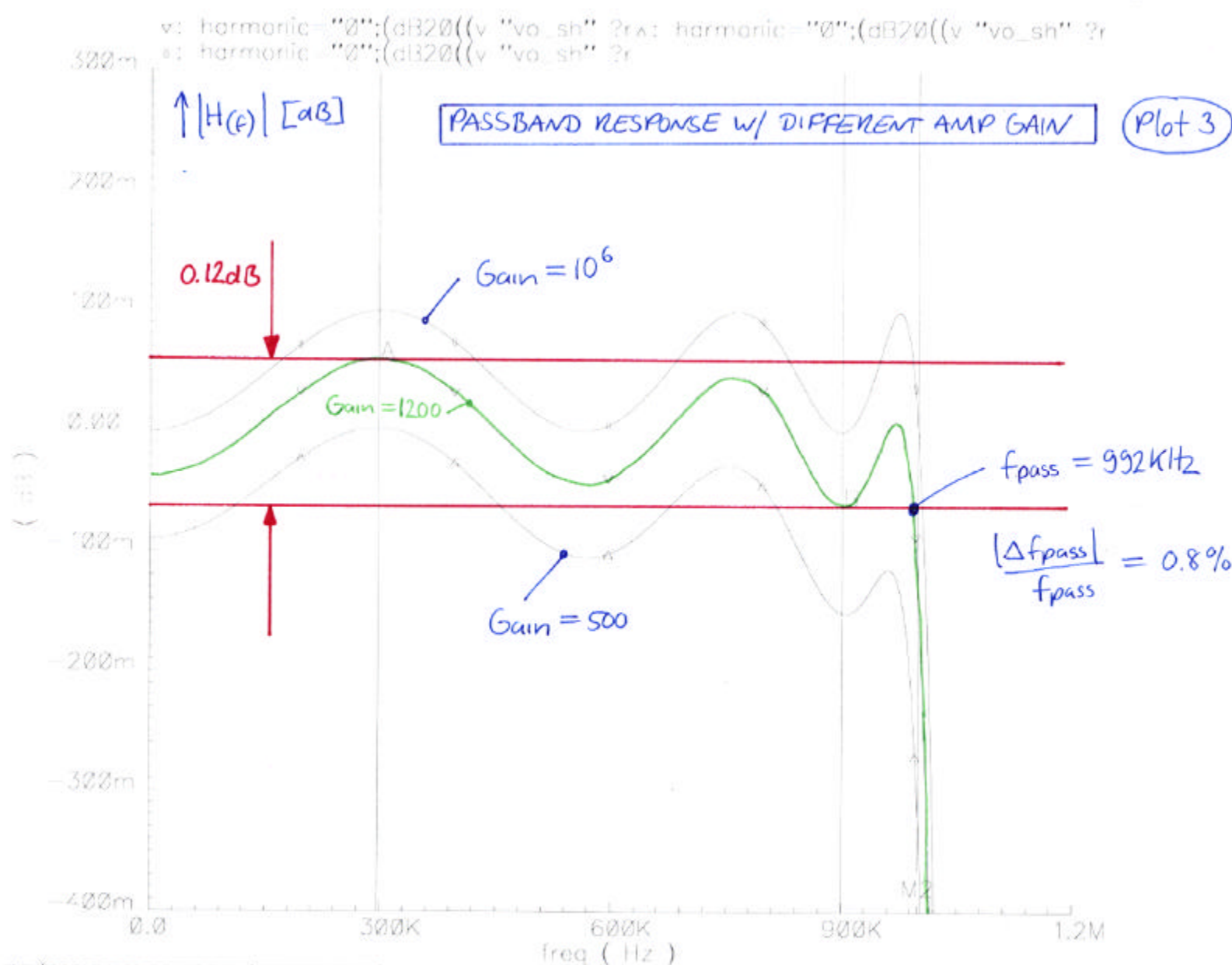
PASSBAND RESPONSE (Gain = 10^6) **Plot 1**



A: (*K 2.3758K)

```
wt: (wavew12s1i1() - wavew12s1i2())
-: harmonic="0";dB20((v "vsinc" ?result "pac2-pac" ?results))
-: harmonic="0";dB20((v "vs_h" ?result "pac2-pac" ?results))
```





A: (299.072K -59.3953m) delta: (601.808K -121.808m)

B: (900.82K -62.4126m) slope: -202.403n

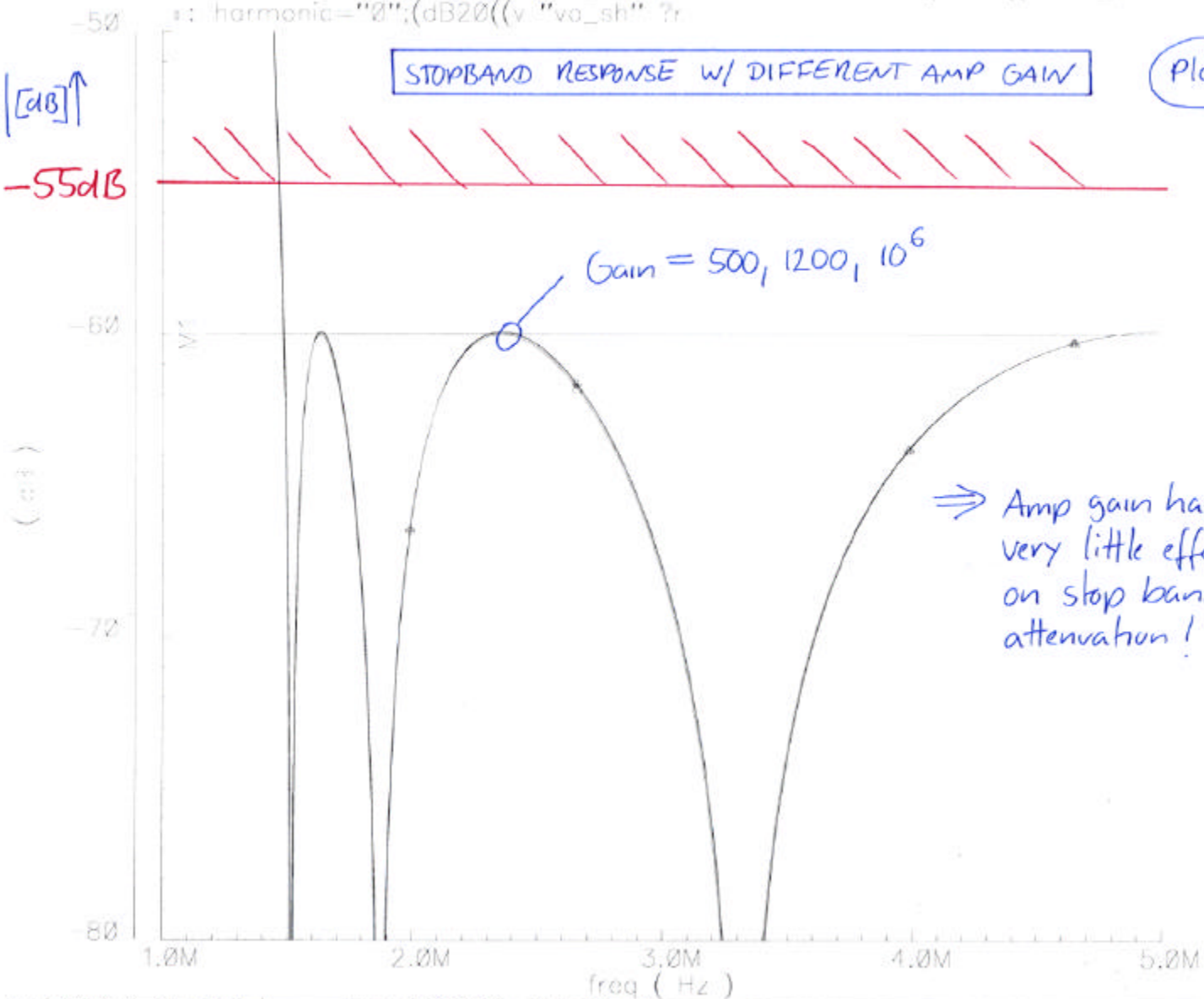
Δ: harmonic="0";(dB20((v "vo_sh" ?r-> harmonic="0";(dB20((v "vo_sh" ?r
*: harmonic="0";(dB20((v "vo_sh" ?r

STOPBAND RESPONSE W/ DIFFERENT AMP GAIN

Plot 4

$|H(f)| [dB] \uparrow$

-55dB



Gain = 500, 1200, 10^6

⇒ Amp gain has very little effect on stop band attenuation!

A: (300.94K 67.5233m) delta: (599.88K -117.389m)
B: (900.82K -49.8657m) slope: -195.687n

% EE247 Homework #4 Boris Murmann

Matlab Script

①

% filter specification

```
clear;
Wpass = 2*pi*1e6;           % passband edge [rad]
Wstop = 2*pi*1.5e6;        % start of stopband [rad]
Rp = 0.1;                   % passband ripple (dB)
Rs = 60;                    % stopband attenuation (dB)
```

% sampling frequency and normalized band specifications

```
Wsamp = 2*pi*10e6;
Wp = 2*Wpass/Wsamp;
Ws = 2*Wstop/Wsamp;
```

% discrete time filter synthesis

```
[N,Wn] = ellipord(Wp, Ws, Rp, Rs);
[num,den] = ellip(N, Rp, Rs, Wn);
freqz(num,den);
```

% break up into biquads - matlab provides optimized pole zero grouping

```
[SOS,G] = tf2sos(num,den)
num1 = SOS(1,1:3);
num2 = SOS(2,1:3);
num3 = SOS(3,1:3);
den1 = SOS(1,4:6);
den2 = SOS(2,4:6);
den3 = SOS(3,4:6);
```

% calculate Q of continous time equivalent sections

```
[Z1, P1, K1] = tf2zp( num1, den1 );
[Z2, P2, K2] = tf2zp( num2, den2 );
[Z3, P3, K3] = tf2zp( num3, den3 );
s1 = (Wsamp/pi) * (P1(1)-1) / (P1(1)+1);
s2 = (Wsamp/pi) * (P2(1)-1) / (P2(1)+1);
s3 = (Wsamp/pi) * (P3(1)-1) / (P3(1)+1);
Q1 = 0.5*sqrt(1+(imag(s1)/real(s1))^2 )
Q2 = 0.5*sqrt(1+(imag(s2)/real(s2))^2 )
Q3 = 0.5*sqrt(1+(imag(s3)/real(s3))^2 )
```

% normalize to positive powers of z and divide by "a2" to match (5.27) Gregorian

```
NUM1 = num1 / den1(3);
NUM2 = num2 / den2(3);
NUM3 = num3 / den3(3);
DEN1 = den1 / den1(3);
DEN2 = den2 / den2(3);
DEN3 = den3 / den3(3);
```

% scale for unity gain at DC (z=1) for each biquad

```
k1 = sum(DEN1) / sum(NUM1);
k2 = sum(DEN2) / sum(NUM2);
k3 = sum(DEN3) / sum(NUM3);
NUM1 = k1 * NUM1;
NUM2 = k2 * NUM2;
NUM3 = k3 * NUM3;
```

% calculate component values, for Q>3 use hi Q circuit

```
C0=1e-12;
if Q1>3
    Caps1 = HiQ(NUM1, DEN1, C0)
else
    Caps1 = LoQ(NUM1, DEN1, C0)
end
if Q2>3
    Caps2 = HiQ(NUM2, DEN2, C0)
else
```

```
    Caps2 = LoQ(NUM2, DEN2, C0)
end
if Q3>3
    Caps3 = HiQ(NUM3, DEN3, C0)
else
    Caps3 = LoQ(NUM3, DEN3, C0)
end
```

②

```
% Lo Q (Q<3) Gregorian p.286
function Caps = LoQ(NUM, DEN, C0)
a2 = NUM(1);
a1 = NUM(2);
a0 = NUM(3);
b2 = DEN(1);
b1 = DEN(2);
b0 = DEN(3);
C2 = sqrt(b1+b2+1);
C3 = sqrt(b1+b2+1);
C1x = a2-a0;
C1xx = a0;
C1 = (a0+a1+a2)/C3;
C4 = b2-1;
Caps = C0*[C1,C1x,C1xx,C2,C3,C4];
```

```
% Hi Q (Q>3) Gregorian p.291
function Caps = HiQ(NUM, DEN, C0)
a2 = NUM(1);
a1 = NUM(2);
a0 = NUM(3);
b2 = DEN(1);
b1 = DEN(2);
b0 = DEN(3);
C2 = sqrt( (1+b1+b2)/b2 );
C3 = sqrt( (1+b1+b2)/b2 );
C1x = (a2-a0) / (b2*C3);
C1xx = a2/b2;
C1 = (a0+a1+a2)/ (b2*C3);
C4 = (1 - (1/b2)) / C3;
Caps = C0*[C1,C1x,C1xx,C2,C3,C4];
```

Spectre Netlist

①

```
*** EE247 HW #4 Boris Murmann

simulator lang=spectre
parameters fs=10Meg c0=1p Ron=1 AmpGain=1e6
//
*** first low Q section
+c11= 4.529440715720658e-013
+clx1= 4.163336342344337e-029 // =zero
+clxx1= 6.857132907366235e-014
+c21= 4.529440715720658e-013
+c31= 4.529440715720658e-013
+c41= 8.677048917763188e-013
//
*** second low Q section
+c12= 6.072036269121990e-013
+clx2= -8.881784197001252e-028 // =zero
+clxx2= 2.985596869872886e-013
+c22= 6.072036269121991e-013
+c32= 6.072036269121991e-013
+c42= 4.049018365178336e-013
//
*** hi Q section
+c13= 6.302625148882051e-013
+clx3= -2.079239384327061e-027 // =zero
+clxx3= 4.712310360217251e-013
+c23= 6.302625148882049e-013
+c33= 6.302625148882049e-013
+c43= 1.460155701618134e-013

*** stimulus
vin1 (vin 0) vsource pacmag=1
//vin1 (vin 0) vsource type=sine ampl=1 freq=fs/10
vphi1 (phi1 0) vsource type=pulse val0=0 vall=1 period=1/fs
width=0.45/fs rise=.1n fall=.1n delay=0.05/fs
vphi2 (phi2 0) vsource type=pulse val0=0 vall=1 period=1/fs
width=0.45/fs rise=.1n fall=.1n delay=0.55/fs

*** circuit
b1 (vin vo1 phi1 phi2) loq pc0=c0 pc1=c11 pclxx=clxx1 pc2=c21
pc3=c31 pc4=c41
b2 (vo1 vo2 phi1 phi2) loq pc0=c0 pc1=c12 pclxx=clxx2 pc2=c22
pc3=c32 pc4=c42
b3 (vo2 vout phi1 phi2) hiq pc0=c0 pc1=c13 pclxx=clxx3 pc2=c23
pc3=c33 pc4=c43

*** sample and hold output
c1 (vout 0) capacitor c=100f
buf1 (voutbuf 0 vout 0) vcvs gain=1
s2 (voutbuf vo_sh phi1 0) relay vt1=0 vt2=1 rclosed=1
ropen=100e9
c2 (vo_sh 0) capacitor c=100f

*** sample and hold input (-> sinc response for correction)
s11 (vin vth phi2 0) relay vt1=0 vt2=1 rclosed=1
ropen=100e9
c11 (vth 0) capacitor c=100f
buf11 (vthbuf 0 vth 0) vcvs gain=1
s21 (vthbuf vsinc phi1 0) relay vt1=0 vt2=1 rclosed=1
```



```

ropen=100e9
c21 (vsinc 0) capacitor c=100f

*****
* Lo Q biquad
subckt loq (vi vos phi1 phi2)
parameters pc0 pc1 pclxx pc2 pc3 pc4
rsim1 (vi n2 phi2 phi1 a n1) rsim_series
Csamp=pc1
rsim2 (v1 n4 phi1 phi2 n3 b) rsim_series_inv
Csamp=pc3
clxx (vi n4) capacitor c=pclxx
c2 (n1 n5) capacitor c=pc2
c4 (n5 b) capacitor c=pc4
switch1 (n5 0 phi1 0) relay vt1=0 vt2=1 rclosed=Ron
ropen=100e9
switch2 (n5 vo phi2 0) relay vt1=0 vt2=1 rclosed=Ron
ropen=100e9
switch3 (vos vo phi2 0) relay vt1=0 vt2=1
rclosed=Ron ropen=100e9
amp1 (v1 0 0 n2) vcvs gain=AmpGain
amp2 (vo 0 0 n4) vcvs gain=AmpGain
ca (n2 v1) capacitor c=pc0
cb (n4 vo) capacitor c=pc0
ends loq

* Hi Q biquad
subckt hiq (vi vos phi1 phi2)
parameters pc0 pc1 pclxx pc2 pc3 pc4
rsim1 (vi n2 phi2 phi1 a n1) rsim_series
Csamp=pc1
rsim2 (v1 n4 phi1 phi2 n3 b) rsim_series_inv
Csamp=pc3
clxx (vi n4) capacitor c=pclxx
c2 (n1 n5) capacitor c=pc2
c4 (n2 vo) capacitor c=pc4
switch1 (n5 0 phi1 0) relay vt1=0 vt2=1 rclosed=Ron
ropen=100e9
switch2 (n5 vo phi2 0) relay vt1=0 vt2=1 rclosed=Ron
ropen=100e9
switch3 (vos vo phi2 0) relay vt1=0 vt2=1
rclosed=Ron ropen=100e9
amp1 (v1 0 0 n2) vcvs gain=AmpGain
amp2 (vo 0 0 n4) vcvs gain=AmpGain
ca (n2 v1) capacitor c=pc0
cb (n4 vo) capacitor c=pc0
ends hiq

* simulated resistor with capacitor in series
subckt rsim_series (v1 vr phi1 phi2 n1 n2)
parameters Csamp
cs (n1 n2) capacitor c=Csamp
s1 (v1 n1 phi1 0) relay vt1=0 vt2=1 rclosed=Ron ropen=100e9
s2 (n1 0 phi2 0) relay vt1=0 vt2=1 rclosed=Ron ropen=100e9
s3 (n2 0 phi2 0) relay vt1=0 vt2=1 rclosed=Ron ropen=100e9
s4 (n2 vr phi1 0) relay vt1=0 vt2=1 rclosed=Ron ropen=100e9
cp1 (n1 0) capacitor c=1f
cp2 (n2 0) capacitor c=1f

```

```
ends rsim_series

* simulated resistor with capacitor in series and charge inversion
subckt rsim_series_inv (v1 vr phi1 phi2 n1 n2)
  parameters Csamp
  cs      (n1 n2)          capacitor c=Csamp
  s1      (v1 n1 phi1 0 ) relay vt1=0 vt2=1 rclosed=Ron ropen=100e9
  s2      (n1 0 phi2 0 ) relay vt1=0 vt2=1 rclosed=Ron ropen=100e9
  s3      (n2 0 phi1 0 ) relay vt1=0 vt2=1 rclosed=Ron ropen=100e9
  s4      (n2 vr phi2 0 ) relay vt1=0 vt2=1 rclosed=Ron ropen=100e9
  cp1     (n1 0)           capacitor c=1f
  cp2     (n2 0)           capacitor c=1f
ends rsim_series_inv
*****

pss2 pss fund=fs maxacfreq=fs/2 tstab=1/fs/4
pac2 pac start=1k stop=fs/2 lin=1000
*tran1 tran stop=10/fs method=gear2only

simOptions options
+ rawfmt=psfbin
+ reltol=1e-5
+ vabstol=1n
+ iabstol=1p

alter1 alter param=AmpGain value=1.2e3
pss3 pss fund=fs maxacfreq=fs/2 tstab=1/fs/4
pac3 pac start=1k stop=fs/2 lin=1000

alter2 alter param=AmpGain value=0.5e3
pss4 pss fund=fs maxacfreq=fs/2 tstab=1/fs/4
pac4 pac start=1k stop=fs/2 lin=1000
```